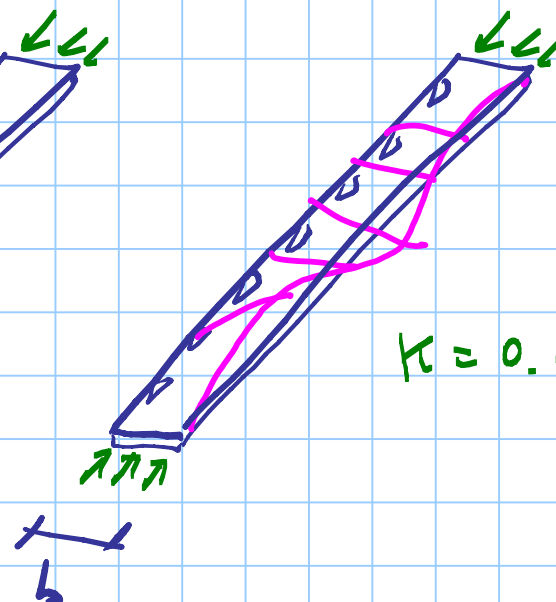
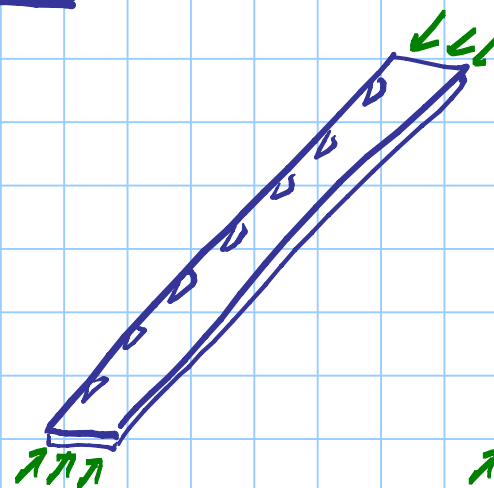
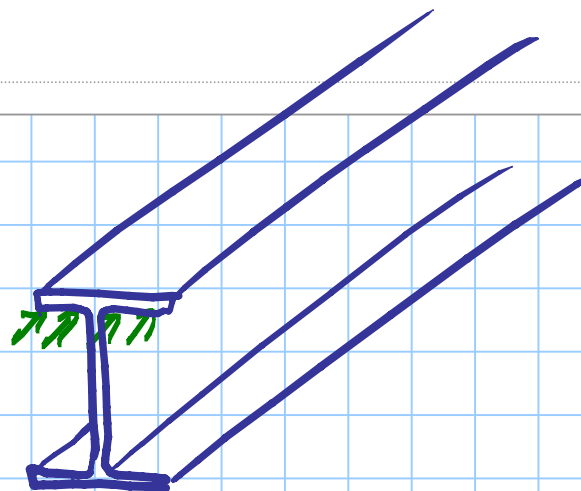
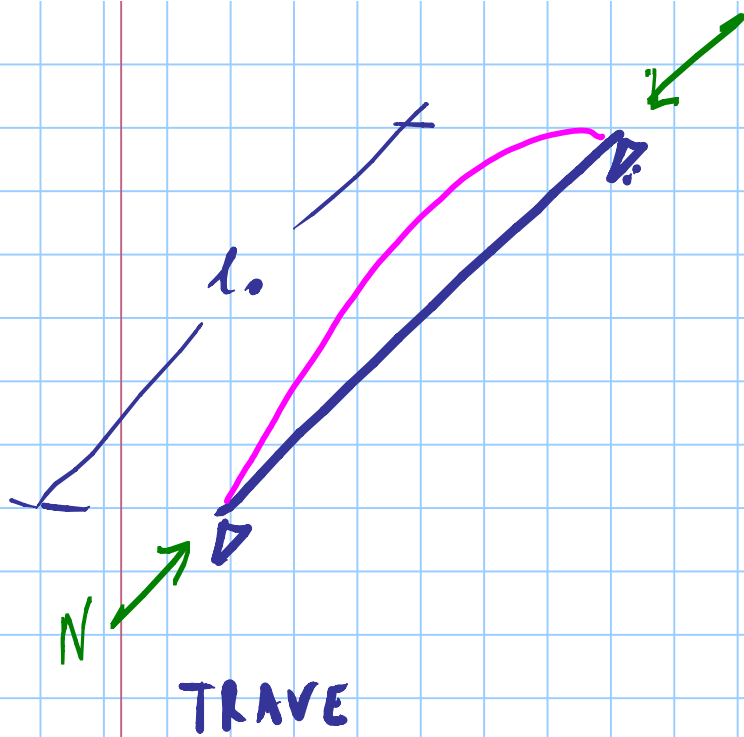


