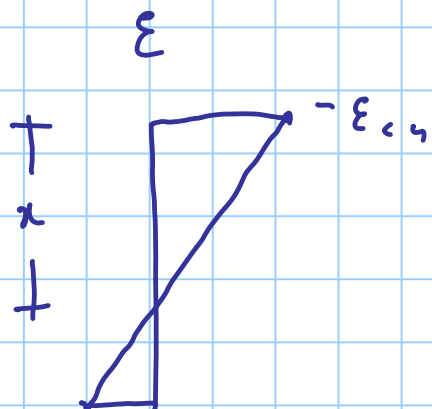
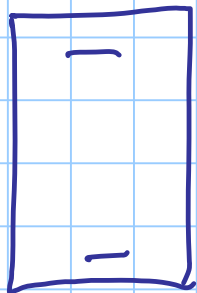


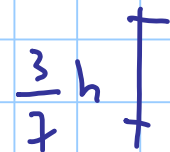
FLESSIONE COMPOSTA - SLV

Titolo nota

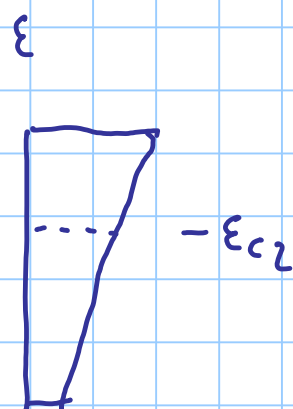
29/11/2016



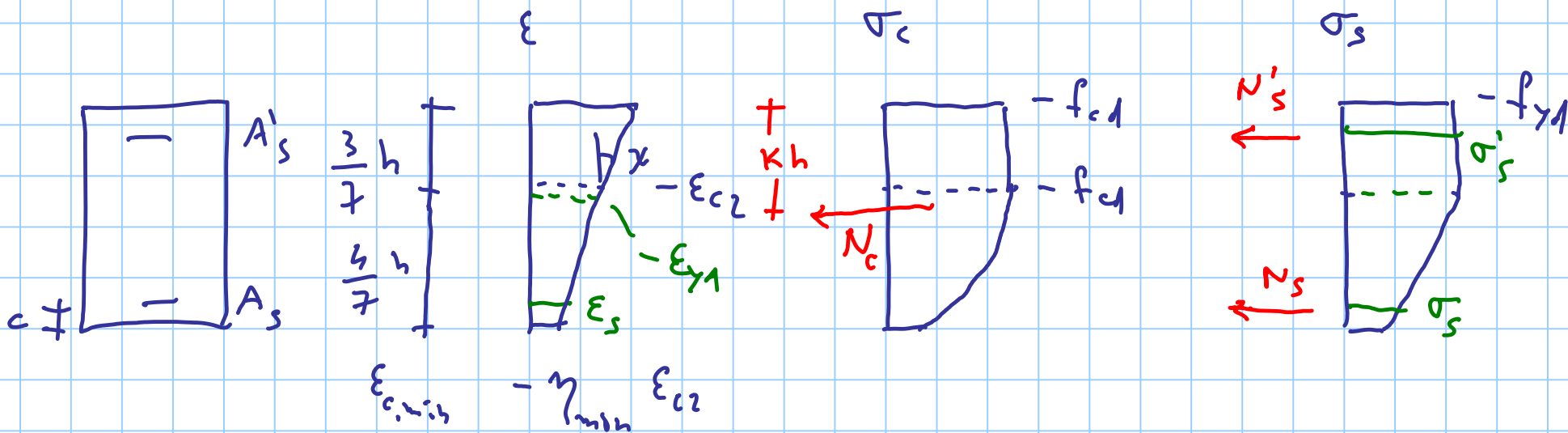
$$x = h ; \eta_{min} = 0$$



$$\epsilon_{c, min} - \eta_{min} \epsilon_{c2}$$



$$M_{Ed} \quad N_{Ed}$$



$$N = \int \sigma dA = N_{Ed}$$

$$N_c = -\beta b \cancel{h} f_{cd}$$

$$N = N_s + N'_s + N_c = N_{Ed}$$

$$\beta = 0.810 \quad \text{per} \quad \eta_{min} = 0$$

$$N_s = A_s \sigma_s \quad N'_s = A'_s \sigma'_s$$

$$\beta = 1 \quad \text{per} \quad \eta_{min} = 1$$

