

COMPRESSIONE

Titolo nota

25/03/2014

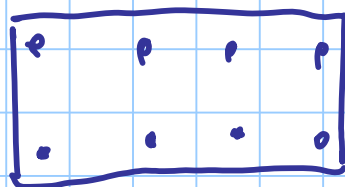
$$A_{ci} = A_s + n A_s$$

$$\sigma_c = \frac{N}{A_{ci}}$$

$$\sigma_s = n \sigma_c$$

a tempo infinito, per tener conto degli effetti viscosi

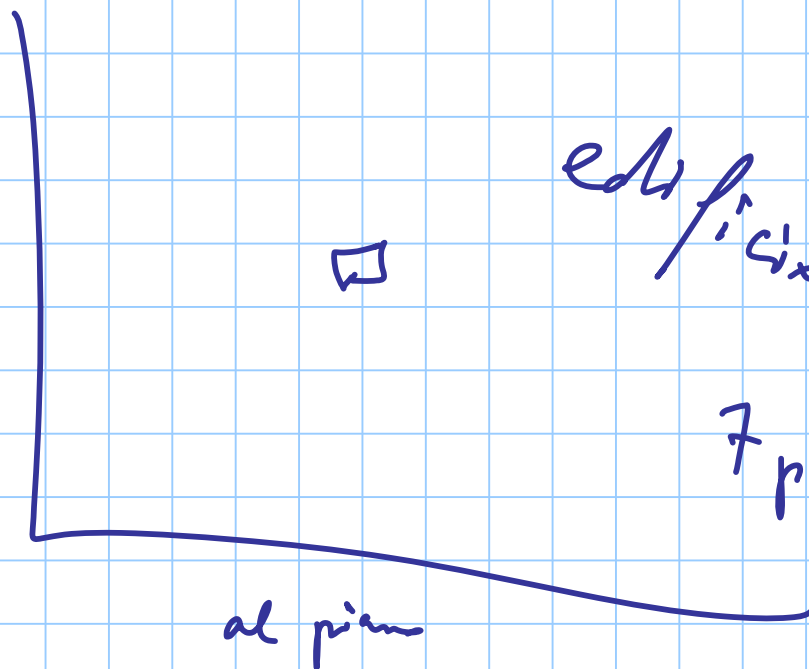
$$n = 15$$



8φ14

30

60



N

$$g_k = 170 \text{ kN}$$

$$q_k = 50 \text{ kN}$$

$$\psi_2 = 0.3$$

quasi permanente

$$g_k + \psi_2 q_k$$

al pian. $170 + 0,3 \times 50 =$
 $= 185 \text{ kN}$

$$N = 7 \times 185 = 1295 \text{ kN}$$

d. vari dir
- 1295
push comp

stato tensioni

q. perm.

$$t = \infty$$

$$n = 15$$

$$A_{ci} = A_c + n A_s = 30 \times 60 + 15 \times 8 \times 1,54 = 1985 \text{ cm}^2$$

