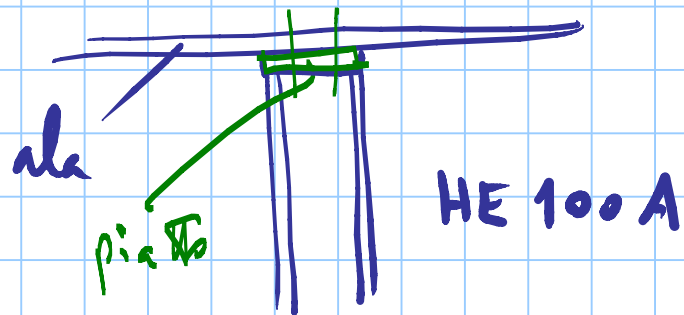


S275

Titolo nota

15/01/2013

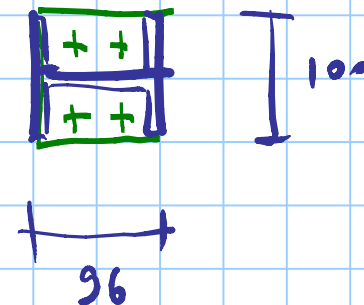


$$N_{EA} = 500 \text{ kN}$$

$$F_{t,EA} = \frac{500}{4} = 125 \text{ kN}$$

$$A \geq \frac{N_{Ed} \gamma_m}{f_y}$$

$$= \frac{500 \times 10^3 \times 1.05}{275} = 19.09 \times 10^2 \text{ mm}^2$$



$$F_{t,R1} = 0.9 A_{ns} \frac{f_{ub}}{\gamma_{M2}}$$

M_{18} $\xrightarrow{\hspace{2cm}}$ 102
 bulloni M16 $A_{ns} = 157 \text{ mm}^2$

$$f_{ub} \geq \frac{F_{t,Ed} \gamma_{M2}}{0.9 A_{ns}} = \frac{125 \times 10^3 \times 1.25}{0.9 \times 157} = 1106 \text{ MPa}^{90\%}$$

4 bulloni M18 classe 10.9

verifica a punzonamento

- alba del profilo superiore
- piatto da saldare

$$F_{T,Ed} \leq B_{r,ed} = 0.6 \pi d_m t \frac{f_u}{\gamma_{M2}} \geq 125 \text{ kN}$$