$$\varepsilon_s = -\varepsilon_{c2} + \chi \left(\frac{4}{7} h - c \right)$$

$$\chi = \frac{-\eta_{\min} \varepsilon_{c2} + \varepsilon_{c2}}{\frac{4}{7} h}$$

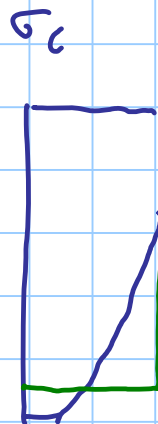
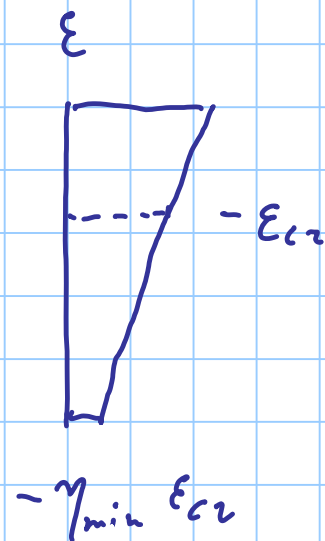
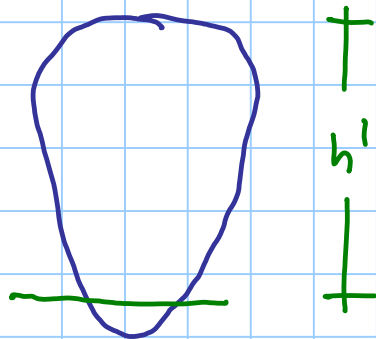
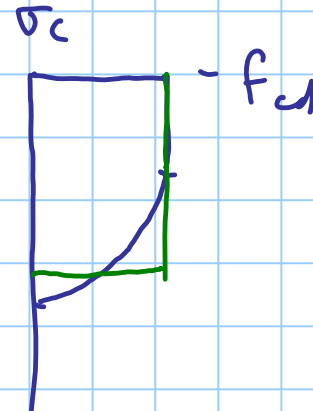
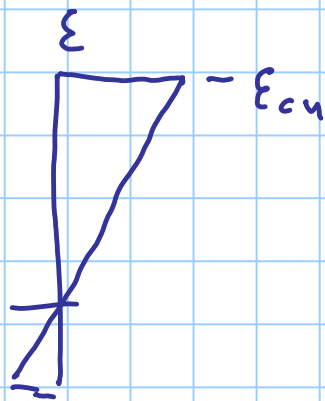
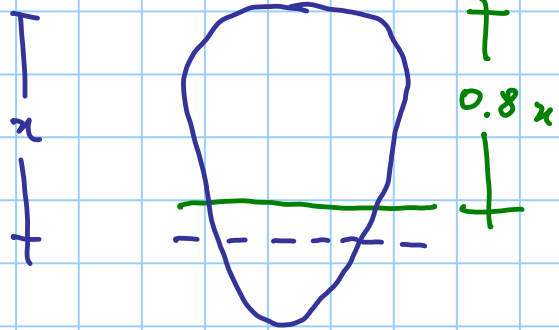
$$\varepsilon_s = - \left[\frac{c}{\frac{4}{7} h} (1 - \eta_{\min}) + \eta_{\min} \right] \varepsilon_{c2}$$

$$N_c = -\beta b h f_{cd}$$

$$\beta = 1 - \frac{4}{21} (1 - \eta_{\min})^2$$

$$k = \frac{1}{2} \frac{1 - 16/21 (1 - \eta_{\min})^2}{1 - 4/21 (1 - \eta_{\min})^2}$$

