

$$\frac{N_{Ed} \cdot \gamma_{M1}}{\chi_{min} \cdot f_{yk} \cdot A} + \frac{M_{yeq,Ed} \cdot \gamma_{M1}}{f_{yk} \cdot W_y \cdot \left(1 - \frac{N_{Ed}}{N_{cr,y}}\right)} + \frac{M_{zeq,Ed} \cdot \gamma_{M1}}{f_{yk} \cdot W_z \cdot \left(1 - \frac{N_{Ed}}{N_{cr,z}}\right)} \leq 1$$

metod. A
circulor

$$\chi_{min} \frac{f_y A}{\gamma_{m1}} = N_{b,Rd}$$

$$\frac{f_y W_y}{\gamma_{m1}} = M_{y,Rd}$$

$$\gamma_{m1} = \gamma_{m1}$$

$$\frac{N_{Ed}}{N_{b,Rd}} + \frac{M_{y,Ed}}{M_{y,Rd} \left(1 - \frac{N_{Ed}}{N_{cr,y}}\right)} + \frac{M_{z,Ed}}{M_{z,Rd} \left(1 - \frac{N_{Ed}}{N_{cr,z}}\right)} \leq 1$$

esempl. IPE 160 (anche se non molt. buone
per pressiflessione)

S 275

$$A = 20.1 \times 10^2 \text{ mm}^2$$

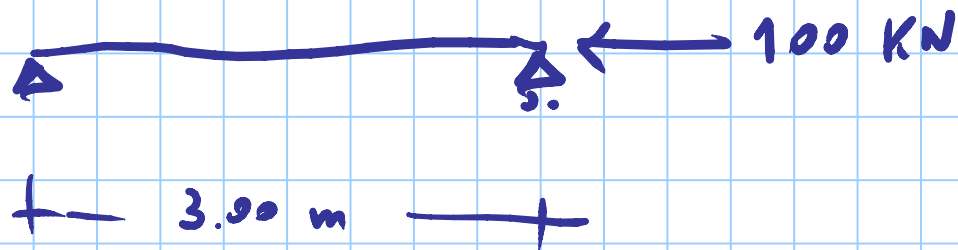
$$W_{pl,y} = 123.9 \times 10^3 \text{ mm}^3$$

$$i_y = 65.8 \text{ mm}$$

$$W_{pl,z} = 26.10 \times 10^3 \text{ mm}^3$$

$$i_z = 18.4 \text{ mm}$$

$$I_y = 869.3 \times 10^4 \text{ mm}^4$$



$$N_{rd} = A \frac{f_y}{\gamma_m} = 20.1 \times 10^2 \times \frac{275}{1.05} = 526.4 \text{ kN}$$

$$M_{y,rd} = W_{pl,y} \frac{f_y}{\gamma_m} = 123.9 \times 10^3 \times \frac{275}{1.05} = 32.45 \text{ kNm}$$

