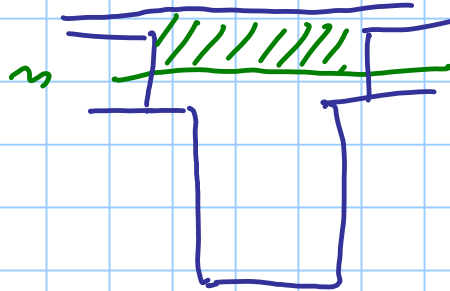
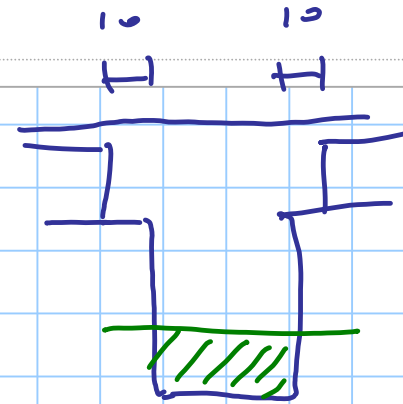


$$M = -350 \text{ KNm}$$


 $M > 0$

 $M < 0$

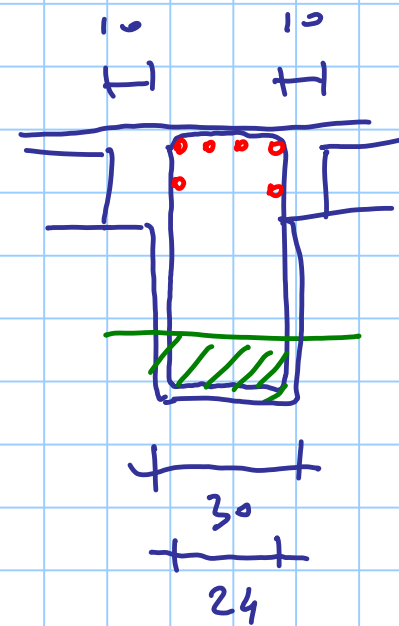
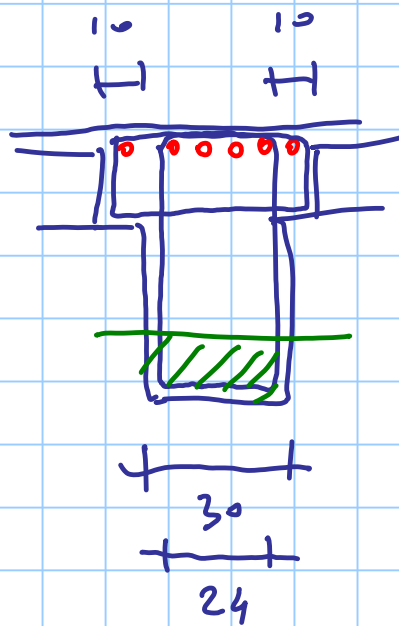
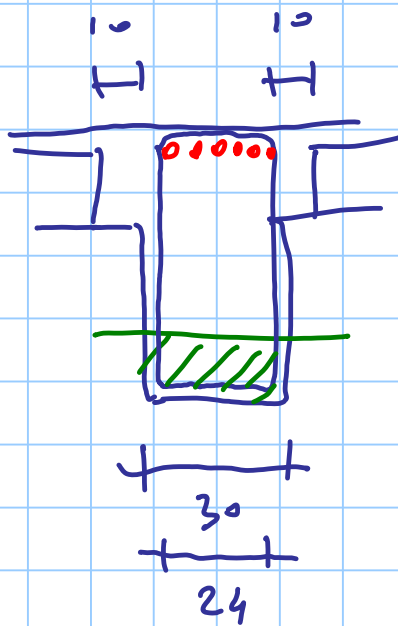
$$d = \eta' \sqrt{\frac{M}{b}}$$

$$= 0.017 \sqrt{\frac{350}{0.30}} = 0.58 \text{ m} = 58 \text{ cm}$$

miglior 30x70

ma io preferisco con 30x60

$$A_s = \frac{M}{0.9 d f_{yA}} = \frac{350 \times 10}{0.9 \times 0.56 \times 391.3} = 17.7 \text{ cm}^2 \quad 6 \phi 20$$