per sezioni non rettilinee

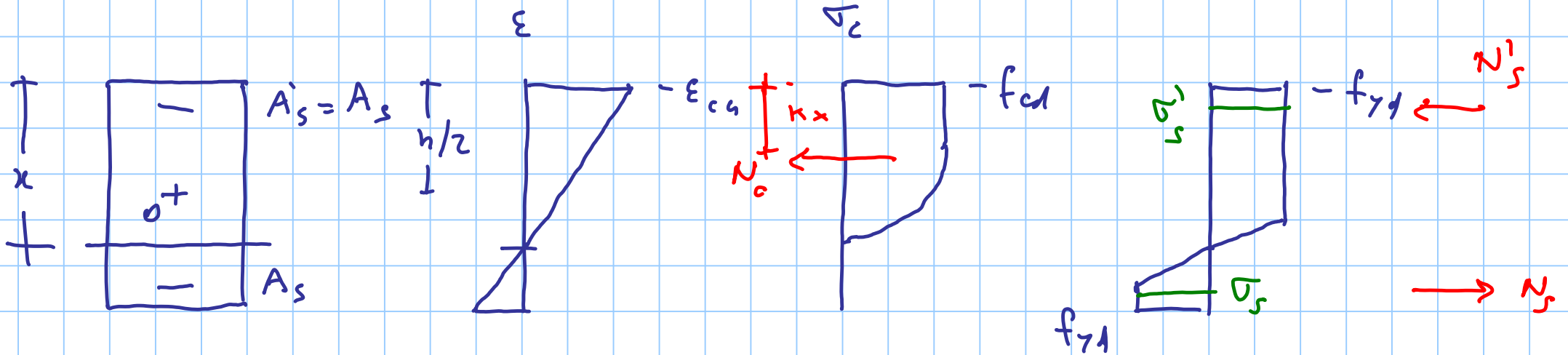


$$h' = \left[1 - 0.2 (1 - \gamma_{min})^2 \right] h$$

SEZIONE RETTANGOLARE

con

$$A_s = A'_s$$

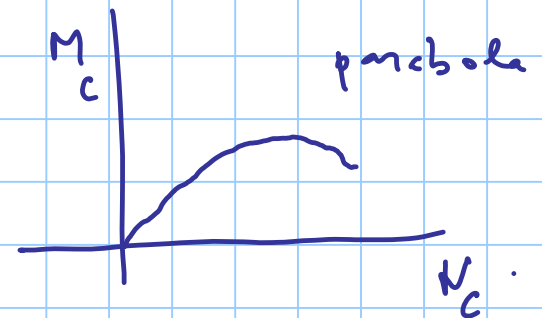


CONTRIBUT- CLS

$$N_c = -\beta b x f_{cd}$$

$$x = -\frac{N_c}{\beta b f_{cd}}$$

$$M_c = -N_c \left(\frac{h}{2} - kx \right)$$



$$M_c = -N_c \left(\frac{h}{2} + k \frac{N_c}{\beta b f_{cd}} \right)$$

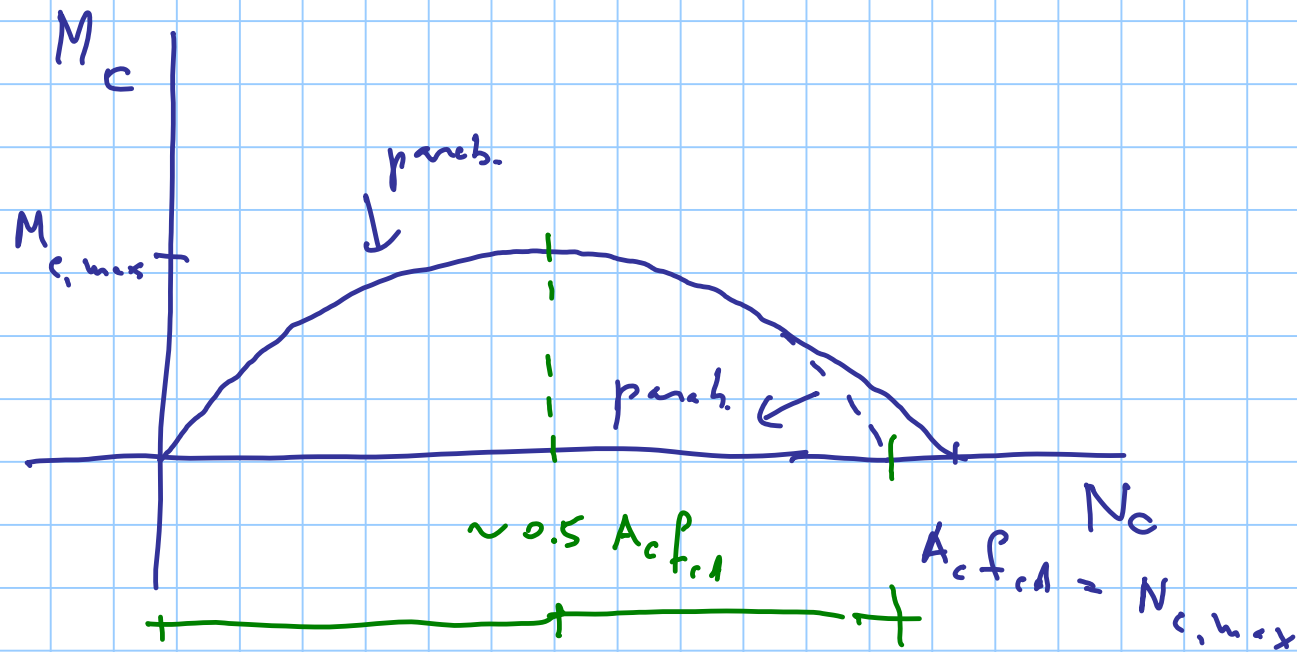
se la sezione è tutta compressa

è ancora

$$M_c = -N_c \left(\frac{h}{2} + k \frac{N_c}{\beta b f_{cd}} \right)$$

ma

β e k non sono costanti:



$$M_c = -N_c \left(\frac{h}{2} + k \frac{N_c}{\beta b f_{cd}} \right)$$

$$\max \quad \approx \quad \frac{dM_c}{dN_c} = 0$$

$$\frac{dM_c}{dN_c} = -\frac{h}{2} - 2N_c \frac{k}{\beta b f_{cd}} = 0$$

$$N_c = -\frac{h}{4} \frac{\beta b f_{cd}}{k} = -\frac{\beta}{4k} A_c f_{cd} = -\nu_n A_c f_{cd}$$

