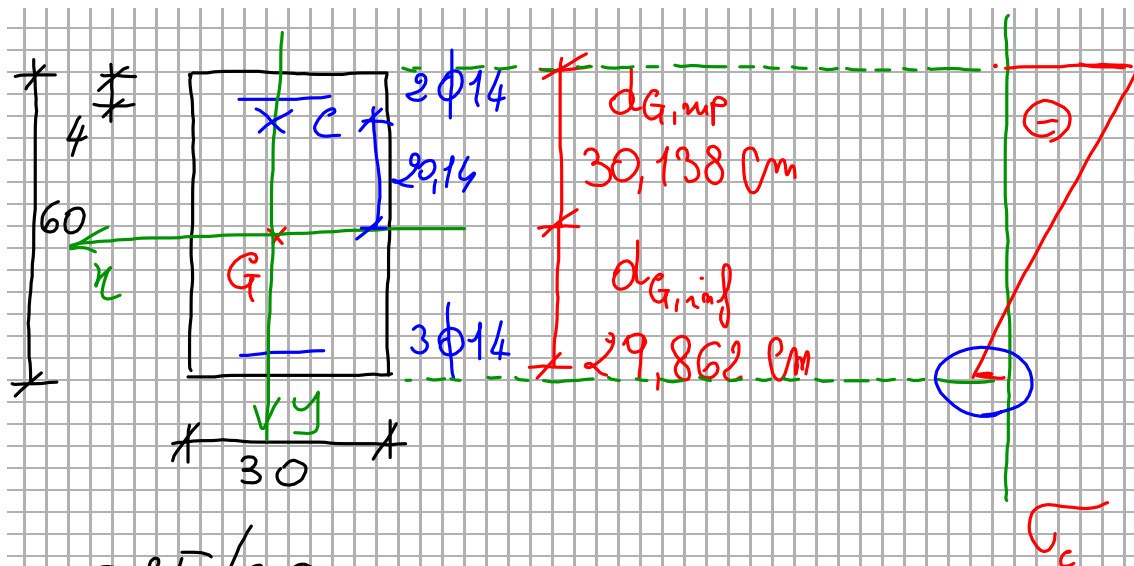


C25/30



C25/30

$m = 6,35$

$$\sigma = \frac{N}{A} + \frac{N e_G}{I_x} d_{G,inf}$$

Tensione di trazione
del CLS

$$e_G = \frac{M}{N} - \left(\frac{h}{2} - d_{G,inf} \right) = \frac{100}{-500} - (0,3 - 0,2986)$$

$$= -0,2014 \text{ m} = -20,14 \text{ cm}$$

$$A = 30 \times 60 + 6,35 \times (3,08 + 4,62) = 1848,9 \text{ cm}^2$$

$$\sigma_s = n \left[\frac{N}{A} + \frac{N e_G}{I_x} (d_{G,inf} - c) \right]$$

$$e_G = \frac{M}{N} - \left(\frac{h}{2} - d_{G,inf} \right) = \frac{100}{-500} - (0,3 - 0,2986)$$

