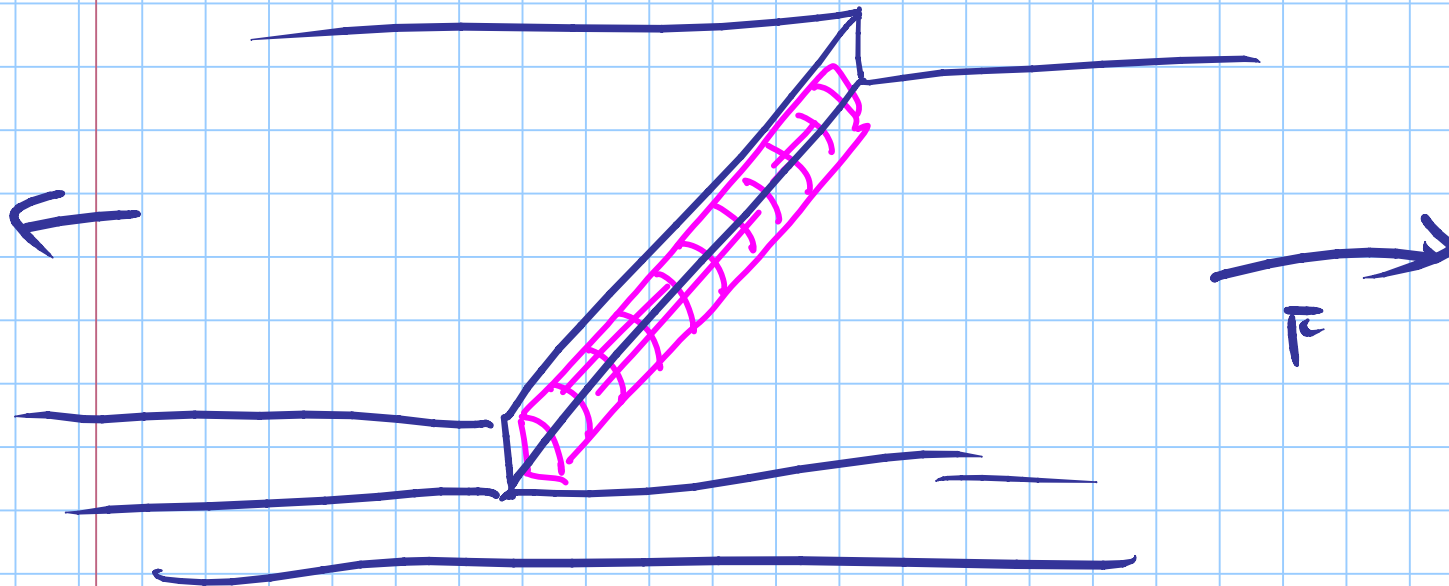
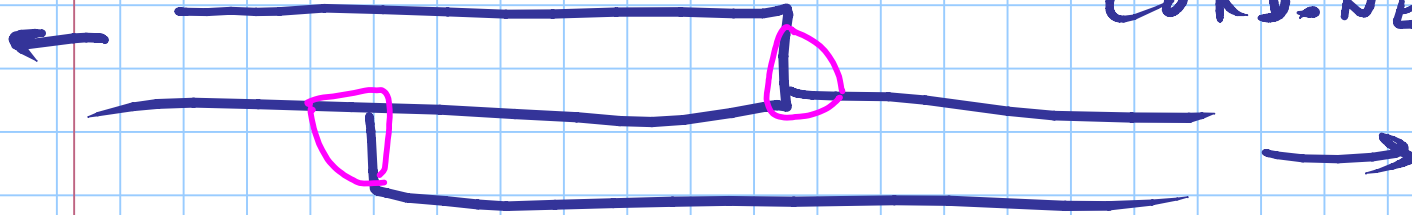


