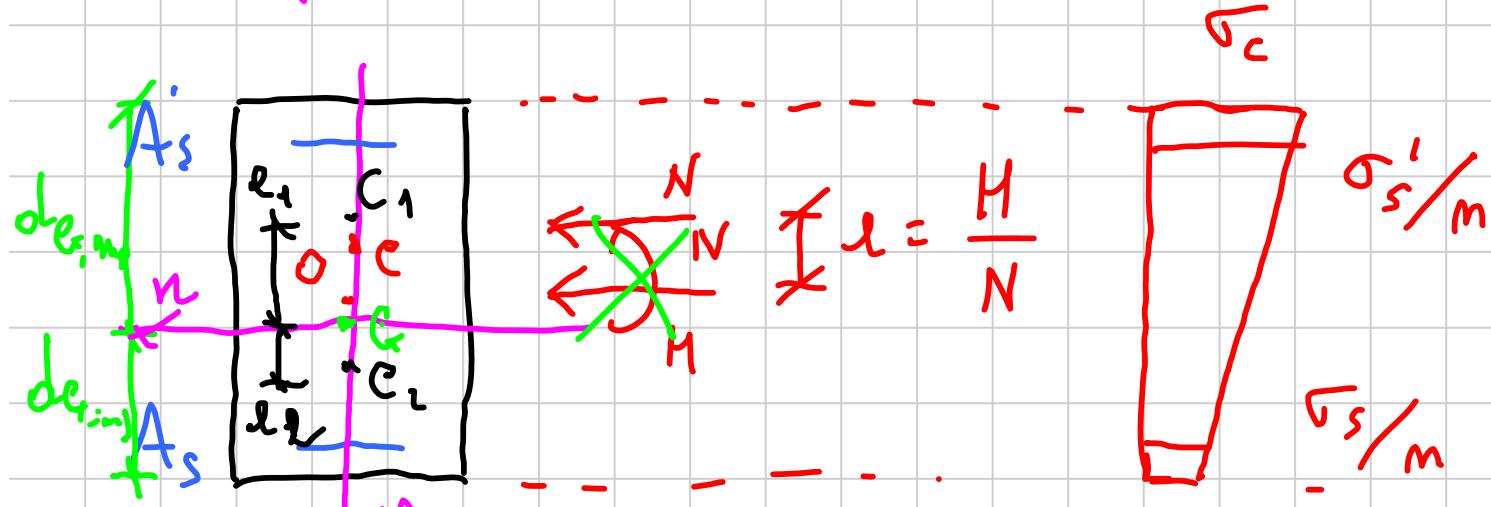


Punto flusione - piccole eccentricità

Titolo nota

23/04/2015



$$S_{sup} = \frac{bh^2}{2} + m A'_s c + m A_s d$$

$$A = b h + m (A'_s + A_s)$$

$$d_{e,mp} = \frac{S_{sup}}{A}$$

$$d_{e,inf} = h - d_{e,mp}$$

$$d_1 = \frac{I}{A_{\text{outer,ring}}}$$

$$d_2 = \frac{I}{A_{\text{inner}}}$$

$$I = \frac{b d_{\text{outer}}^3}{3} + \frac{b d_{\text{inner}}^3}{3} + m A_s (d_{\text{inner}} - e)^2 + \\ + m A_s (d_{\text{outer}} - e)^2$$

$$d_{\text{ext,s}} = \frac{M}{N} - \left(\frac{h}{2} - d_{\text{outer}} \right)$$

$$-e_1 \leq e_{\text{ext,s}} \leq e_2$$

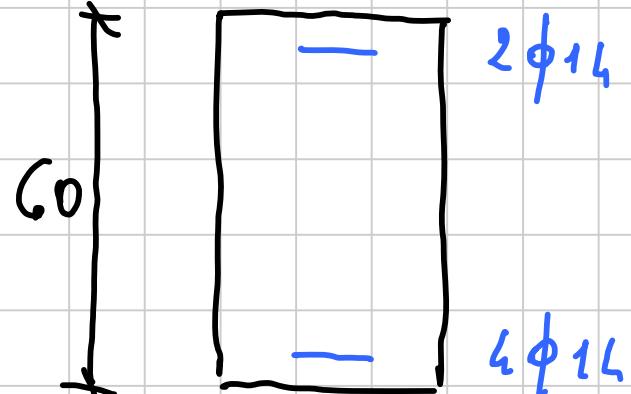
piccole eccentricità

$$\sigma_c = \frac{N}{A} - \frac{N_{ects}}{I} d_{c,mp} \leq 0,6 \text{ fck}$$

Comb, more

$$\sigma_{c,ring} = \frac{N}{A} + \frac{N_{ects}}{I} d_{c,ring}$$

$$\sigma'_s = m \left[\frac{N}{A} - \frac{N_{ects}}{I} (d_{c,mp} - c) \right]$$



$N = -1000 \text{ KN}$
 $M = 100 \text{ KNm}$

C 25/30

B 650 C

e = 4 cm

30 x 60

$$S_{\text{sup}} = \frac{30 \times 60^2}{2} + 15 \times 3,08 \times 4 + 15 \times 6,16 \times 56 = 59359,2 \text{ cm}^3$$