$$= -0,2014 \text{ m} = -20,14 \text{ cm}$$

$$A = 30 \times 60 + 6,35 \times (3,08 + 4,62) = 1848,9 \text{ cm}^2$$

Tensione in A_s

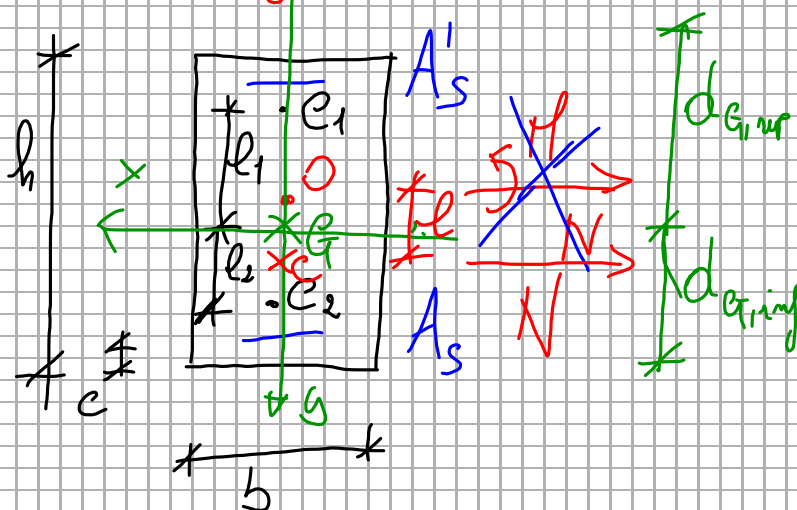
$$I_x = \frac{30 \times 30,14^3}{3} + \frac{30 \times 29,86^3}{3} + 6,35 \times 3,08 \times 26,14^2 + 6,35 \times 4,62 \times 25,86^2 = 573018 \text{ cm}^4$$

$$\sigma_{ef} = \frac{-500}{1848,9} \times 10 + \frac{+500 \times +29,14}{573018} \times 29,86 \times 10$$

$$= 2,54 \text{ MPa} \leq f_{efk} \quad \text{NO}$$

$$C.25/30 \quad f_{efk} = 2,16 \text{ MPa}$$

Tenso-flessione - piccola eccentricita-



$$e_1 = \frac{I_x}{A d_{gring}}$$

$$e_2 = \frac{I_x}{A d_{gring}}$$

$$e = \frac{M}{N}$$

$$-l_1 < l_s < l_2$$

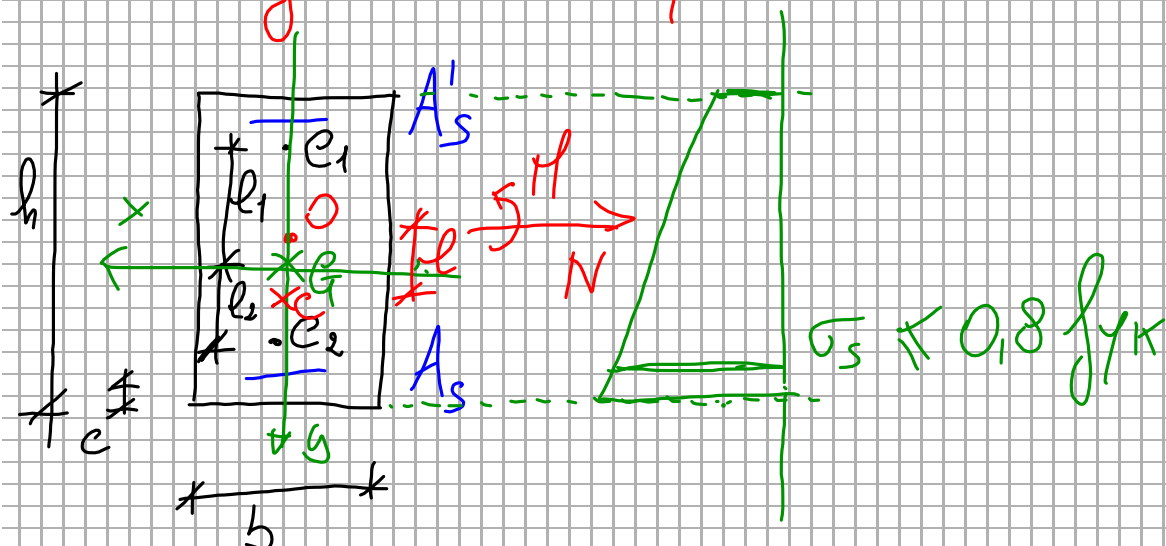
$$l_s = \frac{M}{N} - \left(\frac{h}{2} - d_{gring} \right)$$