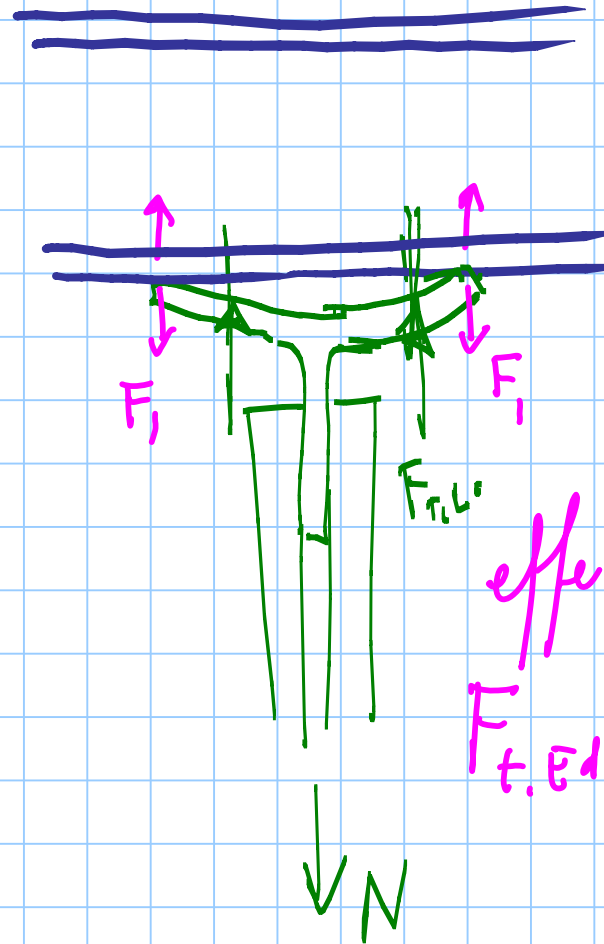
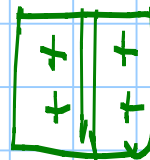
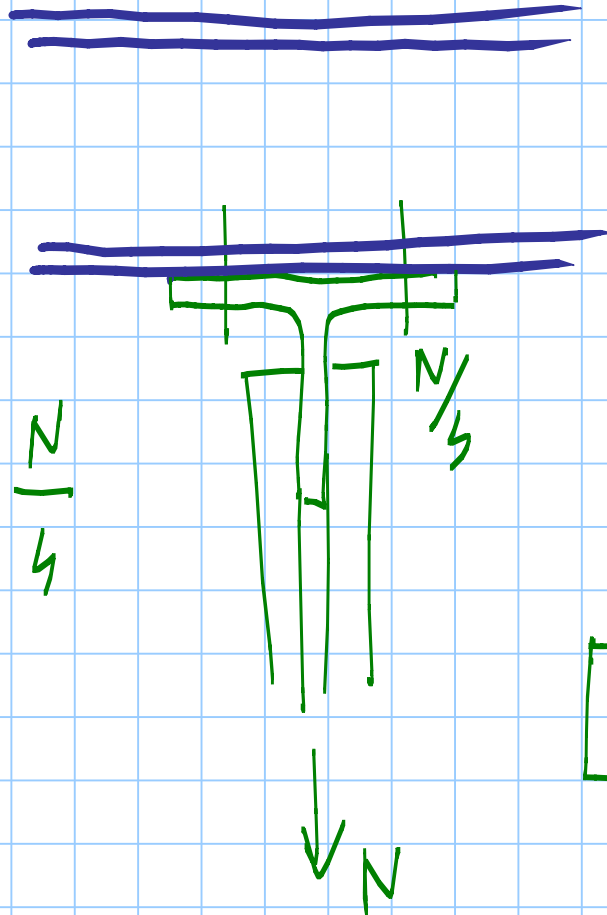
$$d_m \approx 1.6 d = 1.6 \times 18 = 28.8 \text{ mm}$$

$$t \geq \frac{F_{T,Ed} \gamma_{M2}}{0.6 \pi d_m f_u} = \frac{125 \times 10^3 \times 1.25}{0.6 \times 3.14 \times 28.8 \times 430} = 6.7 \text{ mm}$$

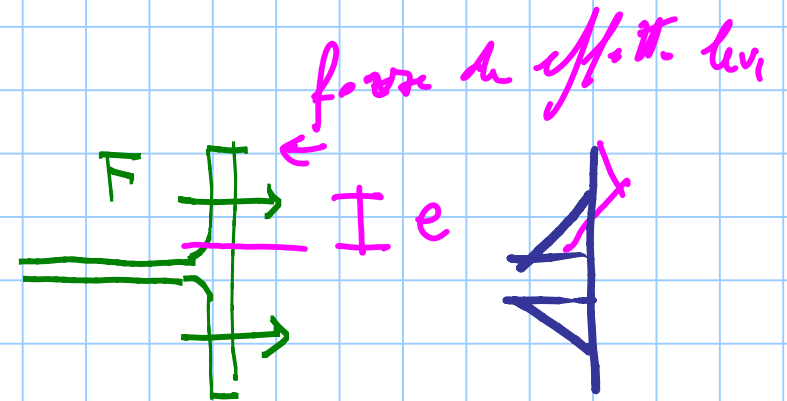
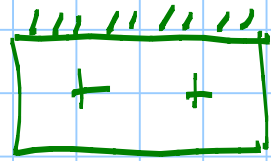
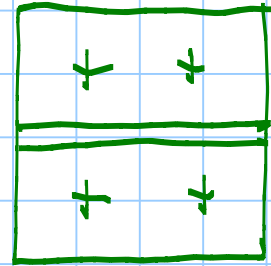
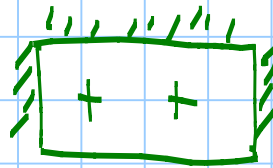
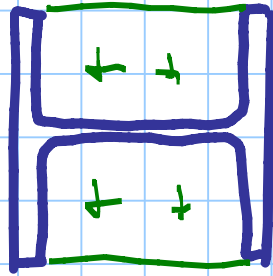
ATTENZIONE