CIA NFR IN

SALDATURA A

COMPLETA PENETRAZIONE

SALDATURA A CORDENE D'ANGOLO



$$\sigma_t = \frac{F}{a l \sqrt{2}}$$

$$\sigma_s = \frac{F}{a l \sqrt{2}}$$

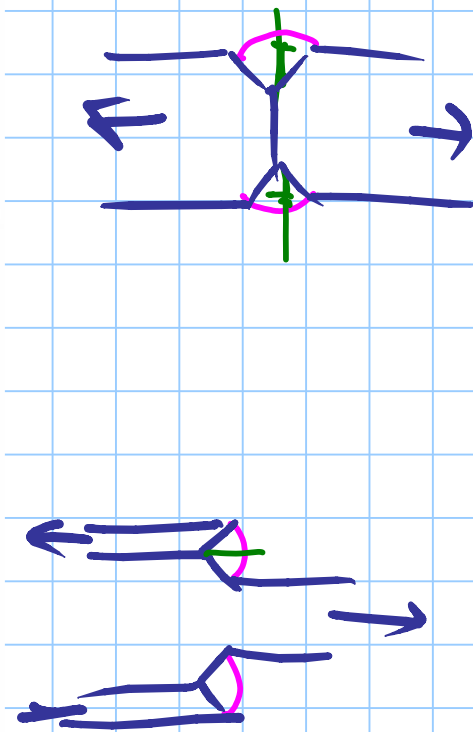
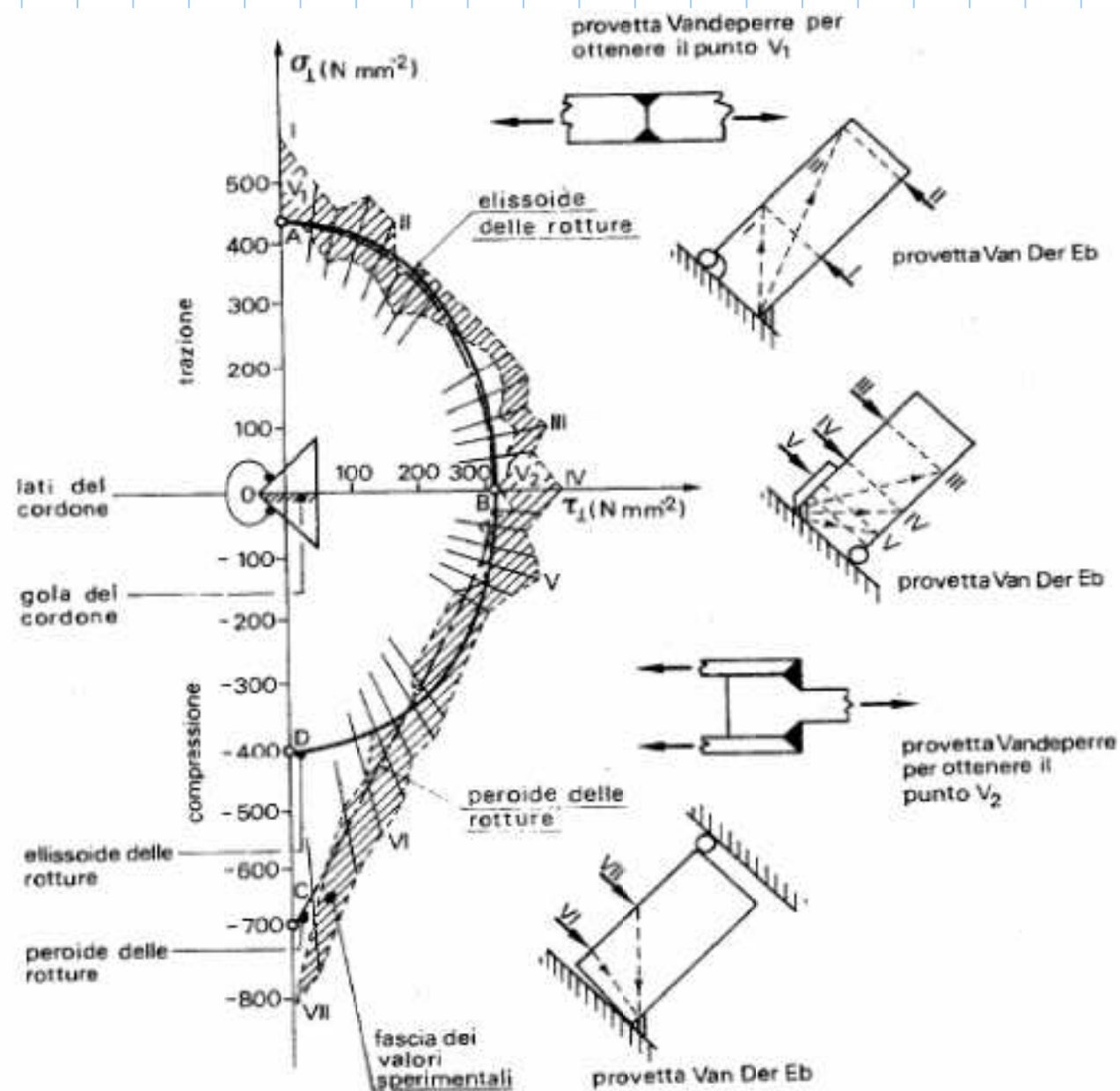
$$\sigma_{\parallel} = 0$$