solo armatura Tesa

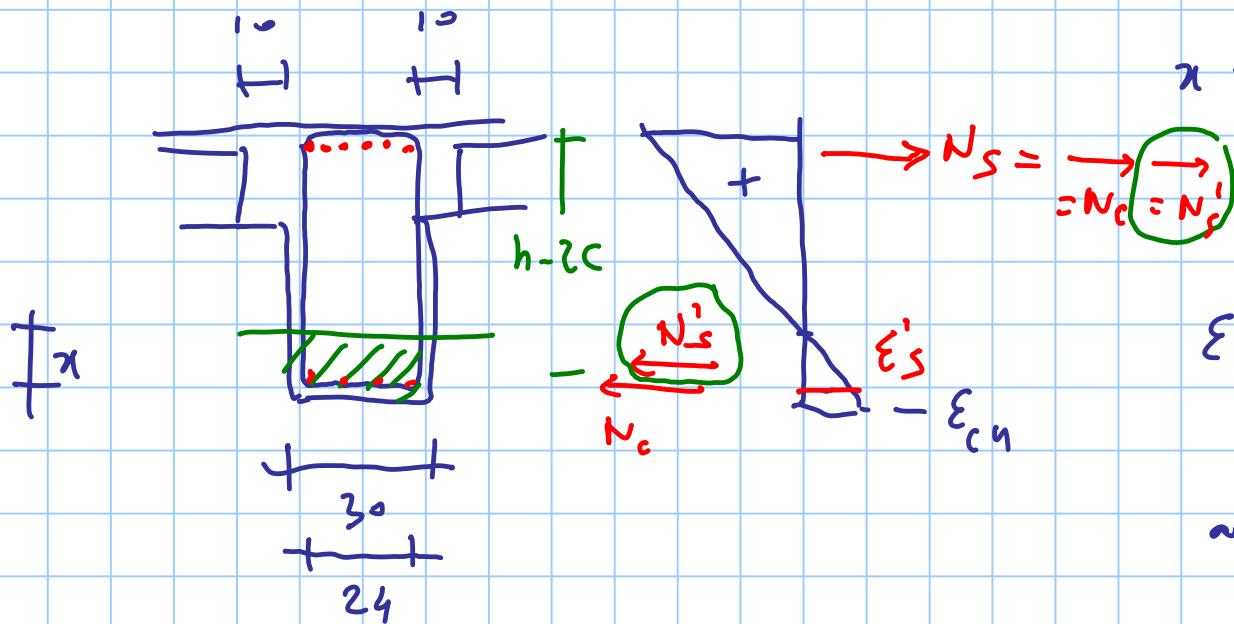
$$M_{Rd} = \frac{b d^2}{\eta^2}$$

$$\eta = 0.0197$$

per C25/30

$$M_{Rd} = \frac{0.30 \times 0.56^2}{0.0197^2} = 242.4 \text{ kNm}$$

serve A'_s



$$x = 0.25 d = 0.25 \times 56 = 14 \text{ cm}$$

$$\epsilon'_s = -\frac{x-c}{x} \quad \epsilon_{cy} = -0.0025$$

area A'_s is shear area

$$\sigma'_s = f_{yd}$$

$$\Delta M = 350 - 242.4 = 107.6 \text{ KNm}$$

$$A'_s = \frac{\Delta M}{(h-2c) \sigma'_s} = \frac{107.6 \times 10}{0.52 \times 391.3} = 5.3 \text{ cm}^2 \quad 4 \phi 14 \text{ (or } 2 \phi 20)$$