LAISTRA

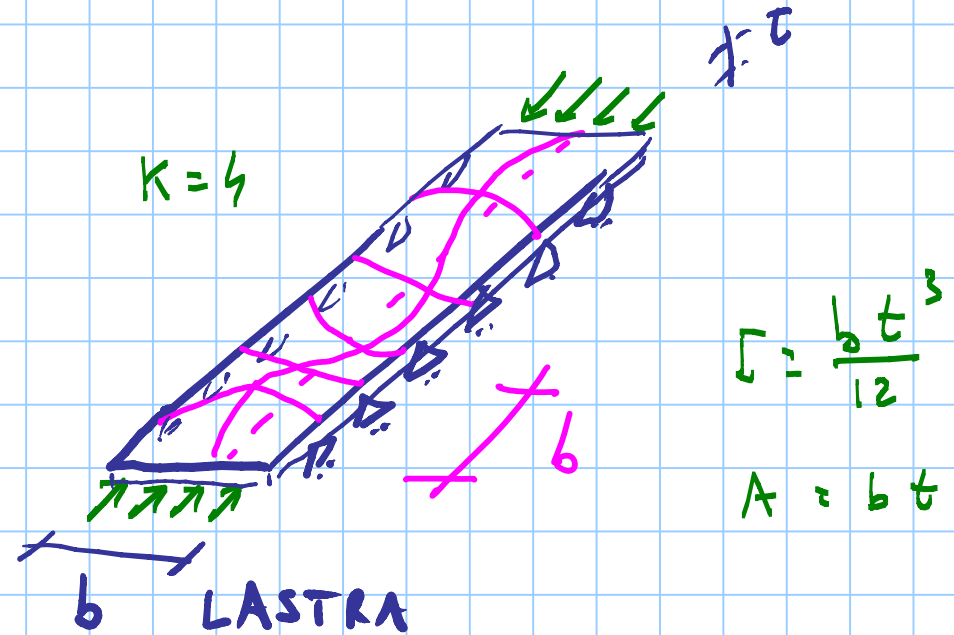


$$\kappa = 0.43$$



$$N_{cr} = \frac{\pi^2 EI}{l_0^2}$$

$$\rho_{cr} = \frac{\pi^2 E}{\lambda^2}$$

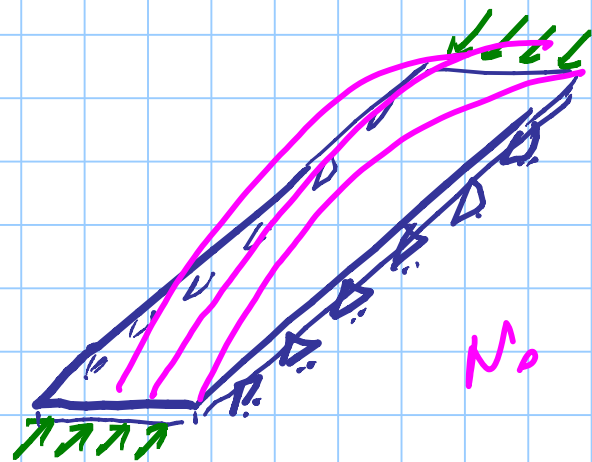


$$I = \frac{b t^3}{12}$$

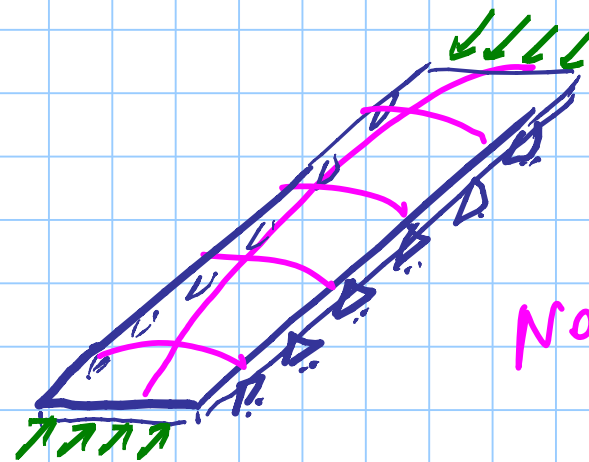
$$A = b t$$

$$N_{cr} = \frac{K \pi^2 EI}{(1-\nu^2) b^2}$$

$$\rho_{cr} = \frac{K \pi^2 E I}{(1-\nu^2) b^2 A} = \frac{K \pi^2 E}{12(1-\nu^2) \left(\frac{b}{t}\right)^2}$$