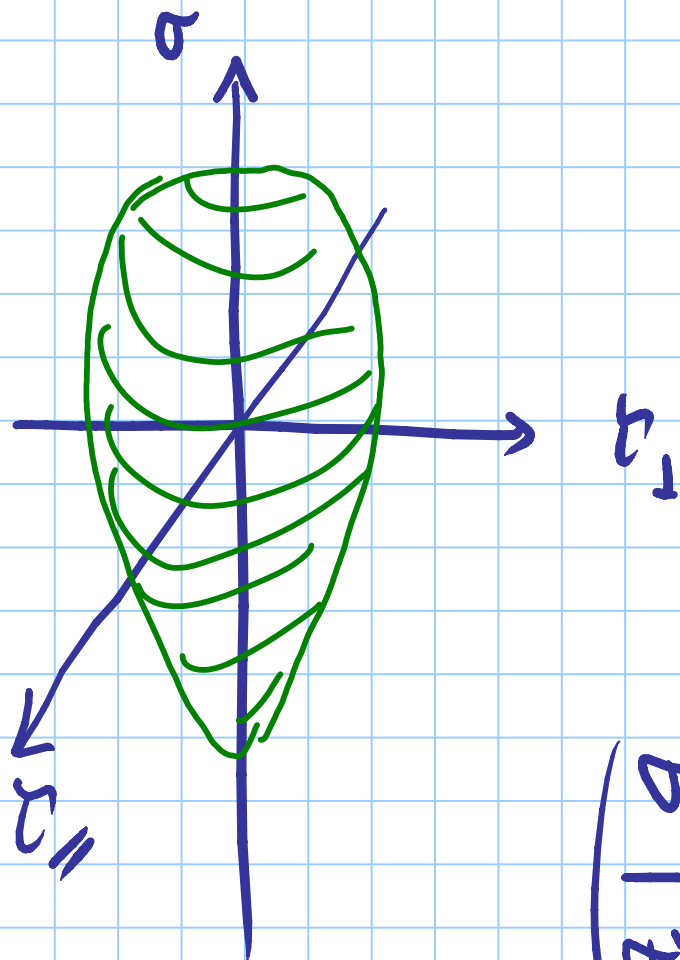
$$\begin{matrix} \gamma & \tau \\ \sigma & \tau \end{matrix}$$

$a =$ altezza di gola

lunghezza delle saldature

SEZIONE axl
DI GOLLA





PEROIDE



ELLISSOIDE

$$\left(\frac{a_1}{a_{max}} \right)^2 + \left(\frac{b_1}{b_{max}} \right)^2 + \left(\frac{b_2}{b_{max}} \right)^2 = 1$$