$$\sigma_c = \frac{1295 \times 10^3}{1985 \times 10^2} = 6,52 \text{ MPa}$$

↑ - 6,52

$$\sigma_s = 15 \times 6,52 = 97,9 \text{ MPa}$$

- 97,9 neg. fivi

zona

al piano

$$170 + 50 = 220 \text{ kN}$$

$g_n + q_n$

alle basi

$$N = 7 \times 220 = 1540 \text{ kN}$$

$$\sigma_c = \frac{1540 \times 10^3}{1985 \times 10^2} = 7.76 \text{ MPa}$$

$$\sigma_s = 116.4 \text{ MPa}$$

C25/30

$\bar{\sigma}_c$

7.75 MPa

F4B44N

$\bar{\sigma}_s = 255 \text{ MPa}$

Tensioni Ammissibili

acciai, $F_e B44K$

$$\bar{\sigma}_s = 255 \text{ MPa}$$

calcestruzzo

$$R_{ck} = 25 \text{ MPa}$$

$$\bar{\sigma}_c = 8,5 \text{ MPa}$$

$$\bar{\sigma}_c = 6 + \frac{R_{ck} - 15}{4}$$

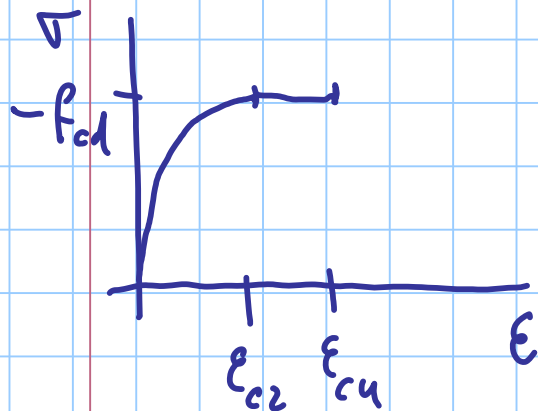
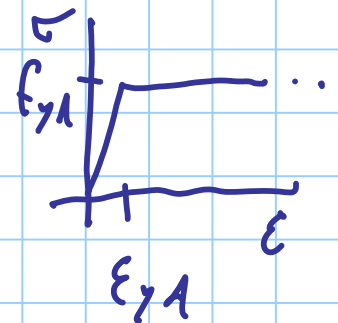
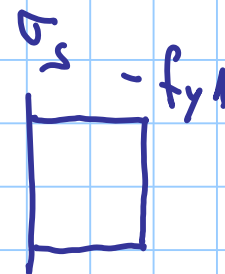
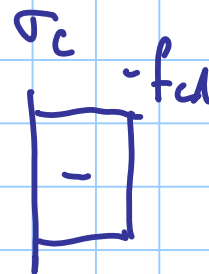
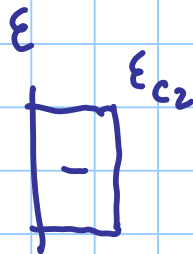
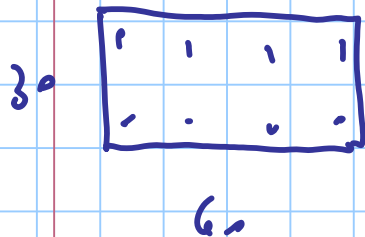
$$R_{ck} = 30 \text{ MPa}$$

$$\bar{\sigma}_c = 9,75 \text{ MPa}$$

per sol N il limite è $0,7 \bar{\sigma}_c$

oggi SLV

tra modelli di comportamento.



sezione pretesata

$$|\epsilon| \leq |\epsilon_{cu}|$$

sezione inf. compressa

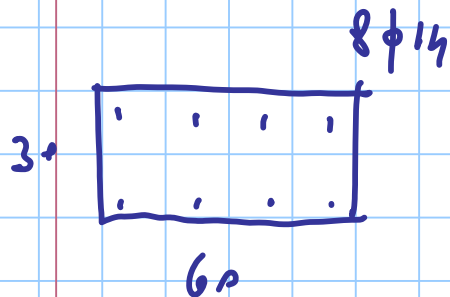
$$|\epsilon| \leq |\epsilon_{c2}|$$

$$N = \int \sigma dA = \int_{cs} \sigma_c dA_c + \int_{acc} \sigma_s dA_s = -A_c f_{cd} - A_s f_{yd}$$

$$N_{Rd} = A_c f_{cd} + A_{s,T.T} f_{yd} \quad (\text{neg. T.T. per due comp.})$$

$$C25/30 \quad f_{cd} = \alpha_{cc} \frac{f_{ck}}{\gamma_c} = 0.85 \frac{25}{1.5} = 14.2 \text{ MPa}$$

$$B450C \quad f_{yd} = \frac{f_{yk}}{\gamma_s} = \frac{450}{1.15} = 391.3 \text{ MPa}$$



$$g_k = 170 \text{ kN}$$

$$q_k = 50 \text{ kN}$$

al piano

SLU

$$g_d = \gamma_g g_k = 1.3 \times 170 = 221 \text{ kN}$$

$$q_d = \gamma_q q_k = 1.5 \times 50 = 75 \text{ kN}$$

alle basi

$$N_{Ed} = 7 \times (221 + 75) = 2072 \text{ kN}$$

$$N_{Rd} = \frac{1800 \times 10^2 \times 14.2 + 8 \times 1.57 \times 10^2 \times 391.3}{10^3} = 3038 \text{ kN}$$