$$\nu_n = \frac{\beta}{4k} = \frac{0.810}{4 \times 0.416} = 0.486 \approx 0.5$$

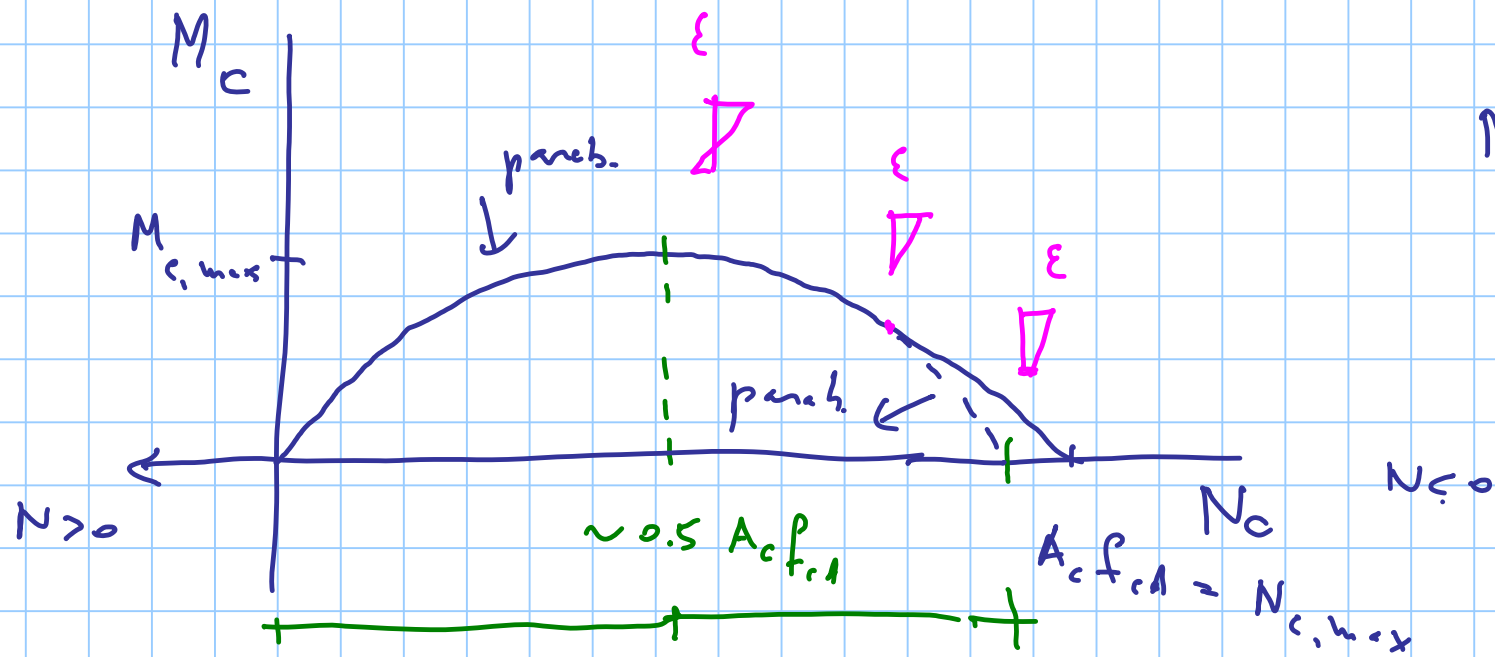
$$M_{c, \max} = M_c (N = v_m A_c f_{cd}) =$$

$$= + v_m A_c f_{cd} \left(\frac{h}{2} + k \frac{v_m A_c f_{cd}}{\beta b f_{cd}} \right) =$$

$$= v_m A_c f_{cd} h \left[\frac{1}{2} - k \frac{v_m \cancel{A_c} \cancel{f_{cd}}}{\beta b \cancel{h} \cancel{f_{cd}}} \right] =$$

$$= A_c f_{cd} h \underbrace{v_m \left[\frac{1}{2} - k \frac{v_m}{\beta} \right]}_{0.1216}$$