$a_1^{max} = f_{wd} = \text{resistenza (a trazione) delle saldature}$

$$\sigma_{\perp}^{\max} < f_{wd}$$

$$\downarrow \frac{f_{wd}}{\sqrt{3}}$$

$$\sigma_{//}^{\max} < f_{wd}$$

$$\downarrow \frac{f_{wd}}{\sqrt{2}}$$

$w \rightarrow$ welding (coldature)

$$\sigma_{\perp}^2 + 3 \tau_{\perp}^2 + 2 \tau_{//}^2 = f_{wd}^2$$

\Downarrow

ellissoide di rotazione

$$\sigma_{\perp}^2 + 3 \tau_{\perp}^2 + 3 \tau_{//}^2 = f_{wd}^2$$

$$\sqrt{\sigma_L^2 + 3(\tau_L^2 + \tau_{II}^2)} \leq f_{wd} \quad \text{verifica di resistenza}$$

sfera di vario reggio (Germania, Gran Bretagna)

sfera notte (Italia)



sfera di reggio. $\frac{f_{wd}}{\sqrt{3}} \Rightarrow \sqrt{\sigma_L^2 + \tau_L^2 + \tau_{II}^2} \leq \frac{f_{wd}}{\sqrt{3}}$

$$f_{wd} = \frac{f_u}{\beta_w \gamma_{M2}}$$

$$f_{vwd} = \frac{f_{wd}}{\sqrt{3}} = \frac{f_u}{\beta_w \sqrt{3} \gamma_{M2}}$$

$$\beta_w = 0.80$$

$$1/\beta_w = 1.25$$

S235

$$0.85$$

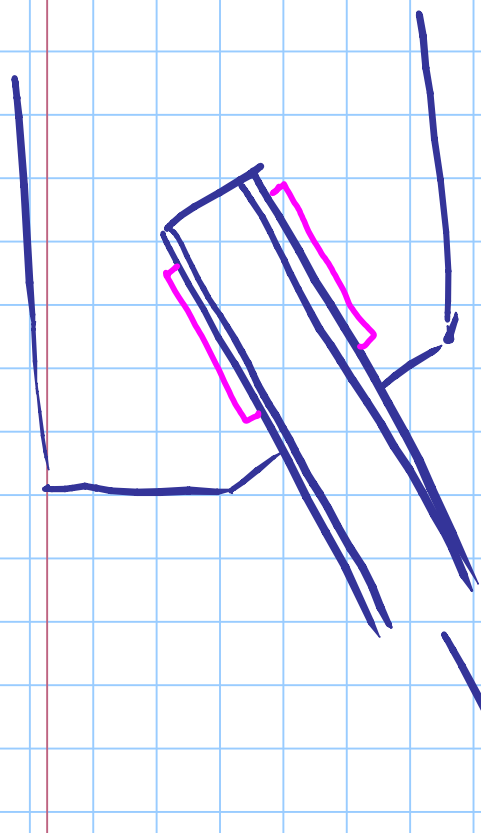
$$1.176$$

S275

$$0.90$$

$$1.111$$

S355



4 cordoni

UPN

$$A = 13.50 \times 10^2 \text{ mm}^2$$

2 UPN

$$N_{Rd} = 707 \text{ kN}$$

$$f_{wd} = 406.7 \text{ MPa}$$

2 UPN 100
S275

$$F_d = 300 \text{ kN}$$

$$f_{vwd} = \frac{430}{0.85 \times \sqrt{3} \times 1.25} = 233.7 \text{ MPa}$$

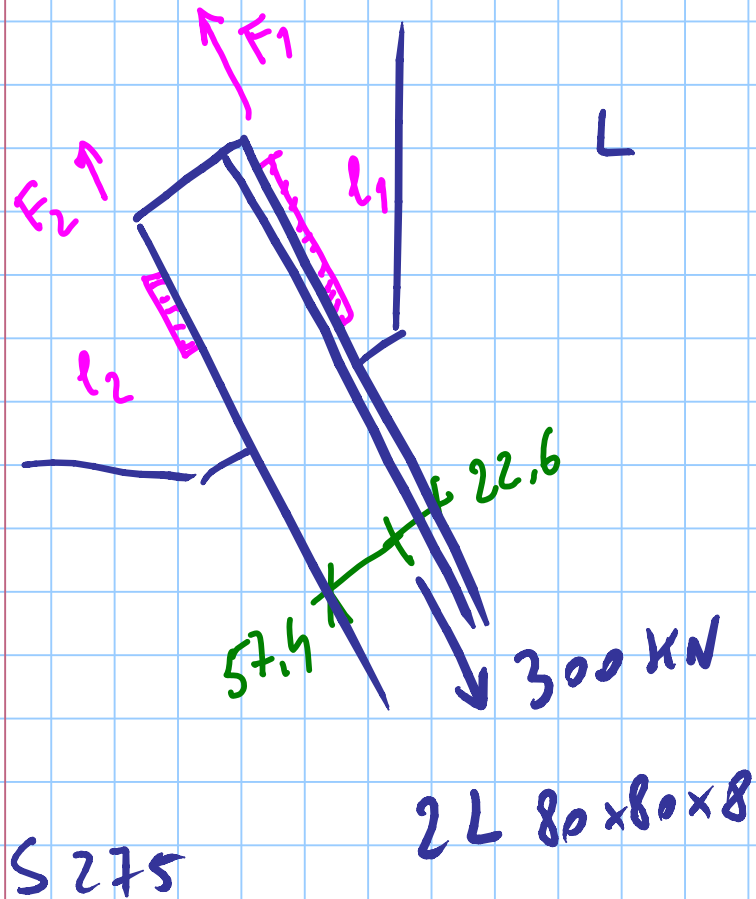
$$\frac{F_d}{4 a l} \leq f_{vwd}$$

$$a l \geq \frac{F_d}{4 f_{vwd}} :$$

$$a = 6 \text{ mm}$$

$$l \geq \frac{321}{6} : 54 \text{ mm}$$

$$= \frac{300 \times 10^3}{4 \times 233.7} : 321 \text{ mm}^2$$