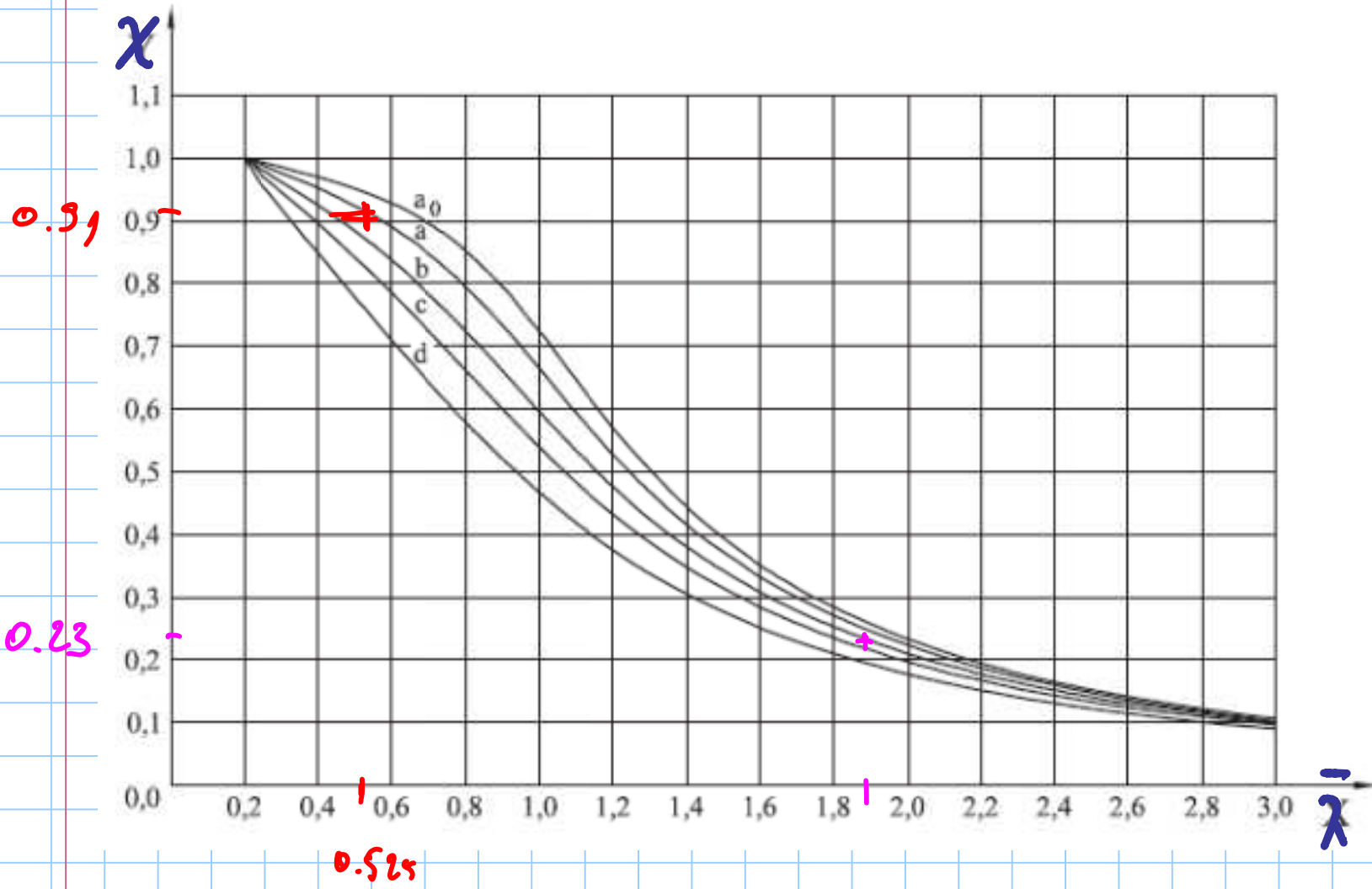
$$M_{z,rd} = W_{pl,z} \frac{f_y}{\gamma_m} = 26.1 \times 10^3 \times \frac{275}{1.05} = 6.84 \text{ kNm}$$

$$\lambda_y = \frac{3000}{65.8} = 45.6$$

$$\lambda_z = \frac{3000}{18.4} = 163.0$$

$$\lambda_1 = \pi \sqrt{\frac{E}{f_y}} = 86.8$$

$$\bar{\lambda} = \bar{\lambda}_z = 1.89 \quad \text{curve b}$$



$$N_{b,Rd} = 0.23 \quad N_{Ed} = 121.1 \text{ kN}$$

Verifica com $N_{Ed} = 100 \text{ kN}$ $M_{y,Ed} = 15 \text{ kNm}$

$$N_{cr,y} = \frac{\pi^2 EI_y}{l_0^2} = \frac{3.14^2 \times 210\,000 \times 869.3 \times 10^4}{3000^2} \times 10^{-3} =$$

$$\approx 2002 \text{ kN}$$

$$\frac{N_{Ed}}{N_{y,Ed}} + \frac{M_{y,Ed}}{M_{y,Ed} \left(1 - \frac{N_{Ed}}{N_{cr,y}} \right)} \leq 1$$

$$\left(\frac{100.0}{121.1} + \frac{15.0}{32.45 \left(1 - \frac{100}{2002} \right)} \right) \leq 1$$