$$0.1216$$



$$N_{c,max} = A_c f_{cd}$$

$N < 0$ compression

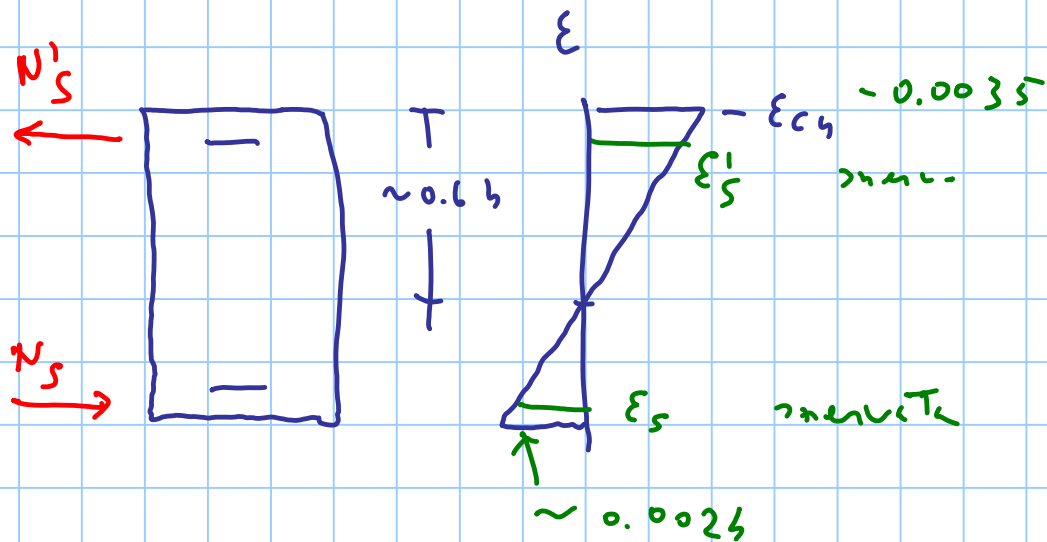
$$M_c = M_{c,max} \left[1 - \left(\frac{N + \nu_n N_{c,max}}{\nu_n N_{c,max}} \right)^2 \right]$$

max for $N = -\nu_n N_{c,max}$

si ha $M_{c, max}$ quando.

$$N_c = -\beta b x f_{cd} = -\nu_n b h f_{cd}$$

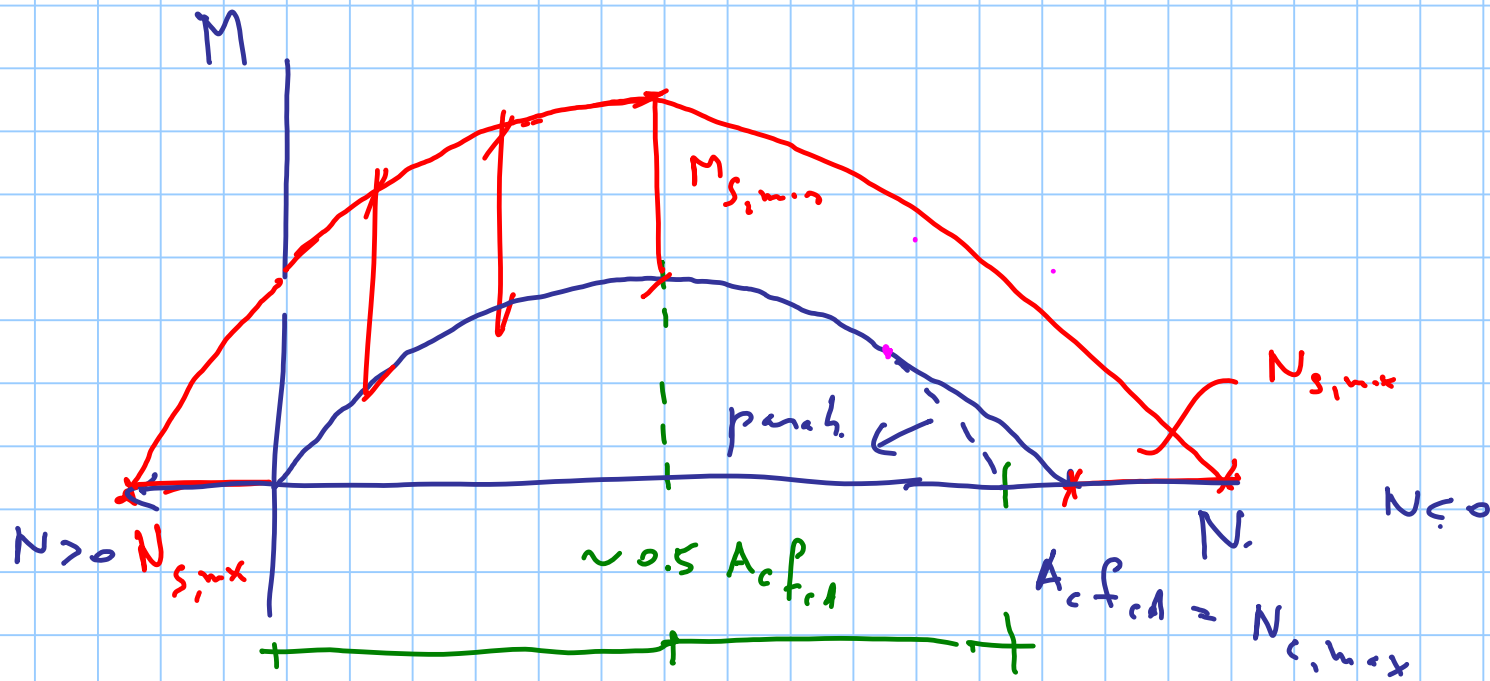
cioè per $x = \frac{\nu_n b h f_{cd}}{\beta b f_{cd}} = \frac{\nu_n}{\beta} h \approx 0.6 h$