$$L \quad A = 12.3 \times 10^2 \text{ mm}^2$$

$$2 a (l_1 + l_2) f_{vwd} \geq F_1$$

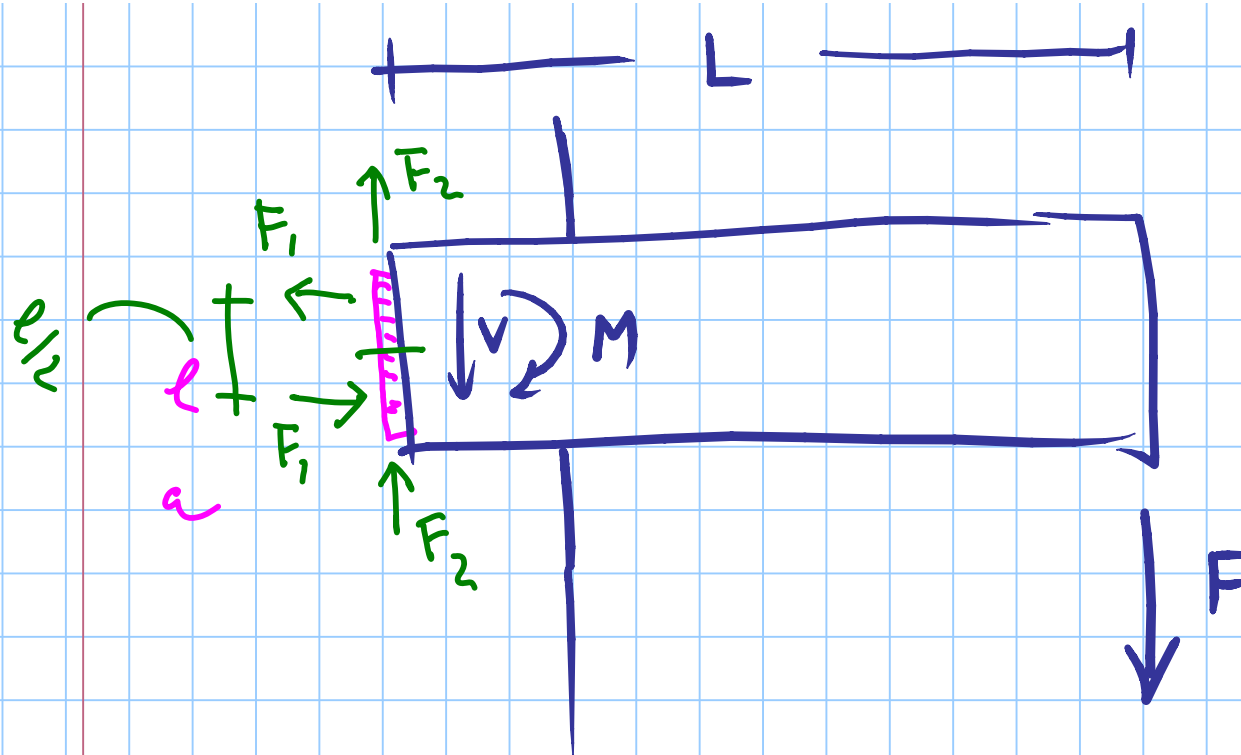
$$\frac{F_1}{57.4} = \frac{F_2}{22.6}$$

$$F_1 = \frac{57.4}{57.4 + 22.6} (F_1 + F_2)$$

$$l_1 + l_2 = \frac{Fd}{2a f_{rad}} = \frac{300 \times 10^3}{2 \times 6 \times 233.7} = 107 \text{ nm}$$

$$l_1 = \frac{57.6}{80} \times 107 = 77 \text{ nm}$$

$$l_2 = 30 \text{ nm}$$

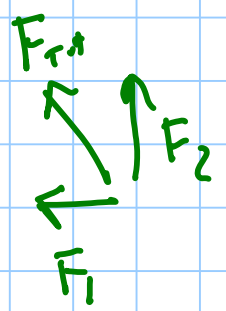


$$V = F$$

$$M = FL$$

$$F_1 = \frac{M}{l/2}$$

$$F_2 = \frac{V}{2}$$



$$F_{T.r} = \sqrt{F_1^2 + F_2^2}$$

crit. di resistenza SFERA

$$\frac{F_{TOT}}{a l / 2} \leq f_{vwd}$$

$$\frac{\sqrt{\left(\frac{M}{l/2}\right)^2 + \left(\frac{V}{2}\right)^2}}{a l / 2} \leq f_{vwd}$$

