

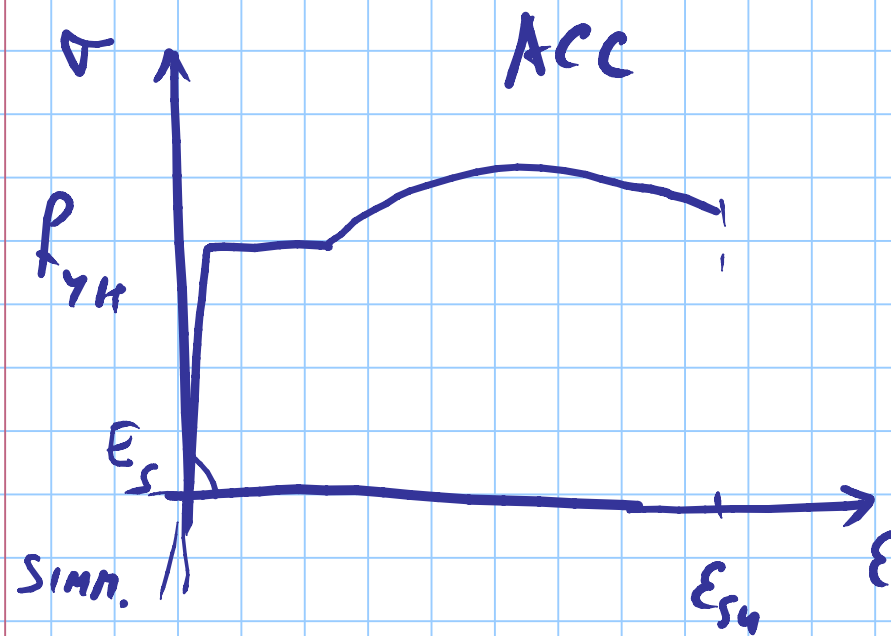
per $\sigma_c > 0.85 f_{ck}$
comport. non stabile

$$\alpha_{cc} f_{ck}$$

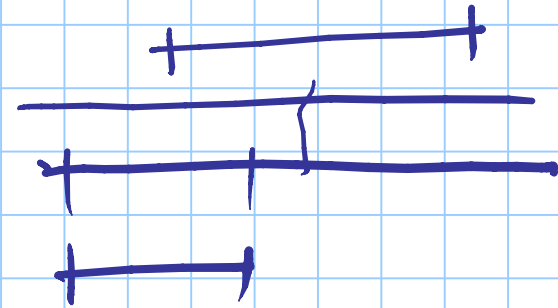
↑
0.85

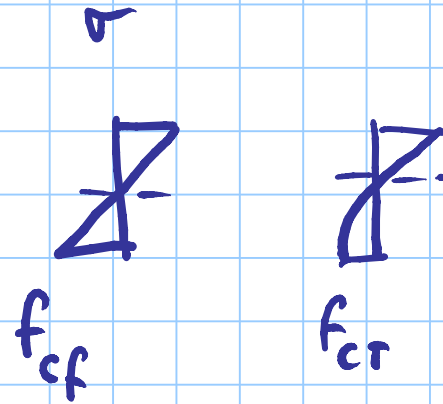
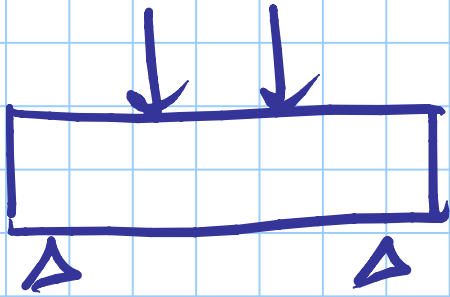
C 25/30
↑ ↑
 f_{ck} R_{ck}

$$E_c = 31500 \text{ MPa}$$



$$E_s = 206000 \text{ MPa}$$





$$f_{ctk} = 1.2 f_{ct}$$

①

DEFORMAZIONI / TENSIONI.