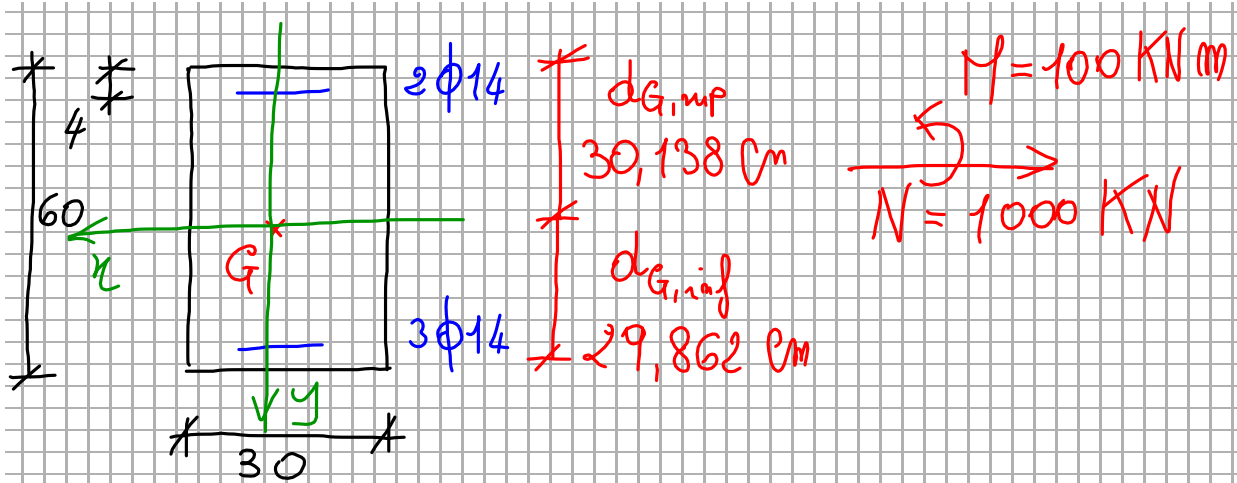
$$\sigma = \frac{N}{A} + \frac{N e_s}{I_x} y$$

solo acciaio

$$\sigma_s = \frac{N}{A} + \frac{N e_s}{I_x} (d_{gring} - e)$$

Tenso-flessione - piccola eccentricità

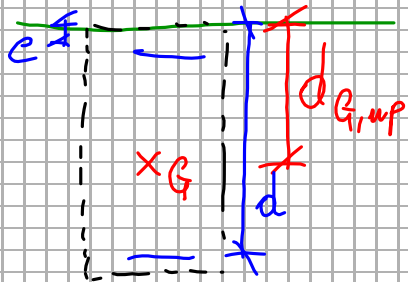




C25/30

$$I_1 = \frac{I_x}{A d_{G,inf}}$$

$$d_{G,inf} = 60 - 35,2 = 24,8 \text{ cm}$$



$$d_{G,up} = \frac{S_0}{A} = \frac{271,04}{7,7} = 35,2 \text{ cm}$$

$$A = 3,08 + 4,62 = 7,7 \text{ cm}^2$$

$$S_0 = 3,08 \times 4 + 4,62 \times 56 = 271,04 \text{ cm}^3$$

$$\begin{aligned}
 I_x &= A_s (d_{\text{ging}} - e)^2 + A'_s (d_{\text{grup}} - e)^2 \\
 &= 4,62 \times (24,8 - 4)^2 + 3,08 \times (35,2 - 4)^2 \\
 &= 4997 \text{ cm}^4
 \end{aligned}$$

$$e_1 = \frac{I_x}{A d_{\text{ging}}} = 26,2 \text{ cm}$$

$$e_2 = \frac{I_x}{A d_{\text{grup}}} = \frac{4997}{7,7 \times 35,2} = 18,4 \text{ cm}$$

$$\begin{aligned}
 e_s &= \frac{M}{N} - \left(\frac{h}{2} - d_{\text{ging}} \right) = \frac{100}{1000} - (0,3 - 0,248) \\
 &= 0,048 \text{ m} = 4,8 \text{ cm}
 \end{aligned}$$