quando abbiamo bulloni tesi

$$F_{t,Ed} = \frac{N}{4}$$



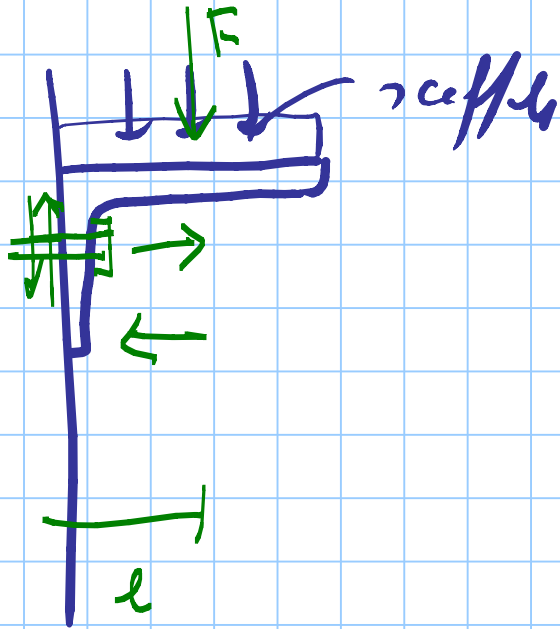
effetto leva
 $F_{t,Ed} > \frac{N}{4}$



l'effetto leva

- aumenta sollecitazioni a trazione nel bullone (e rischio di puzze)
- riduce la flessione nel piatt.

BULLONI A TAGLIO + TRAZIONE

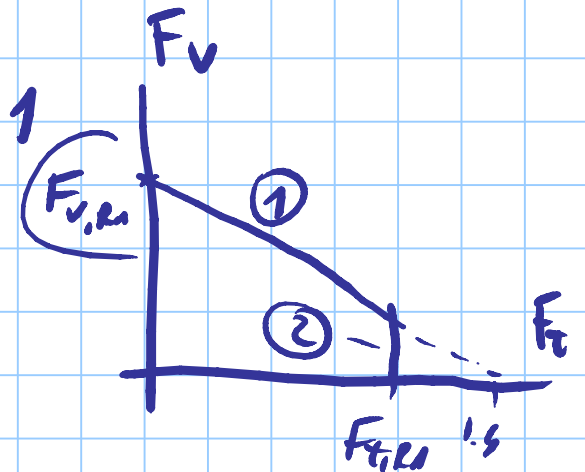


il bullone lavora
sia a Trazione (per M)
che a taglio (per V)

$$M = Fl$$

$$\textcircled{1} \frac{F_{v,Ed}}{F_{v,Rd}} + \frac{F_{t,Ed}}{1.4 F_{t,Rd}} \leq 1$$

$$\textcircled{2} F_{t,Ed} \leq F_{t,Rd}$$



COLLEGAMENTI AD ATTRITO

come per Taglio, ma tale da non superare la res. ad attrito.

serraggio dei bulloni \rightarrow compressioni tra i piatti.

forza di serraggio:

$$F_{p,c} = 0.7 \frac{A_{res} f_{ub}}{\gamma_{M7}}$$

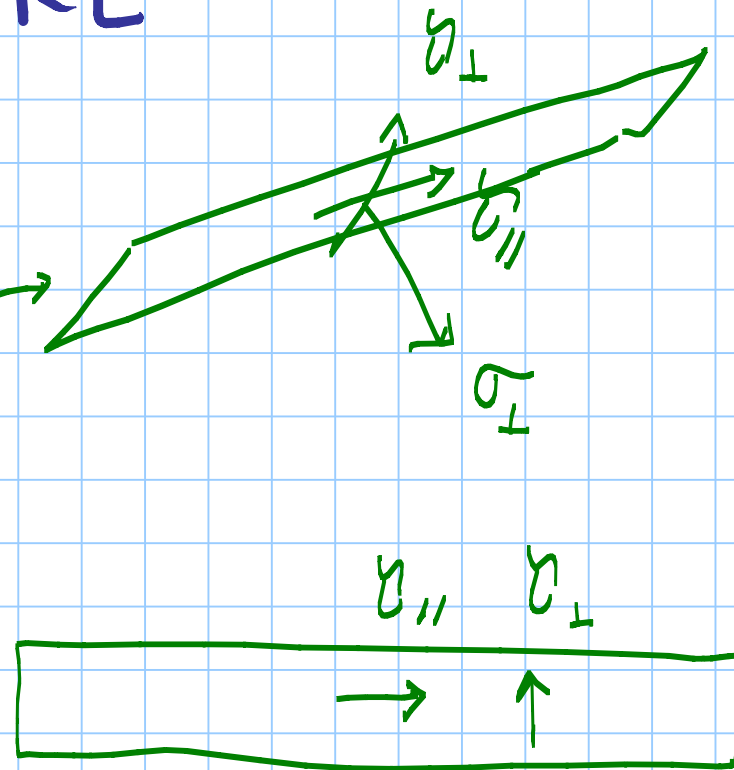
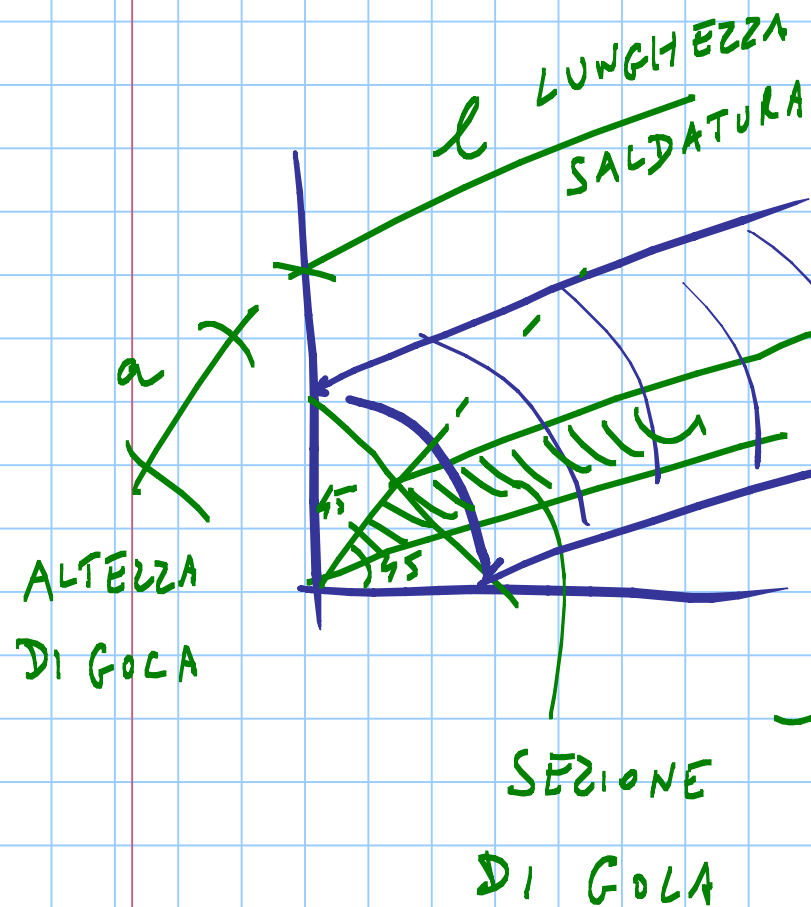
ma $\gamma_{M7} = 1.0$ per serraggio controllato