MOLTO PICCOLE

LEGAME LINEARE

sia a trazione

che a compressione

USATO PER COMPORTAMENTO

PRIMA DELLA FESSURAZIONE
determinare di M_r , N_r di fessurazione

SOTTO I CARICHI DI ESERCIZIO (Zone più sollecitate)
si supera la resistenza a trazione del cls

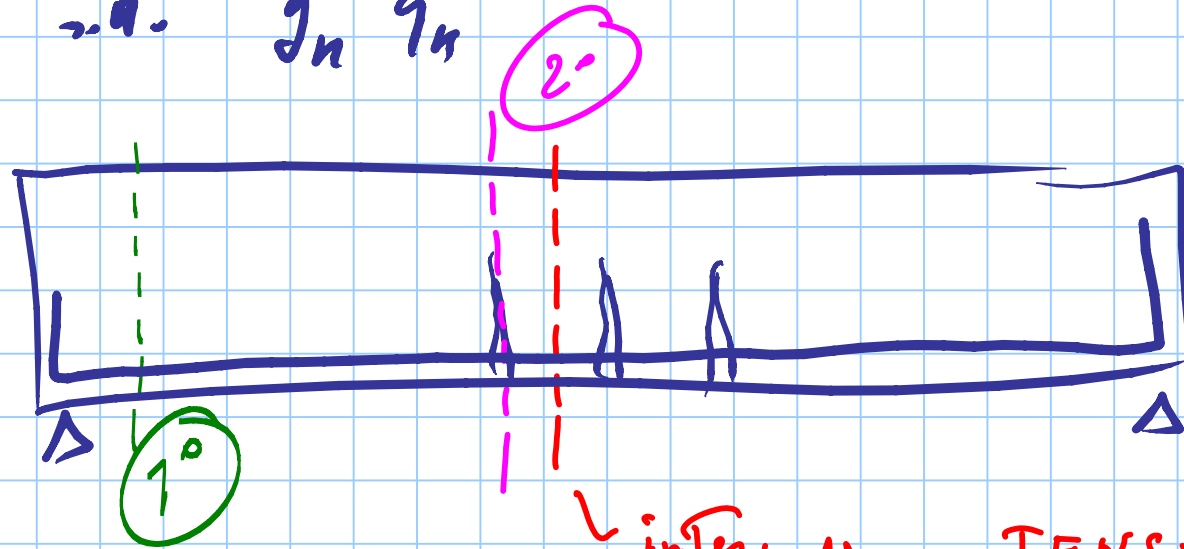
② LEGAME LINEARE PER CLS COMPRESSO
NESSUNA RESISTENZA A TRAZIONE

(VALE IN CORRISP. DELLE LESIONI)

- PERFETTA ADERENZA CLS-ACC $\rightarrow \epsilon_c = \epsilon_s$
- DIAGRAMMA DI DEFORMAZIONE LINEARE

SLE tensioni in acciaio | Verifica TA

TRAVERSE I_n q_n



$M \approx 0$

intermediate

TENSION
STIFFENING

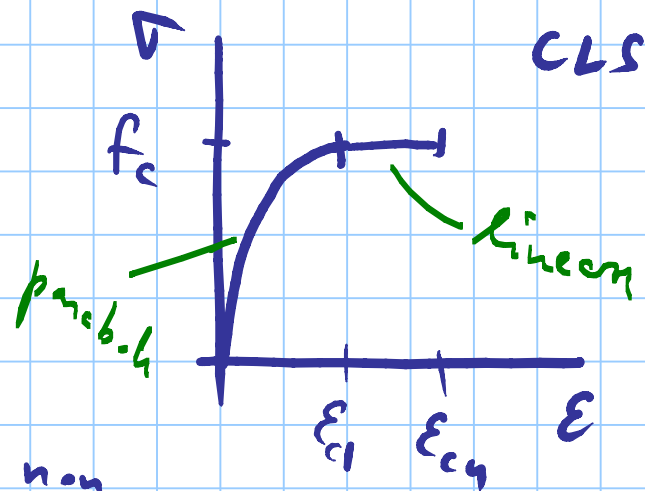
non only
 $\epsilon_c = \epsilon_s$

SLE deformation
formation

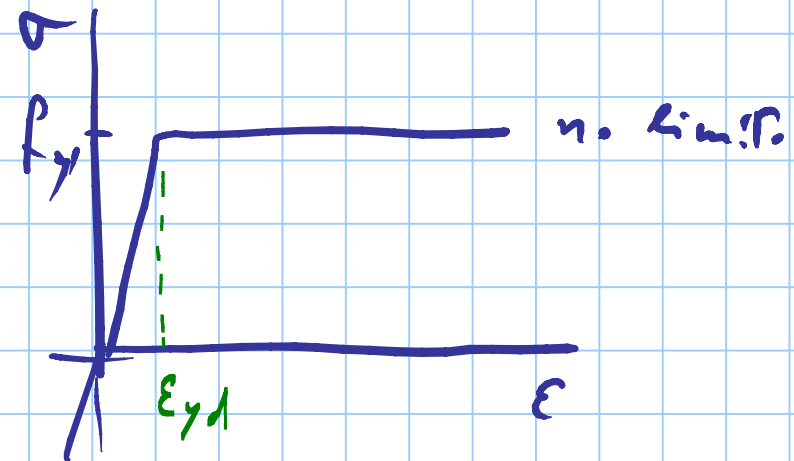
DEFORMAZIONI / TENSIONI ELEVATE

non linearità del materiale

③



CLS non
unif. a fratt.