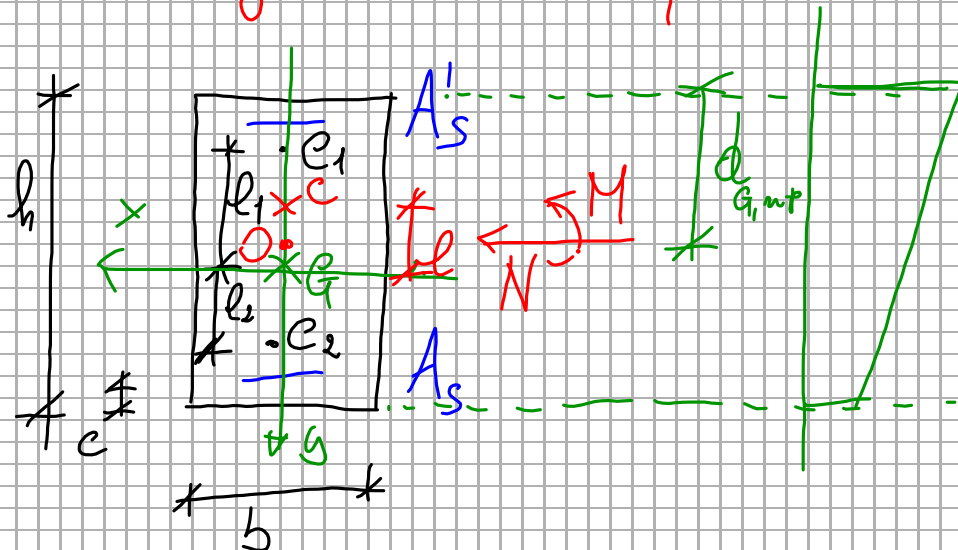
$$\sigma_s = \frac{N}{A} + \frac{N e_s (d_{gring} - c)}{I_x}$$

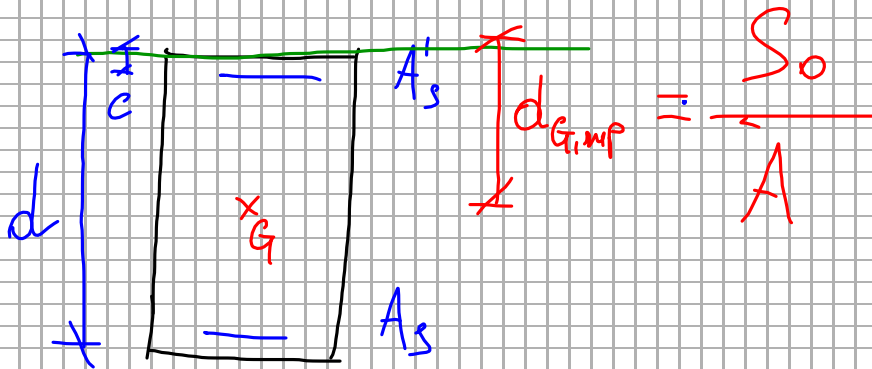
$$= \left[\frac{1000}{7,7} + \frac{1000 \times 4,8}{4997} \times (24,8 - 4) \right] \times 10$$

$$= 1498 \text{ MPa} \leq 0,8 f_{yk} = 360 \text{ MPa}$$

B450C NO

Presso-flessione - piccola eccentricità





$$S_0 = \frac{b h^3}{12} + m A'_s c^2 + m A_s d^2$$

$$A = b h + m (A'_s + A_s)$$

$$e_1 = \frac{I_x}{A d_{G,mp}}$$

$$e_2 = \frac{I_x}{A d_{G,mp}}$$

$$I_x = \frac{b d_{G,mp}^3}{3} + \frac{b d_{G,mp}^3}{3} + m A'_s (d_{G,mp} - c)^2 + m A_s (d_{G,mp} - c)^2$$