$$A = 30 \times 60 + 15 (3,08 + 6,16) = 1938,6 \text{ cm}^2$$

$$\text{OL}_{\text{e, sup}} = \frac{59359,2}{1938,6} = 30,6 \text{ hm}$$

$$d_{\text{er. und}} = 60 - 30,6 = 29,4 \text{ cm}$$

$$I = 30 \times \frac{29,4^3}{3} + 30 \times \frac{30,6^3}{3} + 15 \times 3,08 \times (30,6 - 4)^2 \\ + 15 \times 6,16 \times (29,4 - 4)^2 = 632950 \text{ cm}^4$$

$$d_1 = \frac{632950}{1938,6 \times 29,4} = 11,1 \text{ cm}$$

$$d_2 = \frac{632950}{1938,6 \times 30,6} = 10,7 \text{ cm}$$

$$l_{c+s} = \frac{100}{-1000} \times 10^2 - \left(\frac{60}{2} - 29,4 \right) = -10,6 \text{ cm}$$

$$-l_1 = -11,1 < -10,6 < l_2 = 10,7$$

$$\sigma_c = \frac{-1000}{1938,6} \times 10 - \frac{\cancel{+1000} \times (-10,6)}{\cancel{632950}} \times 30,6 \times 10$$

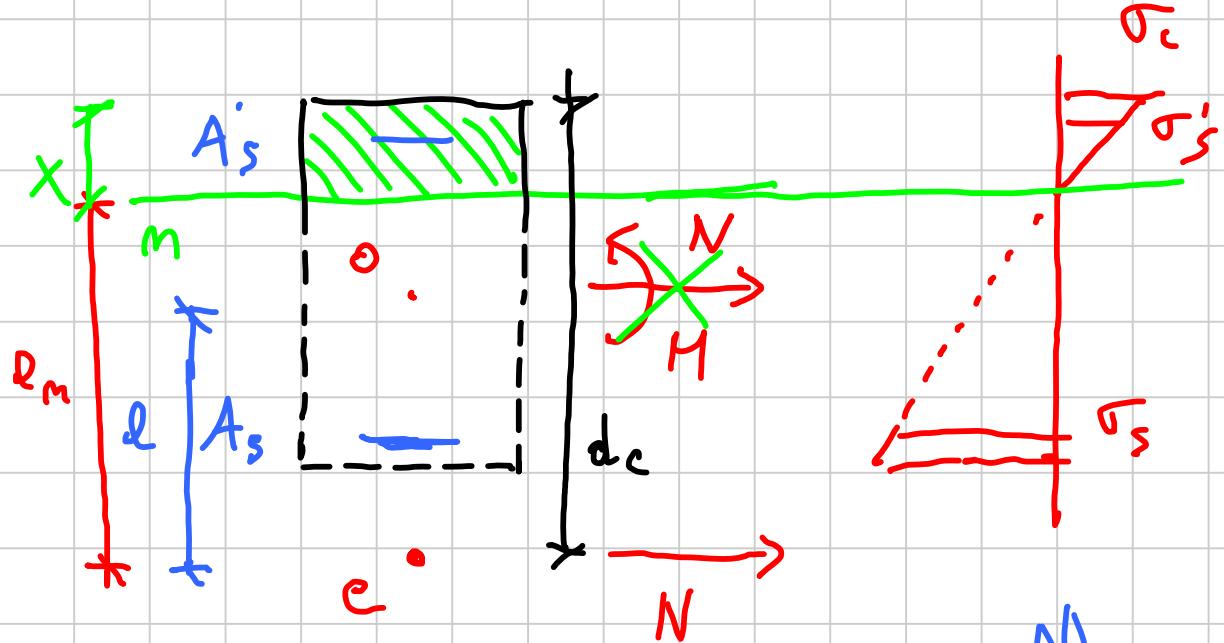
|

$$= -10,3 \text{ MPa}$$

$$\sigma_c = 10,3 \leq 0,6 f_{ck} = 15 \text{ MPa}$$

a
I
o
V

Fletchão com reentrância (II steolis)