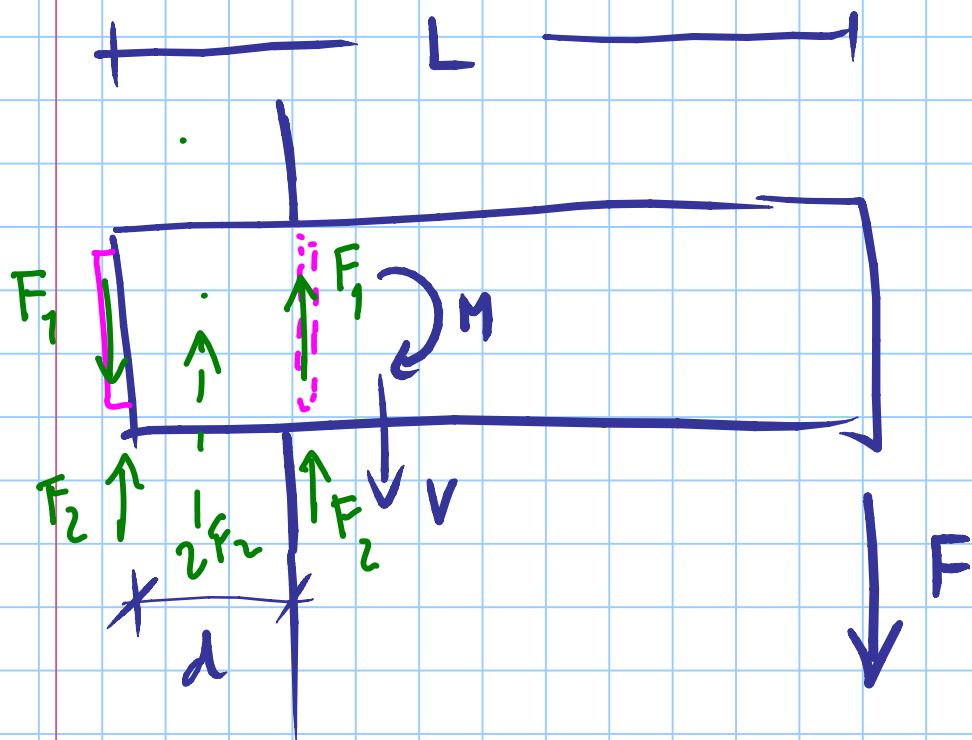
$$\left(\frac{M}{l/2}\right)^2 + \left(\frac{V}{2}\right)^2 \leq \left(f_{vwd} \frac{a l}{2}\right)^2$$

$$\frac{4M^2}{\ell^2} + \frac{v^2}{4} \leq f_{vwd}^2 \frac{a^2 \ell^2}{4}$$

$$4M^2 + \frac{v^2}{4} \ell^2 \leq \frac{f_{vwd}^2}{4} a^2 \ell^4$$

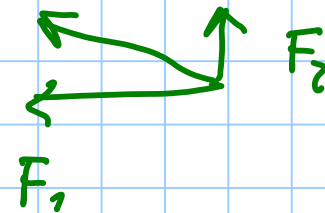
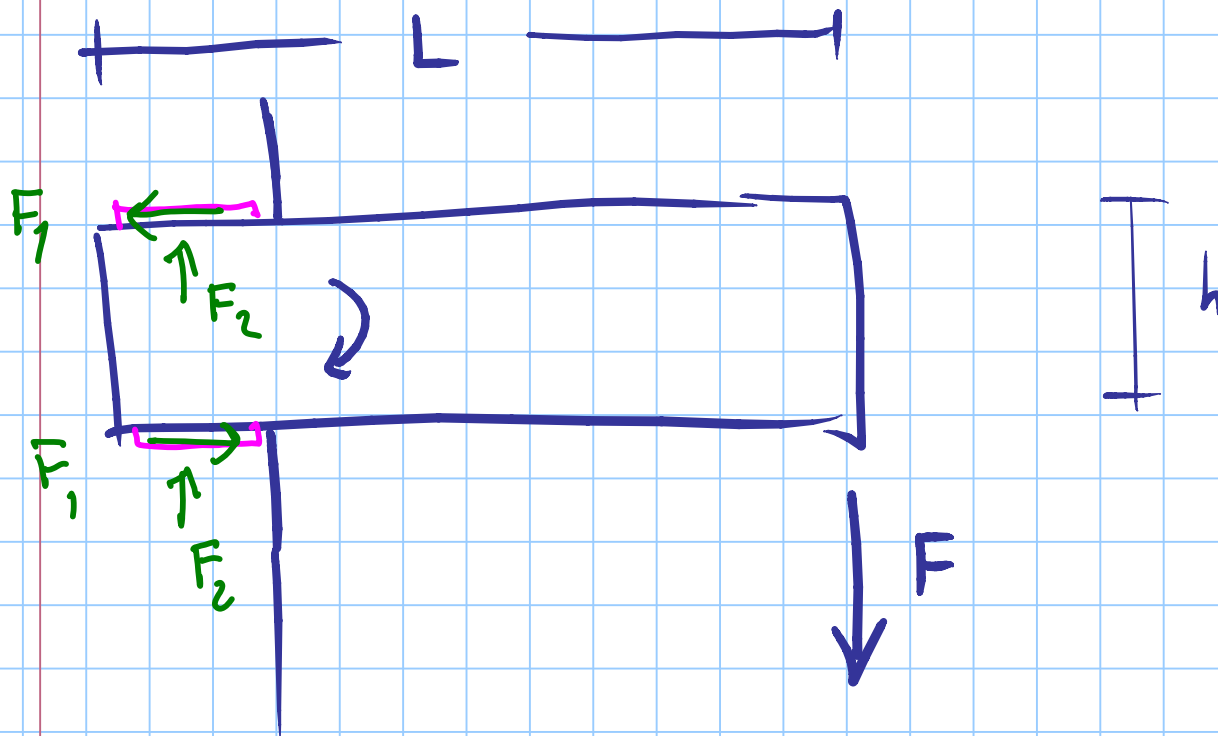
$$\frac{f_{vwd}^2}{4} a^2 \ell^4 - \frac{v^2}{4} \ell^2 - 4M^2 = 0$$