Transverse

$$h = 26 \text{ cm}$$

$$c = 4 \text{ cm}$$

$$d = 22 \text{ cm}$$

$$M_{Ed} = 160 \text{ kNm} > 0 \text{ positive}$$

$$b = \frac{M \eta^2}{d^2} = \frac{160 \times 0.018^2}{0.22^2} = 1.07 \text{ m}$$

$$b = 110 \text{ cm}$$

$$A_s = \frac{M}{0.9 d f_{yd}} = \frac{160 \times 10}{0.9 \times 0.22 \times 391.3} = 20.7 \text{ cm}^2$$

$$7 \phi 20$$

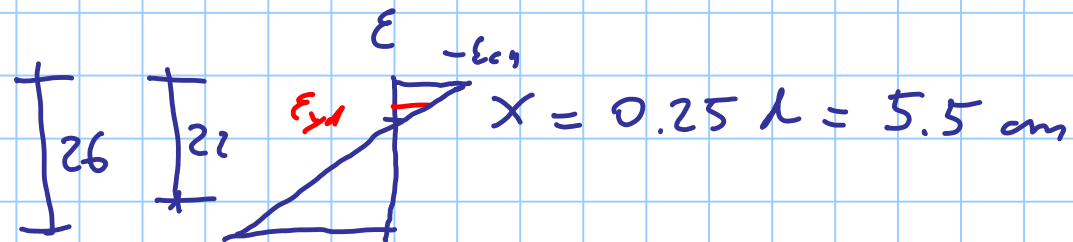
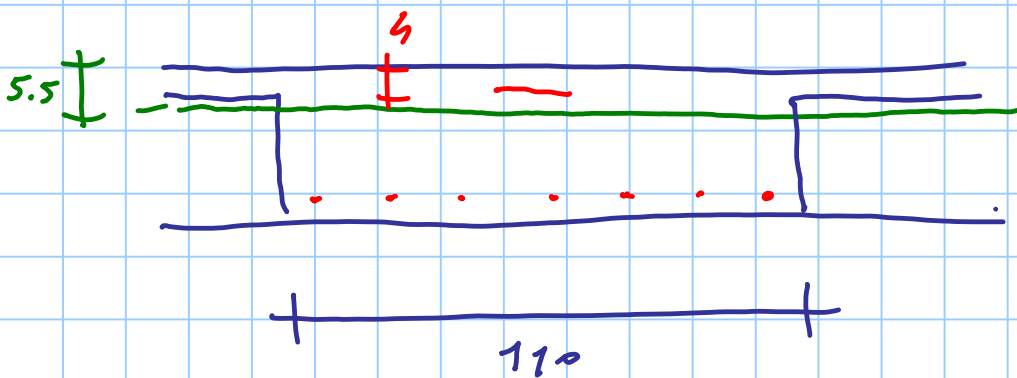
concrete A_s

$$M_{rd} = \frac{b d^2}{\eta^2} = \frac{1.10 \times 0.22^2}{0.0197^2} = 137.2 \text{ kNm}$$

acc. to A'_s

per portion

$$\Delta M = 160 - 137.2 = 22.8 \text{ kNm}$$

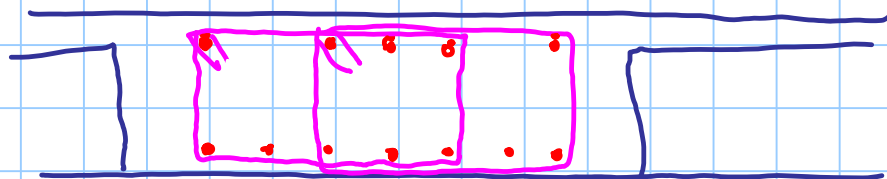


$$\epsilon'_s = - \frac{x - c}{x} \epsilon_{cy} = - 0.000968$$

$$\sigma'_s = \epsilon'_s E_s = 193.6 \text{ MPa}$$

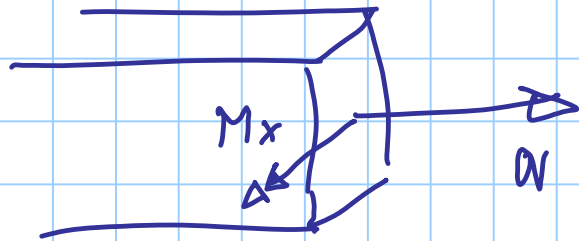
$$A'_s = \frac{\Delta M}{(h - 2c) \sigma'_s} = \frac{22.8 \times 10}{0.18 \times 193.6} = 6.5 \text{ cm}^2$$