$$d = \frac{M}{N}$$

$$l_m = \frac{I_m}{S_m}$$

$$d_c = \frac{h}{2} + l$$

$$l_m = d_c - x$$

$$S_m = -\frac{bx^2}{2} - m A'_s (x-c) + m A_s (d-x)$$

$$I_m = \frac{bx^3}{3} + m A'_s (x-c)^2 + m A_s (d-x)^2$$

$$I_m = S_m l_m$$

$$\left(-\frac{bx^2}{2} - m A'_s x + m A'_s c + m A_s d - m A_s x \right) (l_c - x) =$$

$$= -\frac{bx^2}{2} l_c + \frac{bx^3}{2} - m A'_s l_c x + m A'_s x^2 + m A'_s e l_c +$$

$$- m A'_s c x + m A_c d l_c - m A_s d x - m A_s l_c x + m A_s x^2$$

$$\begin{aligned}
 & -\frac{bx^2}{2}dc + \frac{bx^3}{2} - m\overline{A'_s}dx + m\overline{A'_s}x^2 + m\overline{A'_s}edc \\
 & - m\overline{A'_s}cx + m\overline{A_c}ddc - m\overline{A_s}dx - m\overline{A_s}dcx + m\overline{A_s}x^2 \\
 = & \frac{bx^3}{3} + m\overline{A'_s}x^2 + m\overline{A'_s}e^2 - 2m\overline{A'_s}xe + m\overline{A_s}d^2 + \\
 & m\overline{A_s}x^2 - 2m\overline{A_s}dx
 \end{aligned}$$

$$\begin{aligned}
 & \cancel{\frac{bx^3}{6}} - \frac{3b}{8}dcx^2 + \frac{6m}{b} \left[A'_s(e-d_c) + A_s(d-d_c) \right] x \\
 & - \frac{6m}{b} \left[A'_s(e-d_c)e + A_s(d-d_c)d \right] = 0
 \end{aligned}$$

$$x^3 - 3d_c x^2 + \frac{6m}{b} [A'_s(c-d_c) + A_s(d-d_c)]x +$$

$$- \frac{6m}{b} [A'_s(c-d_c)c + A_s(d-d_c)d] = 0$$

$$\sigma = \frac{N}{S_m} s$$

$$S_m = - \frac{bx^2}{2} - m A'_s(x-c) + m A_s(d-x)$$



$$\sigma = \frac{Ne_m}{I_m} s$$

$$I_m = \frac{bx^3}{3} + m A'_s(x-c)^2 + m A_s(d-c)^2$$

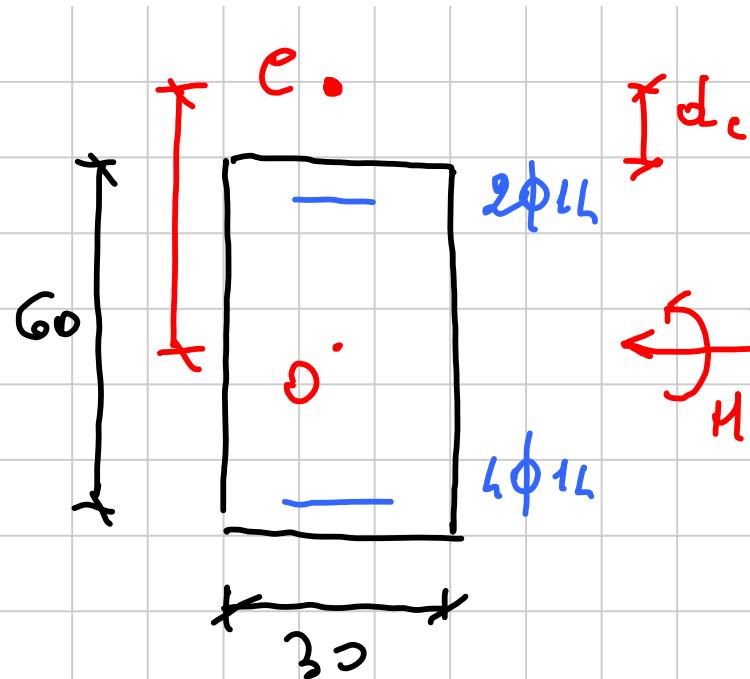
$$\sigma_c = -\frac{N}{S_m} x \leq 0.6 f_{ck}$$

rene

quasi-perm.