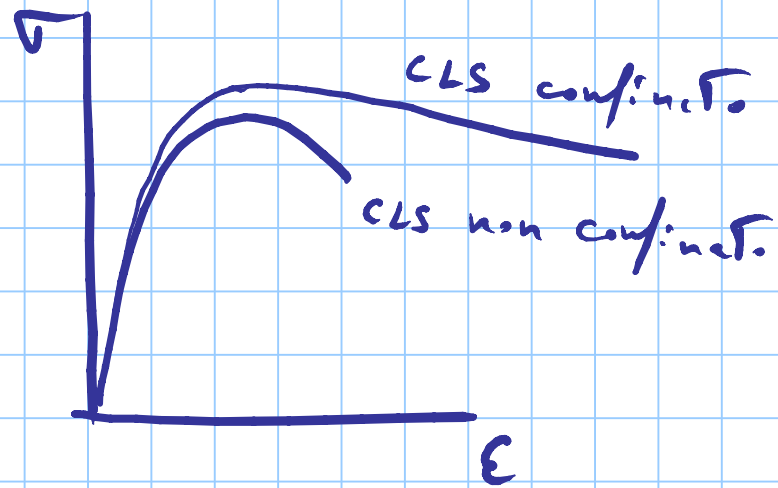


VERIFICHE DI RESISTENZA SLU

$$f_{cd} = \frac{\alpha_{cc} f_{ck}}{\gamma_c}$$

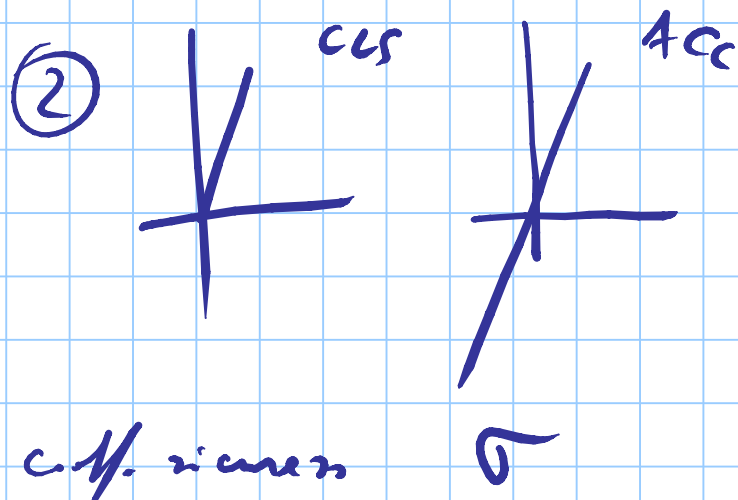
$$f_{yd} = \frac{f_{yk}}{\gamma_s}$$

MODELLI PIÙ SOFISTICATI del materiale