0.826

0.462

0.95

0.486

1.312 $\not\leq$ 1

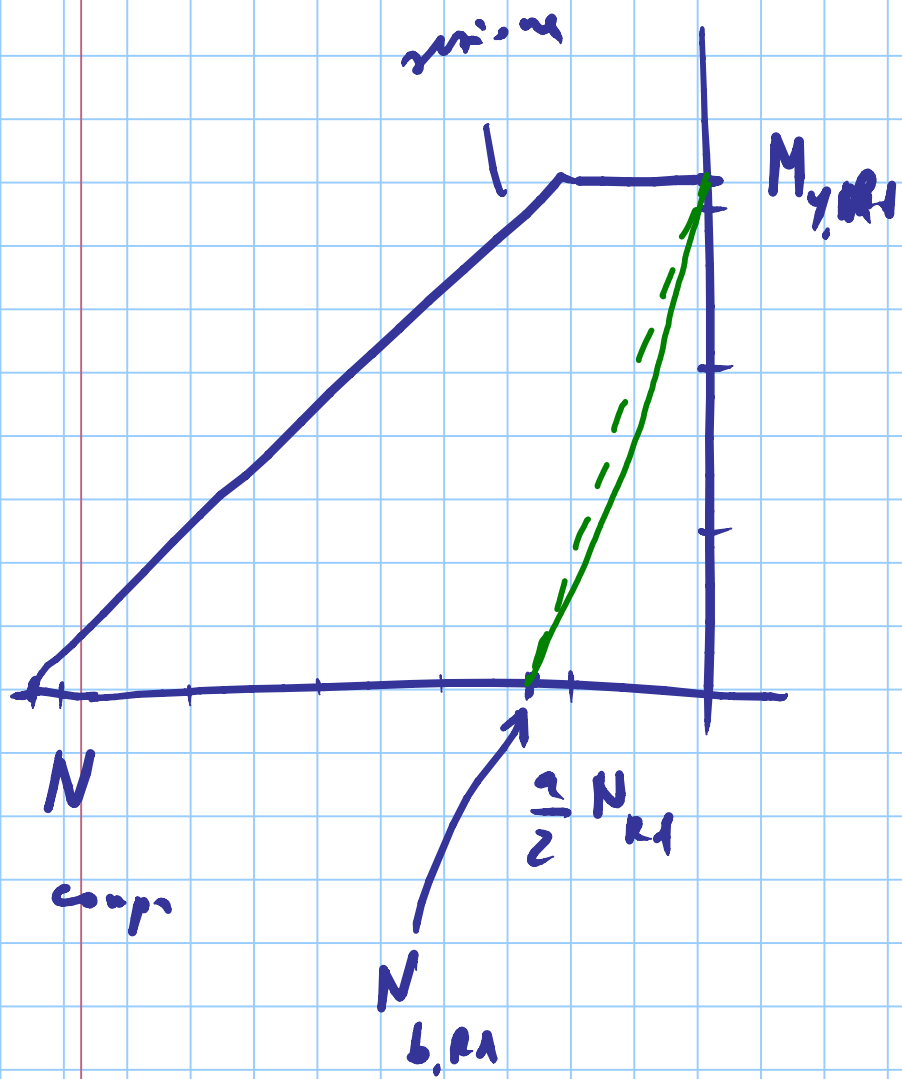
NON VERIFICATA

$$a = \frac{A - 2 b t_f}{A} = \frac{2010 - 2 \times 82 \times 7.4}{2010} = 0.396$$