$$0.15 f_{ck}$$

$$\sigma_s = n \frac{N}{S_m} (d - x) \leq 0.8 f_{ck}$$



$$N = -500 \text{ KN}$$

$M = 200 \text{ KN} \cdot \text{m}$

C25/30

Rc 450 C

e = 40 mm

$$l = \frac{M}{N} = \frac{200}{-500} = -0.4 \text{ m} = -40 \text{ mm}$$

$$x^3 - 3d_c x^2 + \frac{6m}{b} [A'_s(c-d_c) + A_s(d-d_c)] x +$$

$$- \frac{6m}{b} [A'_s(c-d_c)c + A_s(d-d_c)d] = 0$$

$$A = 1$$

$$B = -3 \times (-10) = 30 \text{ cm}$$

$$C = \frac{6 \times 15}{30} \times \left[3.08 \times (4 + 10) + 6.16 \times (56 + 10) \right] = 1349 \text{ cm}^2$$

$$D = -\frac{6 \times 15}{30} \times \left[3.08 \times 14 \times 4 + 6.16 \times 66 \times 56 \right] = -68819,5 \text{ cm}^3$$

$$x = 25,2 \text{ cm}$$

$$\sigma : \frac{N}{S_m} s$$

$$S_m = -\frac{30 \times 25,2^2}{2} - 15 \times 3,08 \times (25,2 - e) + 15 \times 6,16 \times (56 - 25,2)$$
$$= -7659 \text{ cm}^3$$

NO

$$\sigma_c = -\frac{500}{-7659} \times 25,2 \times 10 = |-16,5 \text{ MPa}| \leq 15 \text{ MPa}$$

$$\sigma_s = 15 \times \frac{-500}{-7659} \times (56 - 25,2) \times 10 = 301,6 \text{ MPa} \leq 360 \text{ MPa}$$

Flusso in composite - tensioni ammissibili

$$\bar{\sigma}_c \quad \bar{\sigma}_s$$

$$\sigma_c \leq \bar{\sigma}_c$$

$$\sigma_s \leq \bar{\sigma}_s$$

$$\sigma_m \leq 0.4 \bar{\sigma}_c$$

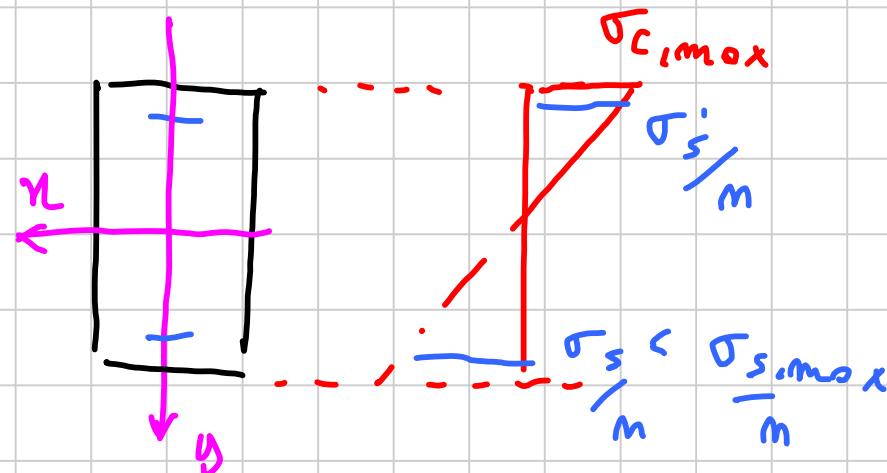
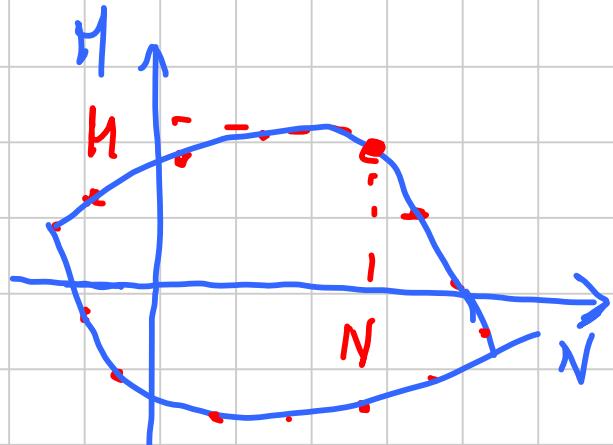
$\sigma_c + \sigma_s$ come per tensioni unidirezionali

Stato limite obiettivo: in esercizio 2

$$\sigma_c = \sigma_{c,\max}$$

0

$$\sigma_s = \sigma_{s,\max}$$



$$N = \int_A \sigma dA$$

$$M = \int_A \sigma_y dA$$

DOMINI H-N e diagrammi limiti di funzionali