PER VALUTARE DUTTILITÀ

TA



$$E_c = E_s$$

$$Q_s = n Q_c$$

$$A_s Q_s$$

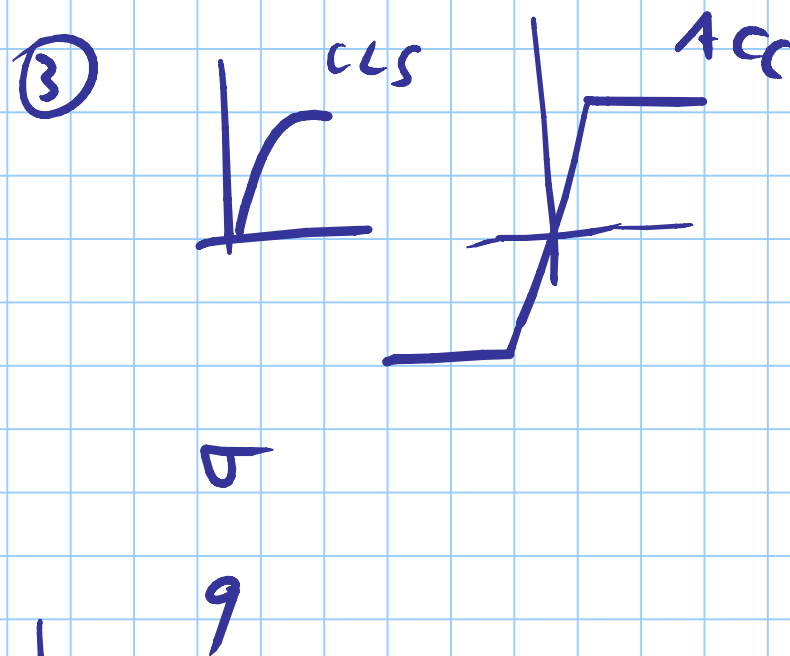
OMOGENEIZZAZ., $n = \frac{E_s}{E_c}$

$$mA_s Q_c$$

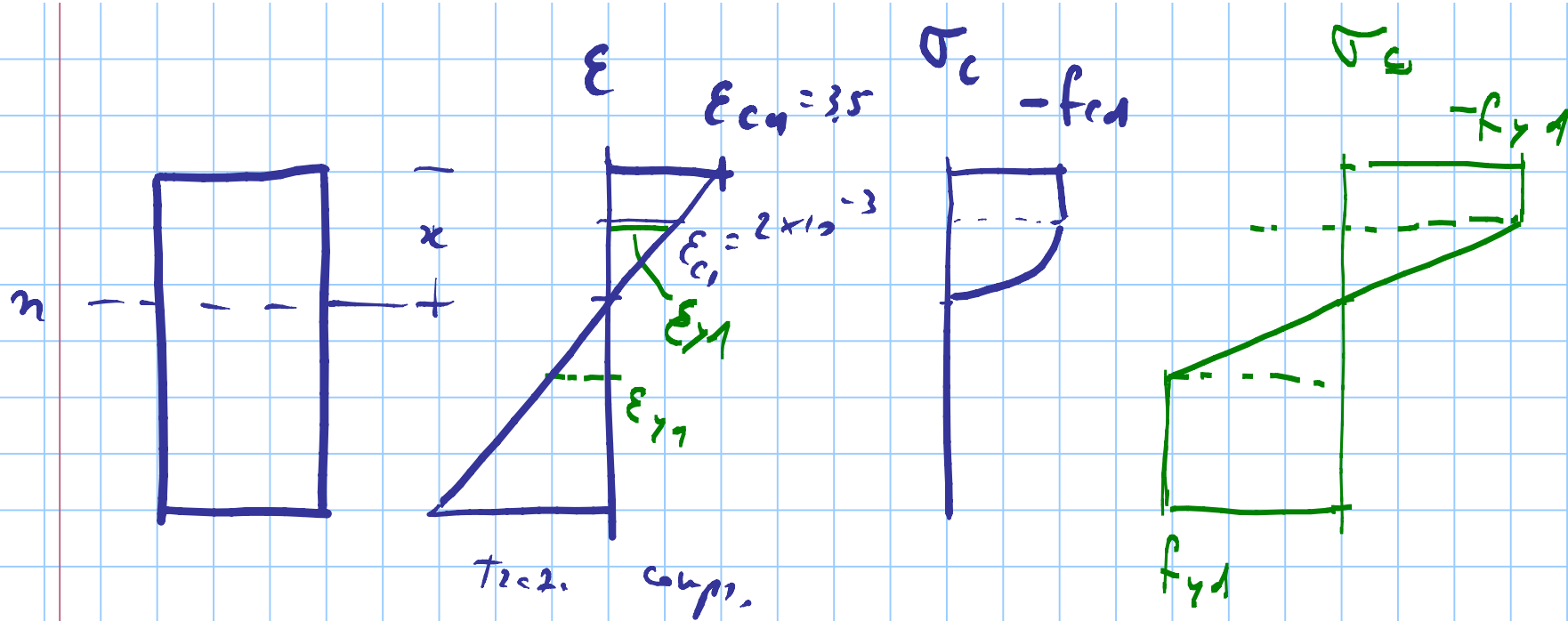
SAC

SEZ. REAGENTE OMOGENEIZZ.