5 ϕ 16



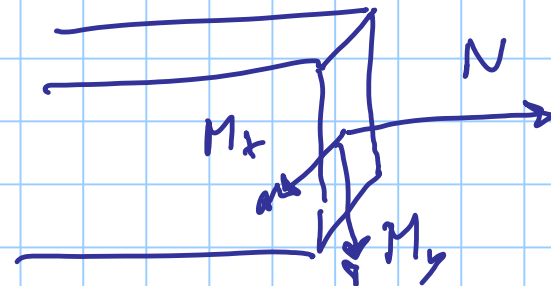
FLESSIONE COMPOSTA

RETTA



modell. lineari
omogeneo

DEVIATA



$$\sigma = \frac{N}{A} + \frac{M_x}{I_x} y - \frac{M_y}{I_y} x$$

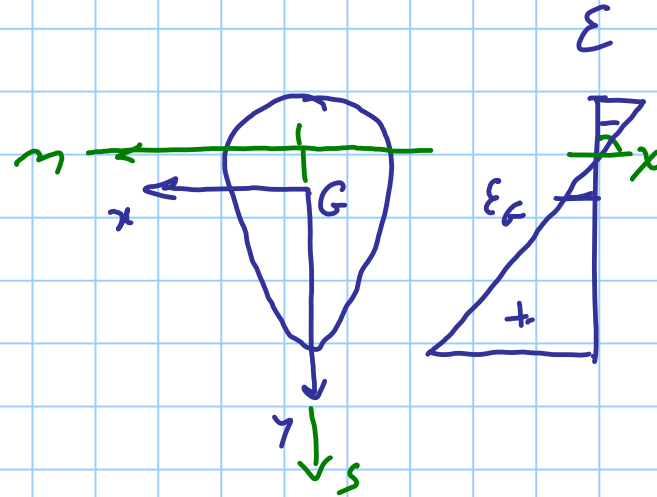
$$N = \int \sigma dA$$

$$M_x = \int \sigma y dA$$

$$N = \int E \chi s dA = E \chi \underbrace{\int s dA}_{S_m}$$

$$N = E \chi S_m$$

$$\begin{aligned} M_m &= \int \sigma s dA = \int E \chi s^2 dA = \\ &= E \chi \underbrace{\int s^2 dA}_{I_m} = E \chi I_m \end{aligned}$$



$$\epsilon = \epsilon_f + \chi y$$

$$\sigma = E \epsilon = E \epsilon_f + E \chi y$$

$$\epsilon = \chi s$$

$$\sigma = E \chi s$$

$$N = E X S_n \rightarrow EX = N / S_n$$

$$M_n = E X I_n$$

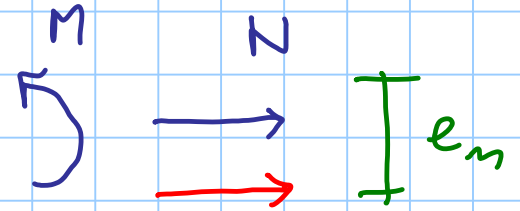
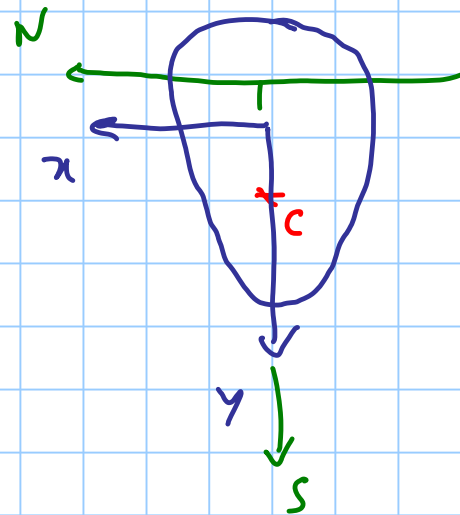
$$EX = M_n / I_n$$

$$e_n = \frac{M_n}{N} = \frac{I_n}{S_n}$$

$$\sigma = E X s$$

$$\sigma = \frac{M_n}{I_n} s$$

$$\sigma = \frac{N}{S_n} s$$



c = centro di sollecitazione

$$e_c = \frac{M}{N}$$