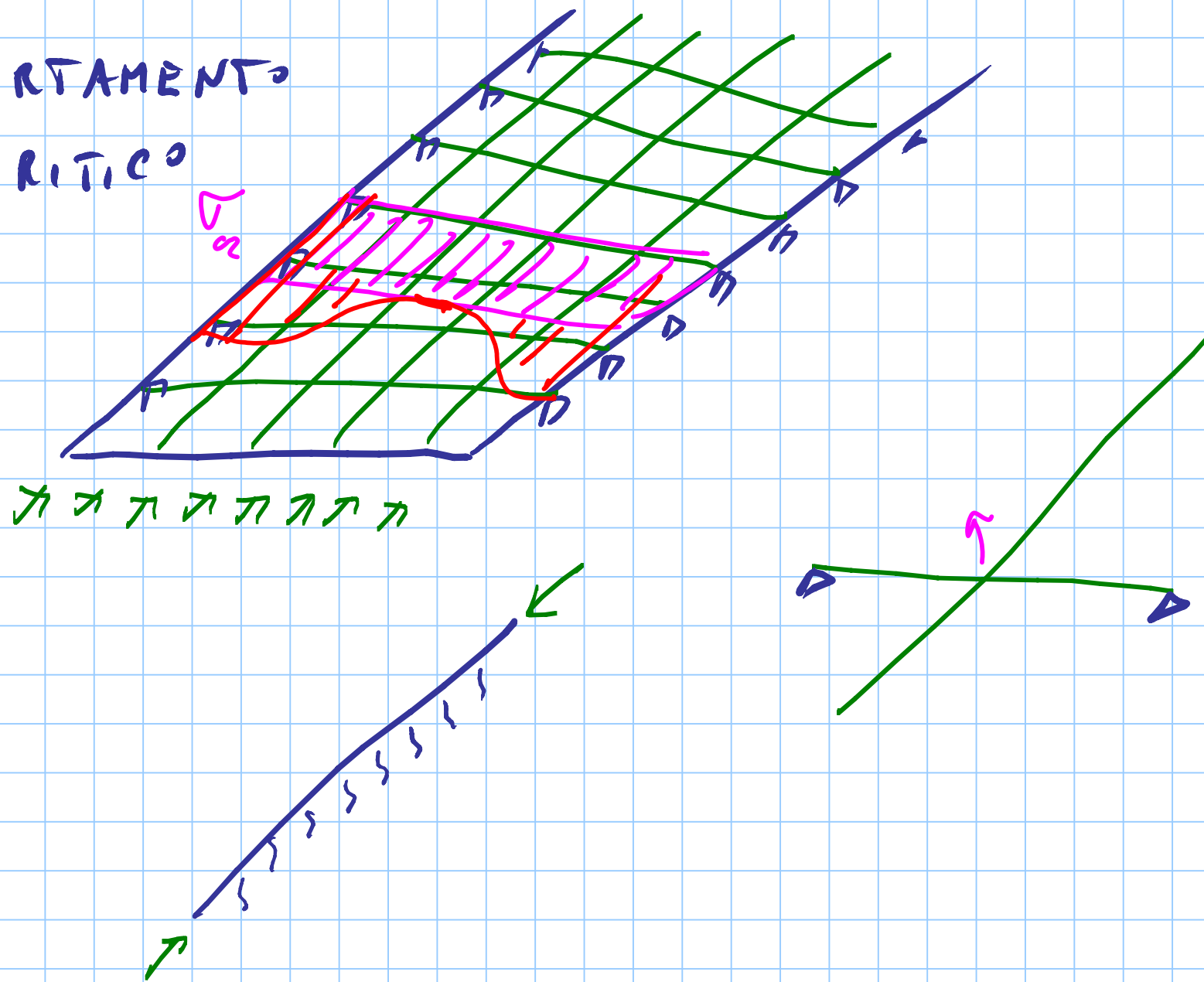


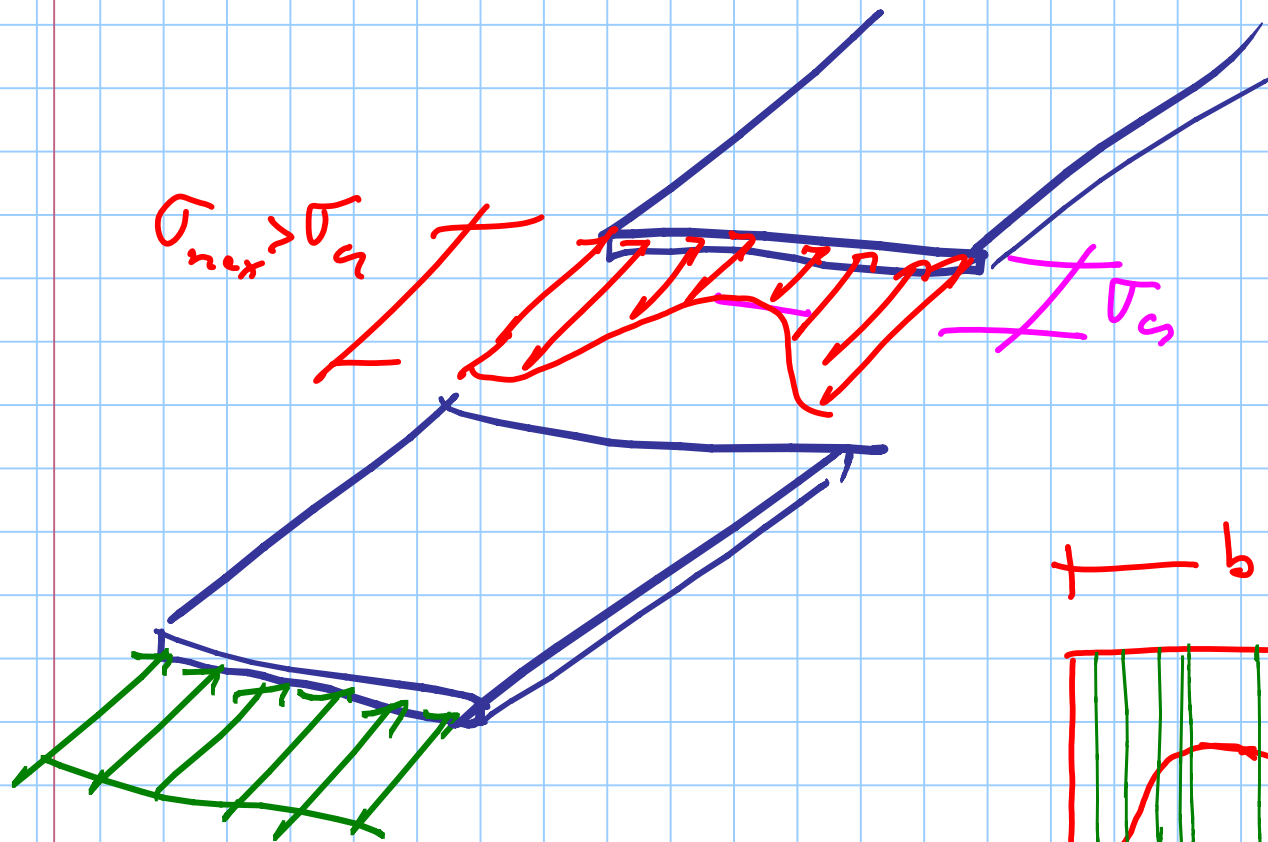
LASTRA



LASTRA

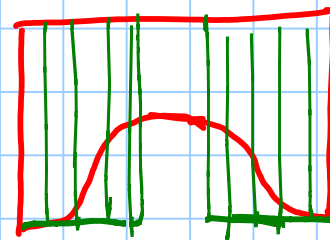
COMPORTAMENTO  
POST-CRÍTICO





Von Karman  
1932

$b$



$\sigma_{max}$

largest  
efficiency

$b_{eff}/2$

$b_{eff}/2$

$b_{eff}$

$b_{eff}$  corris. a  $\sigma_{max}$

è quella  $b$  per cui  $\sigma_{max} = \sigma_c$

$$\sigma_c = \frac{\kappa \pi^2 E}{12(1-\nu^2) \left(\frac{b}{t}\right)^2}$$

$$\frac{\sigma_{max}}{\sigma_c} = \frac{b^2}{b_{eff}^2}$$

$$\sigma_{max} = \frac{\kappa \pi^2 E}{12(1-\nu^2) \left(\frac{b_{eff}}{t}\right)^2}$$