$$b = 82 \text{ mm}$$

$$t_f = 7.4 \text{ mm}$$

$$A = 20.1 \times 10^2 \text{ mm}^2$$



METODO B

circolare ; EC3

$$\frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} + k_{yy} \cdot \frac{M_{y,Ed} \cdot \gamma_{M1}}{\chi_{LT} \cdot W_y \cdot f_{yk}} + k_{yz} \cdot \frac{M_{z,Ed} \cdot \gamma_{M1}}{W_z \cdot f_{yk}} \leq 1$$

$$\frac{N_{Ed} \cdot \gamma_{M1}}{\chi_z \cdot A \cdot f_{yk}} + k_{zy} \cdot \frac{M_{y,Ed} \cdot \gamma_{M1}}{\chi_{LT} \cdot W_y \cdot f_{yk}} + k_{zz} \cdot \frac{M_{z,Ed} \cdot \gamma_{M1}}{W_z \cdot f_{yk}} \leq 1$$

$$\frac{N_{Ed}}{N_{y,b,Rd}} + k_{yy} \frac{M_{y,Ed}}{M_{y,Rd}} + k_{yz} \frac{M_{z,Ed}}{M_{z,Rd}} \leq 1$$

$$\frac{N_{Ed}}{N_{z,b,Rd}} + k_{zy} \frac{M_{y,Ed}}{M_{y,Rd}} + k_{zz} \frac{M_{z,Ed}}{M_{z,Rd}} \leq 1$$

k	Tipi di sezione	Sezioni di classe 3 e 4 (proprietà delle sezioni calcolate in campo elastico)	(proprietà delle sezioni calcolate in campo plastico)
k_{yy}	I, H, Sezioni cave	$\alpha_{my} \cdot \left(1 + 0,6 \cdot \bar{\lambda}_y \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{my} \cdot \left(1 + 0,6 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$	$\alpha_{my} \cdot \left(1 + (\bar{\lambda}_y - 0,2) \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{my} \cdot \left(1 + 0,8 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$
k_{yz}	I, H, Sezioni cave	k_{zz}	$0,6 \cdot k_{zz}$
k_{zy}	I, H, Sezioni cave	$0,8 \cdot k_{yy}$	$0,6 \cdot k_{yy}$
k_{zz}	I, H	$\alpha_{mz} \cdot \left(1 + 0,6 \cdot \bar{\lambda}_y \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{mz} \cdot \left(1 + 0,6 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$	$\alpha_{mz} \cdot \left(1 + (2\bar{\lambda}_y - 0,6) \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{mz} \cdot \left(1 + 1,4 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$
	Sezioni cave		$\alpha_{mz} \cdot \left(1 + (\bar{\lambda}_y - 0,2) \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{mz} \cdot \left(1 + 0,8 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$
Per pressoflessione retta, $M_{y,Ed} \neq 0$, $k_{zy} = 0$ ($M_{z,Ed} = 0$).			

consideriamo $M_{z,Ed} = 0 \Rightarrow k_{zy} = 0$

$$\frac{N_{Ed}}{N_{y,b,Rd}} + K_{yy} \frac{M_{y,Ed}}{M_{y,Rd}} \leq 1$$

$$\frac{N_{Ed}}{N_{z,b,Rd}} \leq 1$$

$$K_{yy} = \alpha_{my} \cdot \left(1 + (\bar{\lambda}_y - 0,2) \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right) \leq \alpha_{my} \cdot \left(1 + 0,8 \cdot \frac{N_{Ed} \cdot \gamma_{M1}}{\chi_y \cdot A \cdot f_{yk}} \right)$$