SLU



cond. di equilibrio

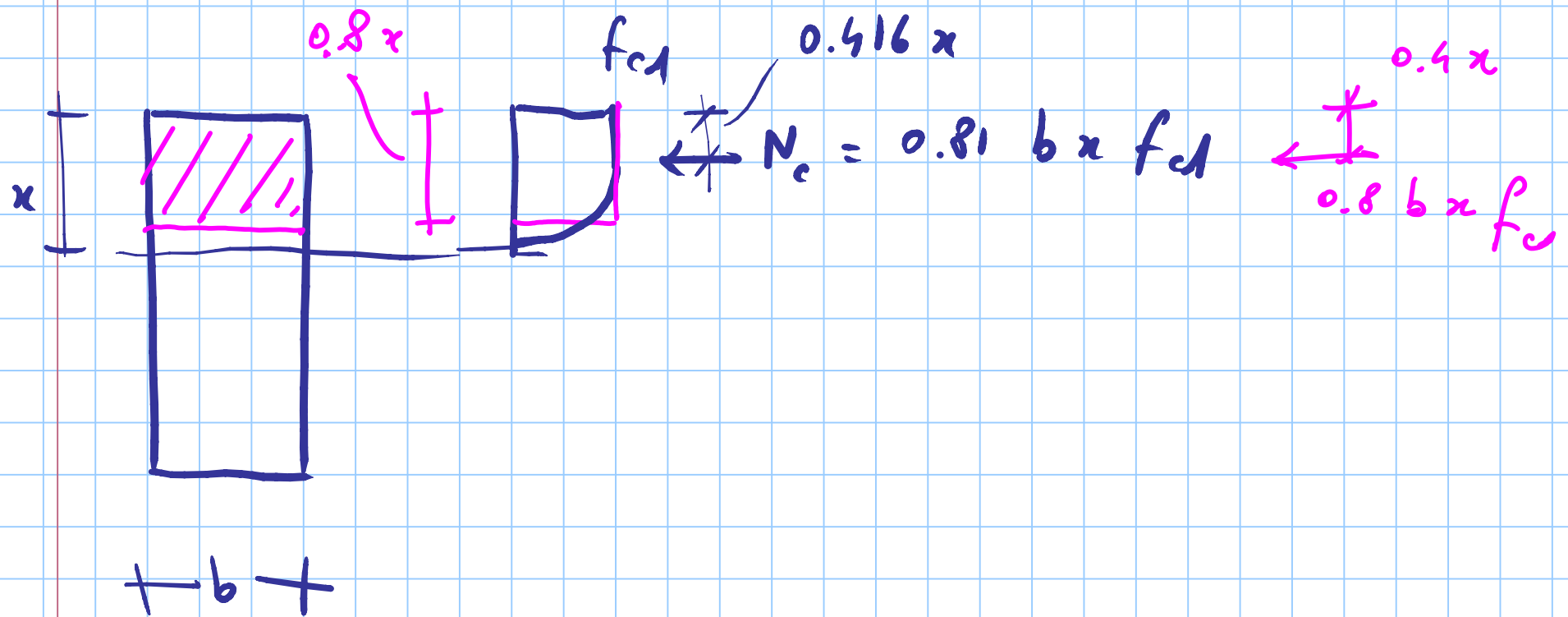


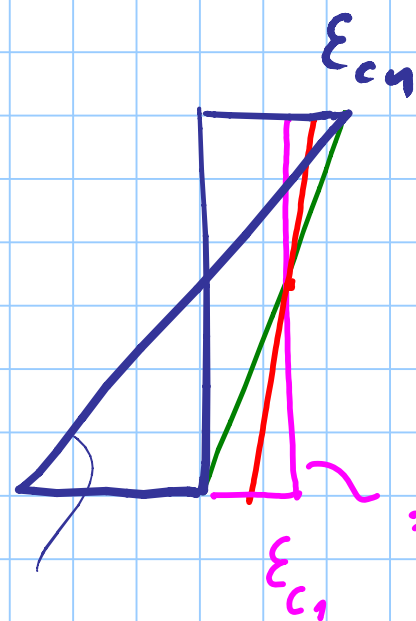
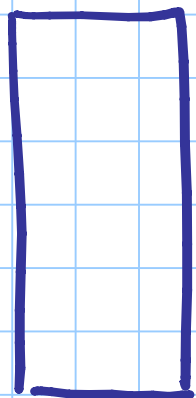
B 450 C

$$f_{yk} = 450 \text{ MPa}$$

$$f_{yd} = \frac{450}{1.15} = 391.3 \text{ MPa}$$

$$\epsilon_{s1} = \frac{f_{yd}}{E_s} = 1.96 \times 10^{-3}$$





not
partial

not unif. comp