$$F_{s,RA} = \sqrt[n]{M} \frac{F_{p,c}}{\gamma_{M3}}$$

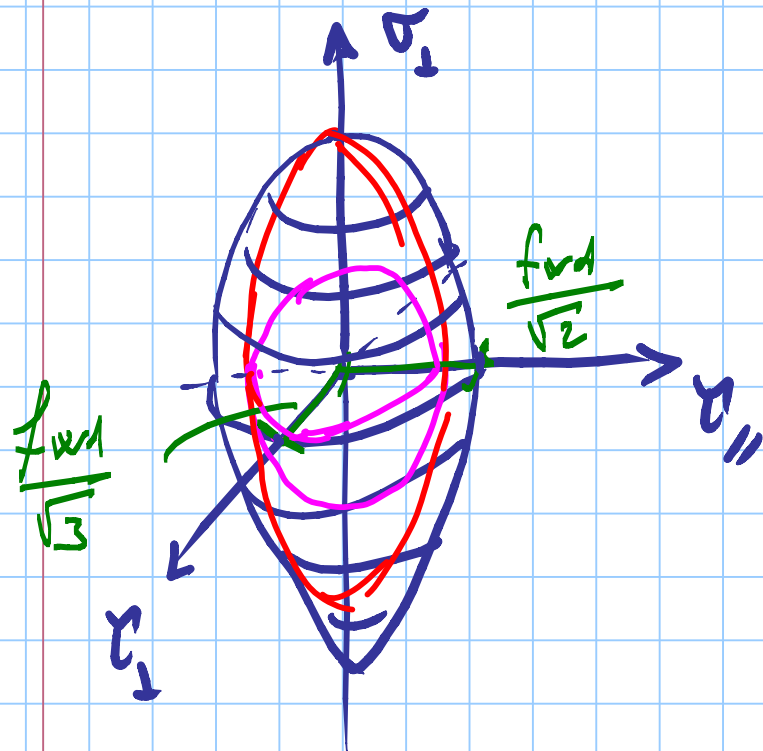
— numero di superfici

$$M = 0.2 \div 0.5$$

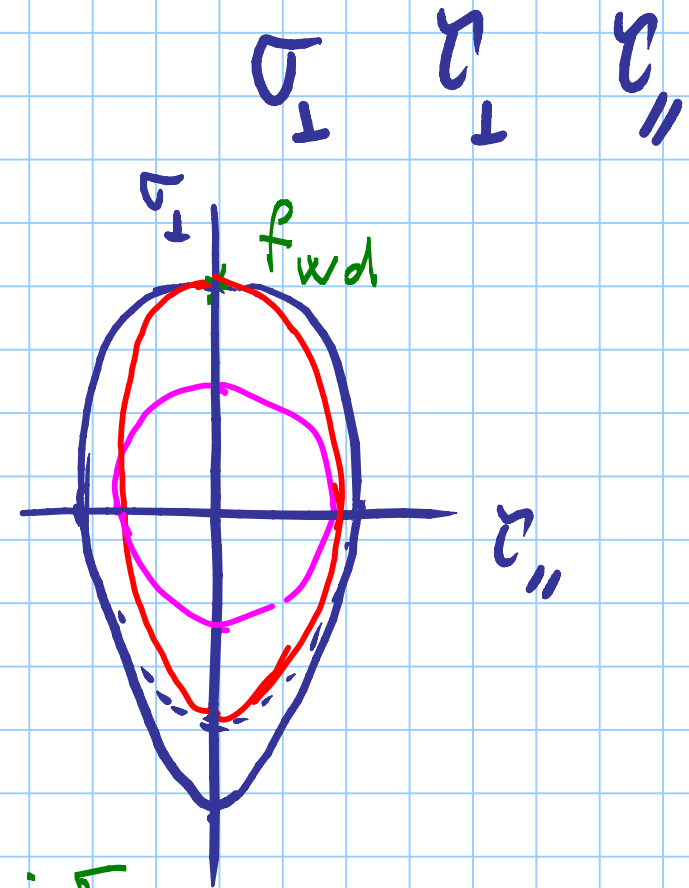
SALDATURE



DOMINIO DI RESISTENZA



PEROIDE



f_{wd} = resistenza
a trazione
della saldatura

perioide \rightarrow ellissoide di rotazione

$$\left(\frac{\sigma_{\perp}}{f_{\text{wd}}} \right)^2 + \left(\frac{\tau_{\parallel}}{f_{\text{wd}}/\sqrt{2}} \right)^2 + \left(\frac{\tau_{\perp}}{f_{\text{wd}}/\sqrt{3}} \right)^2 \leq 1$$

$$\sigma_{\perp}^2 + 2 \tau_{\parallel}^2 + 3 \tau_{\perp}^2 \leq f_{\text{wd}}^2$$

\Downarrow

$$\sigma_{\perp}^2 + 3 (\tau_{\parallel}^2 + \tau_{\perp}^2) \leq f_{\text{wd}}^2$$

①

$$\Downarrow$$

then $3(\sigma_{\perp}^2 + \sigma_{\parallel}^2 + \sigma_{\perp}^2) \leq f_{\text{wd}}^2$

$$\sigma_{\perp}^2 + \sigma_{\parallel}^2 + \sigma_{\perp}^2 \leq \left(\frac{f_{\text{wd}}}{\sqrt{3}}\right)^2 \quad (2)$$