$$\frac{b}{b_{eff}} = \sqrt{\frac{\sigma_{max}}{\sigma_c}} = \bar{\lambda}_p$$

$\downarrow$   
PLATE

$$\bar{\lambda}_p = \sqrt{\frac{f_y}{\sigma_c}}$$

$$\frac{b}{b_{eff}} = \bar{\lambda}_p \quad \Rightarrow \quad \rho = \frac{b_{eff}}{b} = \frac{1}{\bar{\lambda}_p}$$

$$\bar{\lambda}_p = \frac{b/t}{28.4 \varepsilon \sqrt{\kappa}} \quad \varepsilon = \sqrt{\frac{235}{f_y}}$$

$$\bar{\lambda}_p = \sqrt{\frac{f_y 12(1-\nu^2)(b/t)^2}{\kappa \pi^2 E}} = \frac{b}{t} \frac{1}{\sqrt{\kappa}} \sqrt{\underbrace{\frac{235 12(1-\nu^2)}{\pi^2 E}}_{\frac{1}{28.4}} \underbrace{f_y}_{\frac{1}{\varepsilon}}}$$

$$\rho = \frac{b \cdot t}{b} \geq \frac{1}{\bar{\lambda}_p}$$

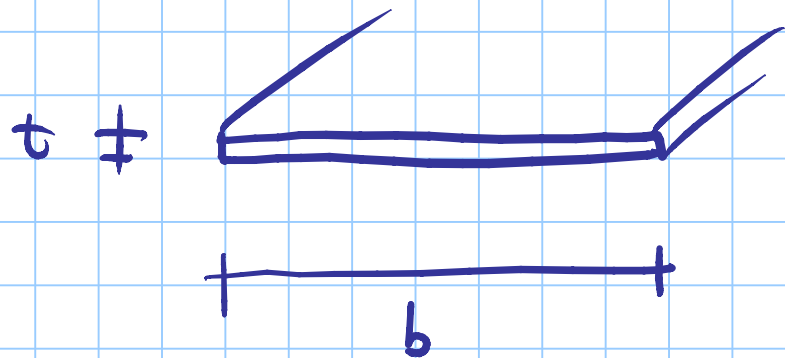
larghezza efficace  
controll. a  $\sigma_{max} = f_y$

$$N_y = f_y \cdot b \cdot t$$

per tener conto delle imperfezioni

$$\rho = \frac{b \cdot t}{b} = \frac{\bar{\lambda}_p - 0.22}{\bar{\lambda}_p^2}$$

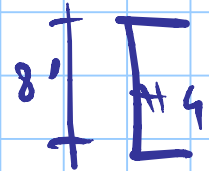




$$b = 80 \text{ mm}$$

$$t = 4 \text{ mm}$$

UPE 80



S 275

$$\sigma_u = \frac{\kappa \pi^2 E}{12(1-\nu^2) \left(\frac{b}{t}\right)^2} = \frac{4 \times 3.14^2 \times 206000}{12(1-0.3^2) \times 20^2} = 1862 \text{ MPa}$$

$$\bar{\lambda}_p = \sqrt{\frac{f_y}{\sigma_u}} = \sqrt{\frac{275}{1862}} = 0.384$$

$$\rho = \frac{0.384 - 0.22}{0.384^2} = 1.11 > 1 \quad \rho = 1 \quad b_{eff} = b$$