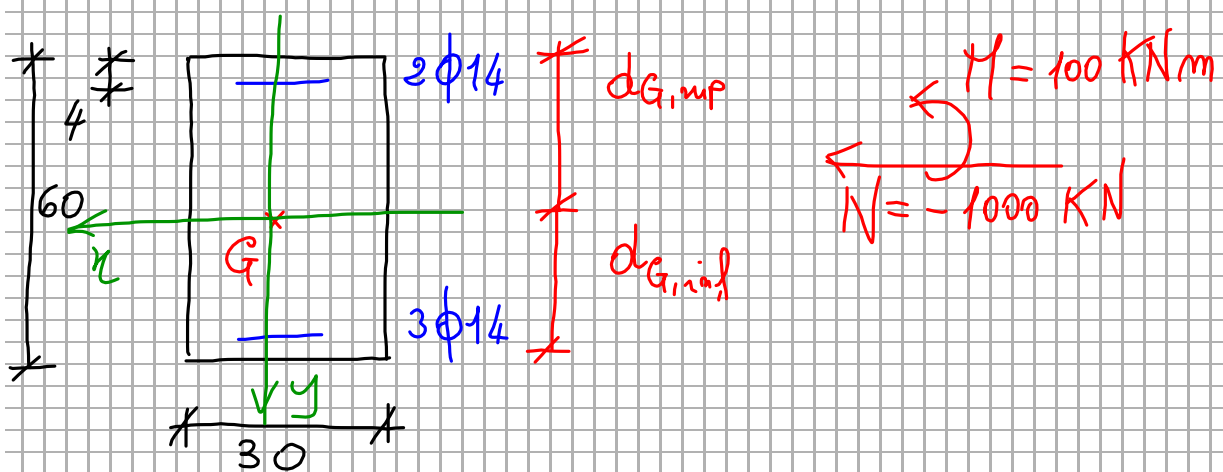
$$e_{cts} = \frac{M}{N} - \left(\frac{h}{2} - d_{G,mp} \right)$$

$$-e_1 \leq e_{cts} \leq e_2$$

piccola
eccentricità

$$\sigma = \frac{N}{A} + \frac{N e_{cs}}{I_x} y$$

$$\sigma_c = \frac{N}{A} - \frac{N e_{cs}}{I_x} d_{G,mp}$$



$$M = 100 \text{ kNm}$$

$$N = -1000 \text{ kN}$$

C25/30

$m = 15$

$$S_0 = \frac{30 \times 60^2}{2} + 15 \times 3,08 \times 4 + 15 \times 4,62 \times 56 =$$

$$= 58065,6 \text{ cm}^3$$

$$A = 30 \times 60 + 15 \times (3,08 + 4,62) = 1915,5 \text{ cm}^2$$

$$d_{g, nr} = \frac{58065,6}{1915,5} = 30,3 \text{ cm}$$

$$d_{g, inf} = 60 - 30,3 = 29,7 \text{ cm}$$

$$I_x = \frac{30 \times 30,3^3}{3} + \frac{30 \times 29,7^3}{3} + 15 \times 3,08 \times 26,3^2 + 15 \times 4,62 \times 25,7^2$$

$$= 617890 \text{ cm}^4$$

$$e_1 = \frac{617890}{1915,5 \times 29,7} = 10,86 \text{ cm}$$

$$e_2 = \frac{617890}{1915,5 \times 30,3} = 10,65 \text{ cm}$$

$$e_{cs} = \frac{100}{-1000} - (0,3 - 0,297) = -10,31 \text{ cm}$$

$$\sigma_c = \left[\frac{-1000}{1915,5} - \frac{+1000 \times +1031}{617890} \times 30,3 \right] \times 10 = -10,3 \text{ MPa}$$