↓
1 x M = const

$$K_{yy} = 1 + (\tilde{\lambda}_y - 0.2) \frac{N_{Ed}}{N_{y,b,Rd}}$$

ma non maggiore di

$$1 + 0.8 \frac{N_{Ed}}{N_{y,b,Rd}}$$

Nell'esempi. di prima

$$\lambda_y = 45.6 \quad \bar{\lambda}_y = 0.525 \quad \chi_y = 0.91$$

$$N_{y,b,Rd} = 0.91 \times 526.4 = 479.0 \text{ kN}$$

$$N_{z,b,Rd} = 121.1 \text{ kN}$$

$$K_{yy} = 1 + (\bar{\lambda}_y - 0.2) \frac{N_{Ed}}{N_{y,b,Rd}} = 1 + (0.525 - 0.2) \frac{1000}{479.0} = 1.068$$

Verifica

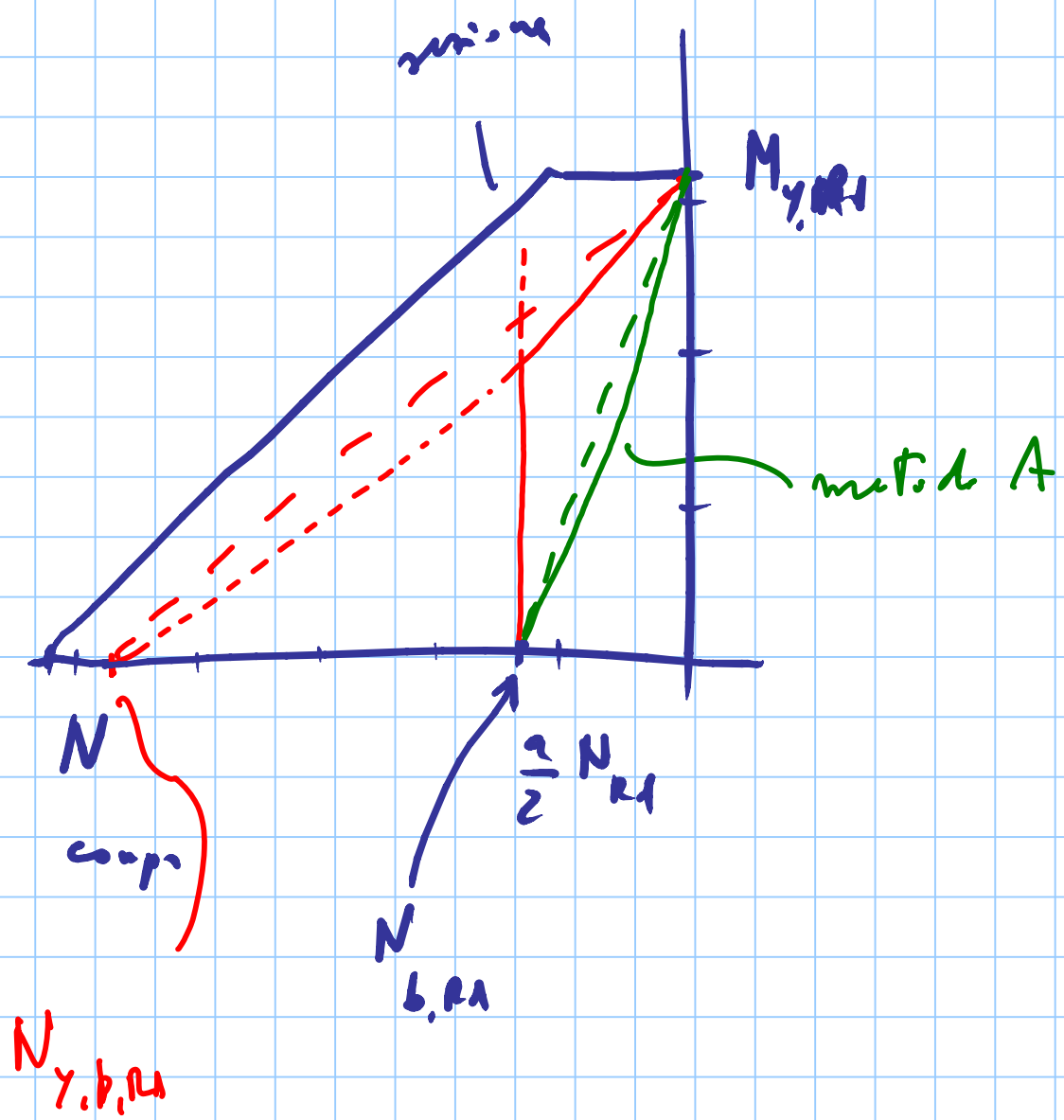
$$\frac{N_{Ed}}{N_{y,b,Rd}} + K_{yy} \frac{M_{y,Ed}}{M_{y,Rd}} \leq 1 \Rightarrow \frac{100.0}{479.0} + 1.07 \frac{15}{32.45} \leq 1$$