$$b = 400 \text{ mm}$$

$$t = 4 \text{ mm}$$

$$\varepsilon = \sqrt{\frac{235}{f_y}} = 0.924 \quad S 275$$

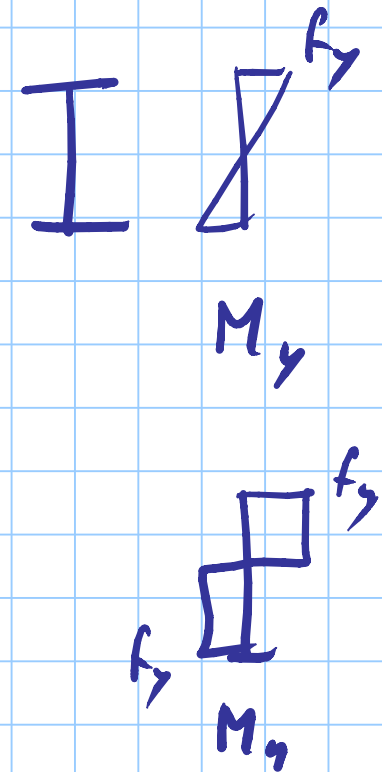
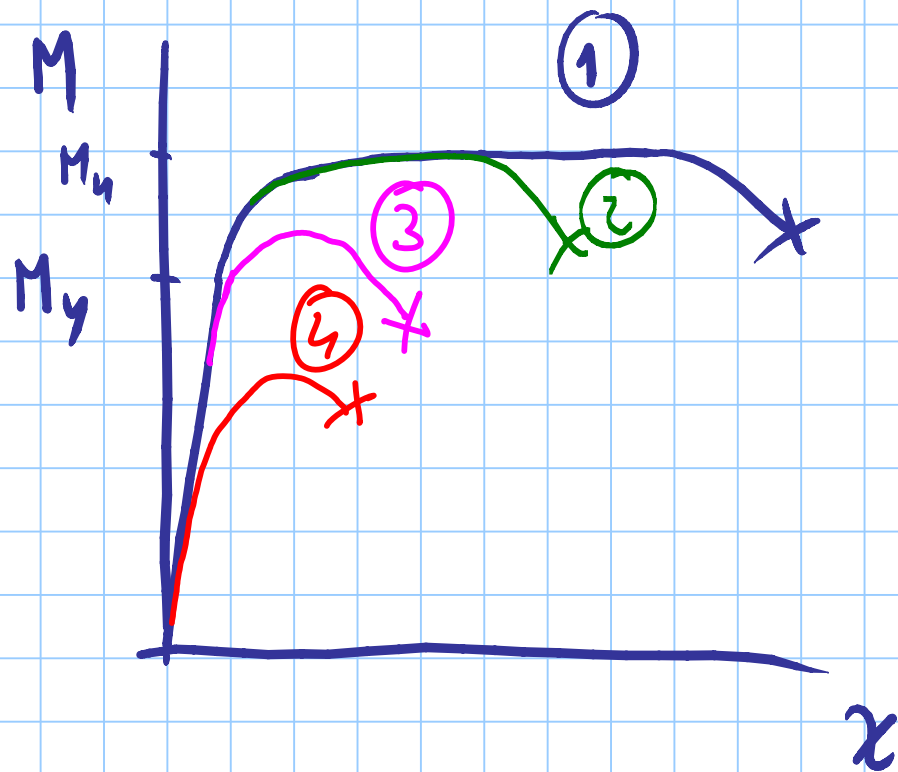
$$\bar{\lambda}_p = \frac{b/t}{28.4 \varepsilon \sqrt{K}} = \frac{100}{28.4 \times 0.924 \times \sqrt{6}} = 1.905$$

$$\rho = \frac{b_{eff}}{b} = \frac{1.905 - 0.22}{1.905^2} = 0.464$$

$$b_{eff} = 400 \text{ mm} \times 0.464 = 185.6 \text{ mm}$$

$$N_{RA} = b_{eff} \cdot t \cdot \frac{f_y}{\gamma_{m0}} = \frac{185.6 \times 4 \times 275}{10^3} = 194.4 \text{ kN}$$

# CLASSIFICAZIONE DELLE SEZIONI



classe 1

max resistenza

$$M_{rd} = W_{pl} \frac{f_y}{\gamma_{m0}}$$

grande duttilità

classe 2

max resistenza

..

media duttilità

classe 3

resistenza lim. a 1° plast

$$M_{rd} = W_{el} \frac{f_y}{\gamma_{m0}}$$

classe 4

fora rif. a sezione efficace

$$M_{rd} = W_{el,eff} \frac{f_y}{\gamma_{m0}}$$