$$\ell^2 = \frac{+\frac{v^2}{4} \pm \sqrt{\left(\frac{v^2}{4}\right)^2 + 4 \cdot \left(\frac{f_{vwd}^2}{4} a^2\right) 4}}{2 \frac{f_{vwd}^2}{4} a^2}$$



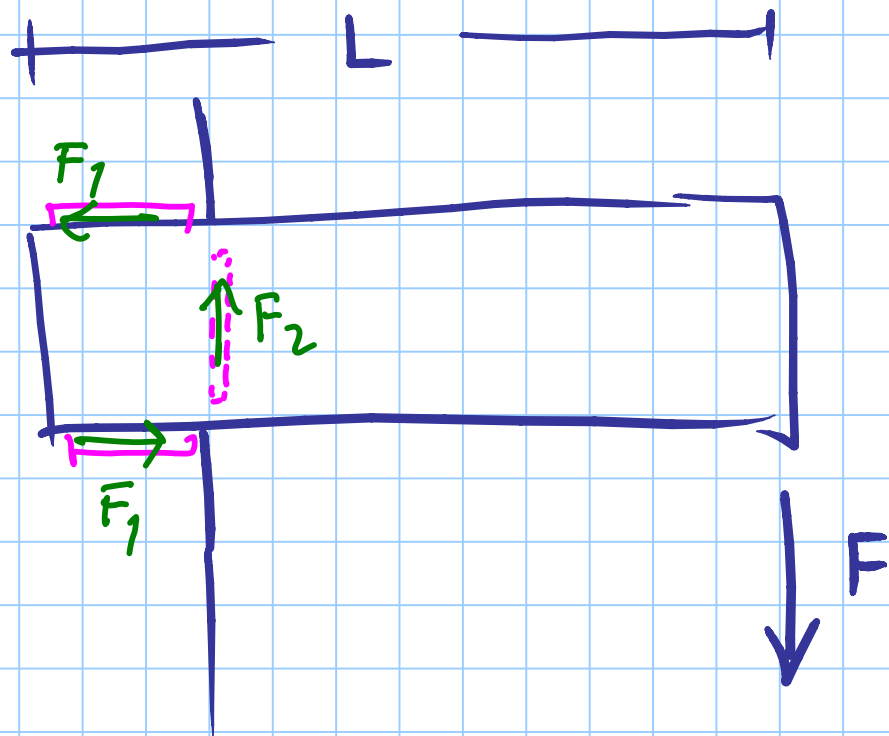
$$F_1 = \frac{F(L-d/2)}{d}$$

$$F_2 = \frac{F}{2}$$



$$F_1 = \frac{M}{h}$$

$$F_2 = \frac{V}{2}$$



$$F_1 \approx \frac{M}{h}$$

$$F_2 \approx V$$