0.209 0.462

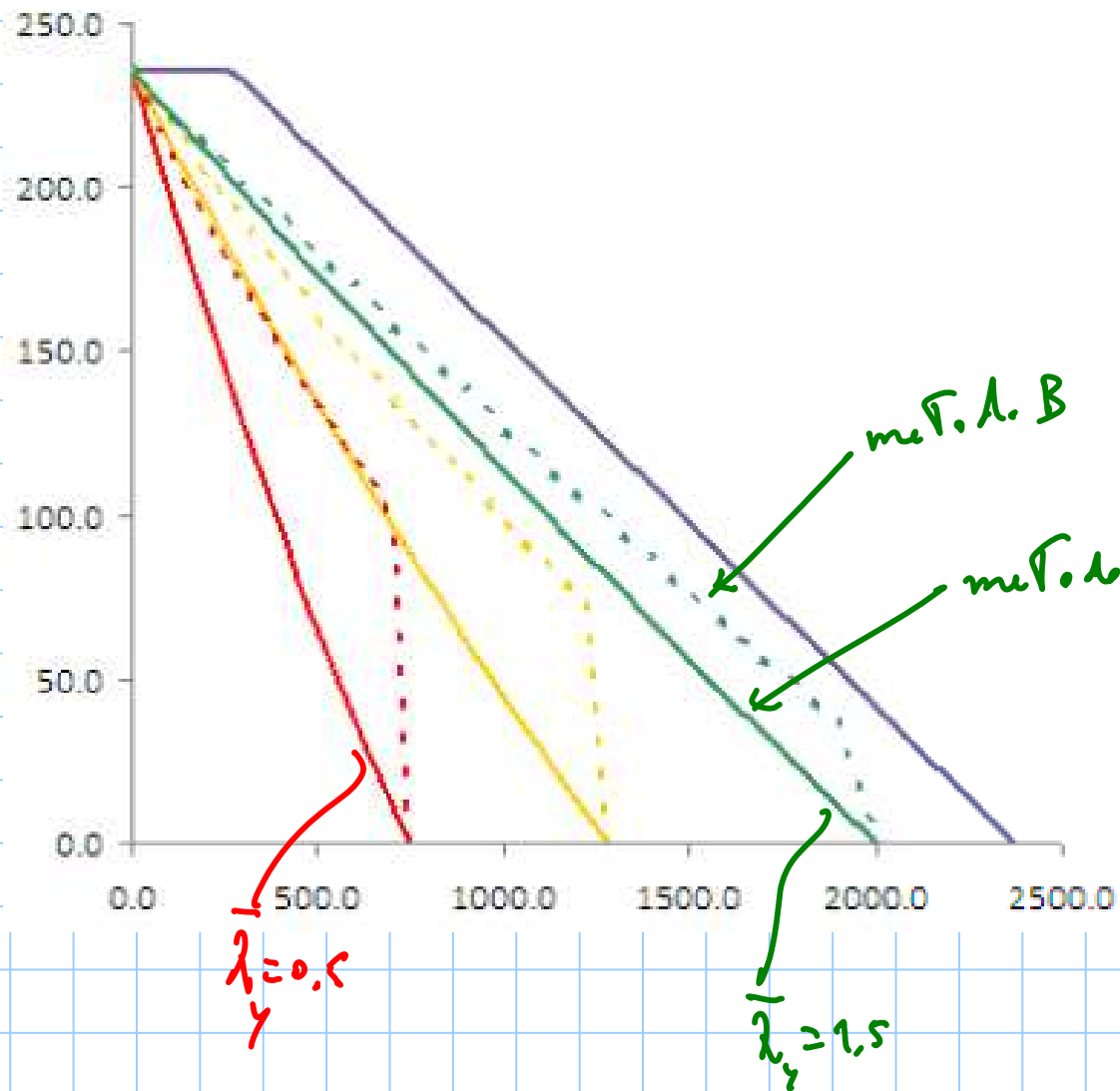
0.475 ok

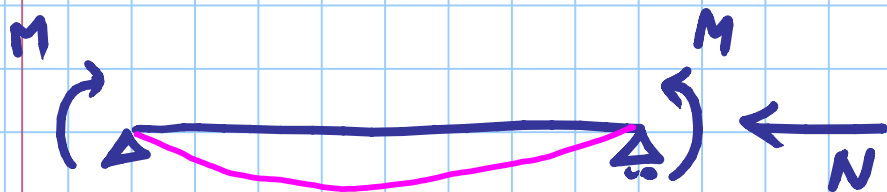
$$\frac{N_{Ed}}{N_{z,b,Rd}} \leq 1$$

$$\frac{100.0}{121.1} \leq 1$$

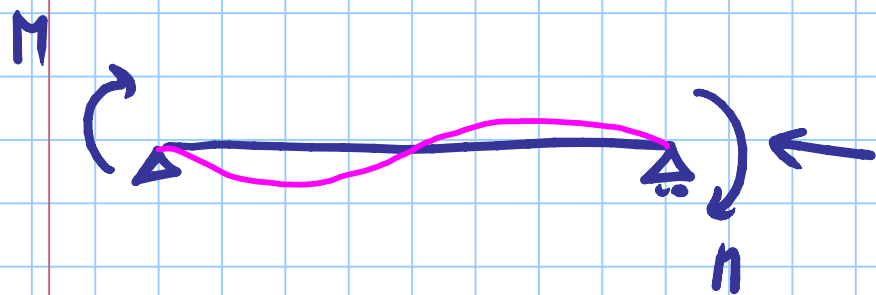
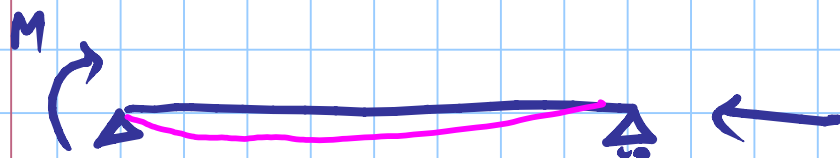


HE B 240





la deformation s'oppose
à l'instabilité



la deformation aide

METODO A

$$M_{eq,Ed} = 0,6 \cdot M_a - 0,4 \cdot M_b \geq 0,4 \cdot M_a$$



$$|M_a| > |M_b|$$

$$M_b = -M_a$$



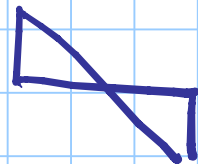
$$M_y = M_a$$

$$M_b = 0$$



$$M_y = 0,6 M_a$$

$$M_b = M_a$$



$$M_y = 0,4 M_a$$

$$\frac{N_{Ed}}{N_{b,Rd}} + \frac{M_{eq,\gamma,Ed}}{M_{\gamma,Rd} \left(1 - \frac{N_{Ed}}{N_{u,\gamma}}\right)} \leq 1$$

$$M_{eq,\gamma,Ed} = \text{coeff.} \cdot M_{Ed}$$