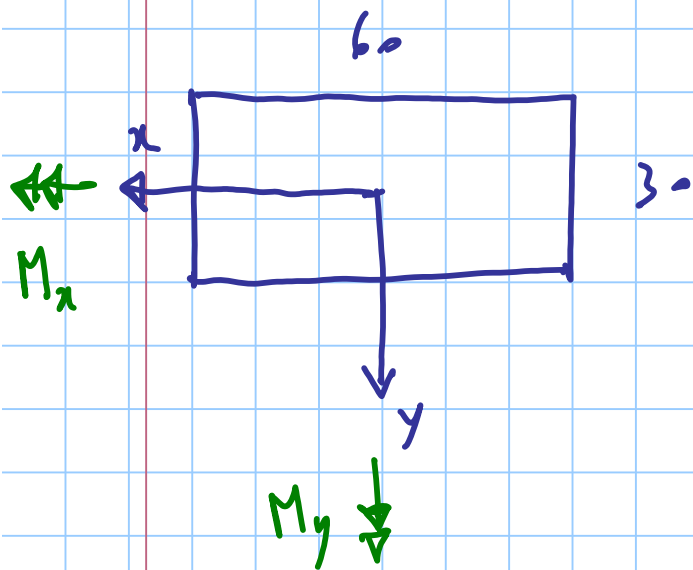
NTC 08 , EC2

c'è sempre M

anche se non c'è (o è piccolo) N

$$M_{ed} = N_{ed} \cdot e$$

$$e = 0,05 h \geq 20 \text{ mm}$$



$$e = \text{MAX} \left(0,05 h ; 2 \text{ cm} \right)$$

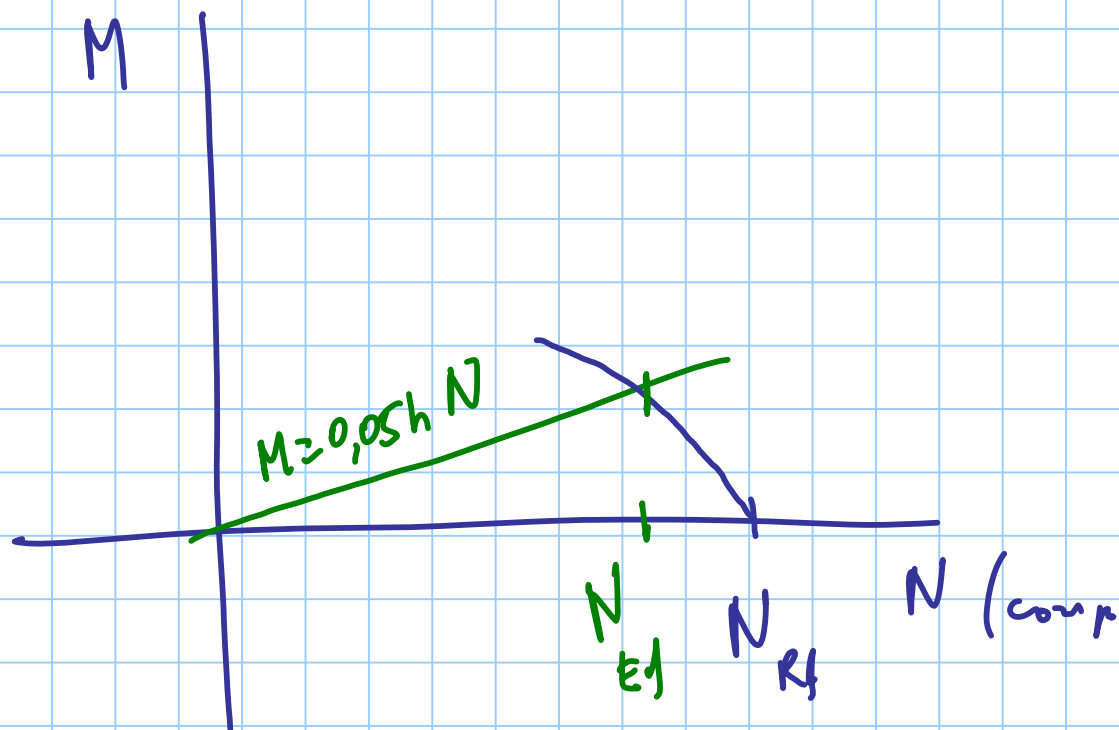
$\text{pr } M_x \quad h = 30 \text{ cm} \quad 0,05 h = 1,5 \text{ cm}$
 $\text{us. } e = 2 \text{ cm}$

$\text{pr } M_y \quad h = 60 \text{ cm} \quad 0,05 h = 3,0 \text{ cm}$
 $\text{us. } e = 3 \text{ cm}$

$$N_{Ed} = 2072 \text{ kN}$$

$$M_{x,Ed} = 2072 \times 0,02 = 41,4 \text{ kNm}$$

$$M_{y,Ed} = 2072 \times 0,03 = 62,1 \text{ kNm}$$



suggerimento progettuali:

$$N_{Rd} \geq 1,20 N_{Ed}$$