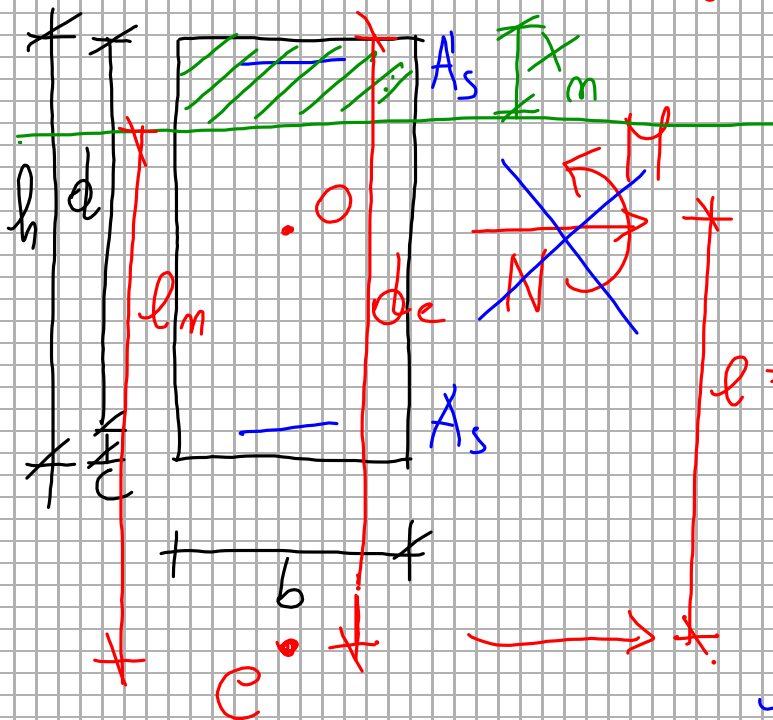
Conf. core

$$|\sigma_c| \leq 0,6 f_{ck} = 0,6 \times 25 = 15 \text{ MPa}$$

c25/30

OK!

Flessione composta - grande eccentricità



$$l_m = \frac{I_m}{S_m}$$

$$e = \frac{M}{N}$$

$$d_e = \frac{M}{N} + \frac{h}{2}$$

$$l_m = d_e - x$$

$$S_m = \frac{bX^2}{2} - mA'_s(X-c) + mA_s(d-x)$$

$$I_m = \frac{bX^3}{3} + mA'_s(X-c)^2 + mA_s(d-x)^2$$

$$\begin{aligned} & \frac{bX^3}{3} + \cancel{mA'_sX^2} + mA'_s e^2 - 2 \cancel{mA'_s cX} + mA_s d^2 + \cancel{mA_s X^2} + \\ & - 2 \cancel{mA_s dX} = - \frac{bX^2}{2} dc - \cancel{mA'_s d c X} + mA'_s c d c + \\ & + mA_s d d c - \cancel{mA_s d c X} + \frac{bX^3}{2} + \cancel{mA'_s X^2} - \cancel{mA'_s c X} \\ & - \cancel{mA_s d X} + \cancel{mA_s X^2} \end{aligned}$$

$$\frac{bX^3}{6} - \frac{bdcX^2}{2} + m[A'_s(c-dc) + A_s(d-dc)]X$$

$$-m[A'_s(c-dc)e + A_s(d-dc)d] = 0$$

$$\boxed{\begin{aligned} & X^3 - 3dcX^2 + \frac{6m}{b}[A'_s(c-dc) + A_s(d-dc)]X + \\ & - \frac{6m}{b}[A'_s(c-dc)e + A_s(d-dc)d] = 0 \end{aligned}}$$

$$\sigma = \frac{N}{S_m}$$

$$\sigma_c = -\frac{N}{S_m} X$$

$$\sigma_s = m \frac{N}{S_m} (d - x)$$