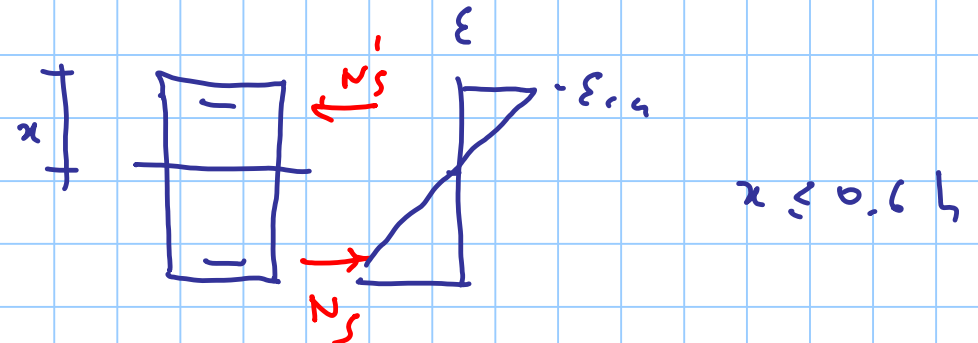
se $\frac{e}{h}$ è piccolo

$A_s \approx A'_s$ sono necessarie

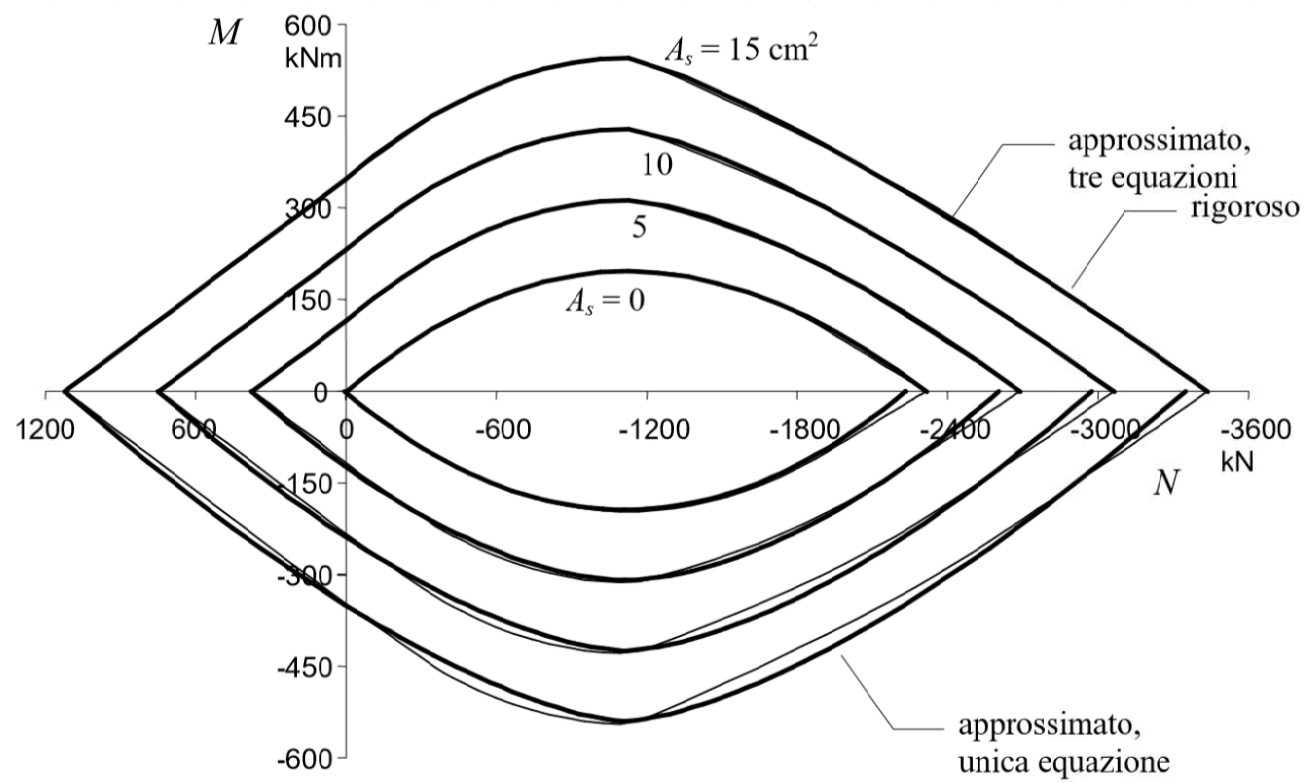
$$N_s = N'_s = A_s f_{yd} \quad \text{comp.} \\ \text{tuz}$$



$$M_{S,max} = A_s f_{yd} (h - 2c)$$

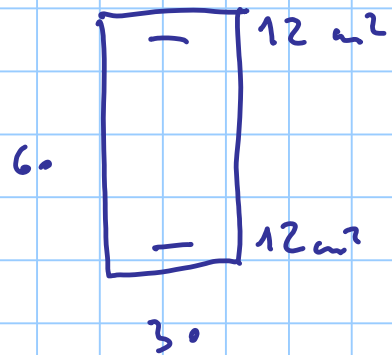


$$N_{S,max} \geq 2 A_s f_{yd} = A_{s,tot} f_{yd}$$



$$M_{RA} = (M_{c,max} + M_{s,max}) \left[1 - \left| \frac{N_{rd} + \nu_n N_{c,max}}{\nu_n N_{c,max} + N_{s,max}} \right|^m \right]$$

$$m = 1 + \frac{\nu_n N_{c,max}}{\nu_n N_{c,max} + N_{s,max}} \approx 1 + \frac{1}{1 + 2 N_{s,max} / N_{c,max}}$$



$$N_{Ed} = -1300 \text{ kN}$$

$$M_{Ed} = 180 \text{ kNm}$$

$$M_{Ed}$$

$$c = 25/30$$

$$B450C$$

$$c = 4 \text{ cm}$$

$$N_{c,max} = b h f_{cd} = 30 \times 60 \times 14.17 \times 10^{-1} = 2551 \text{ kN}$$

$$\begin{aligned} M_{c,max} &\approx 0.12 b h^2 f_{cd} = 0.12 \times 60 \times 10^{-2} \times 2551 = \\ &= 0.12 h N_{c,max} = 183.6 \text{ kNm} \end{aligned}$$

$$N_{s,max} = 2 A_s f_{yd} = 24 \times 391.3 \times 10^{-1} = 939 \text{ kN}$$

$$M_{s,max} = A_s f_{yd} (h - 2c) = \frac{939}{2} \times 0.52 = 244.2 \text{ kNm}$$

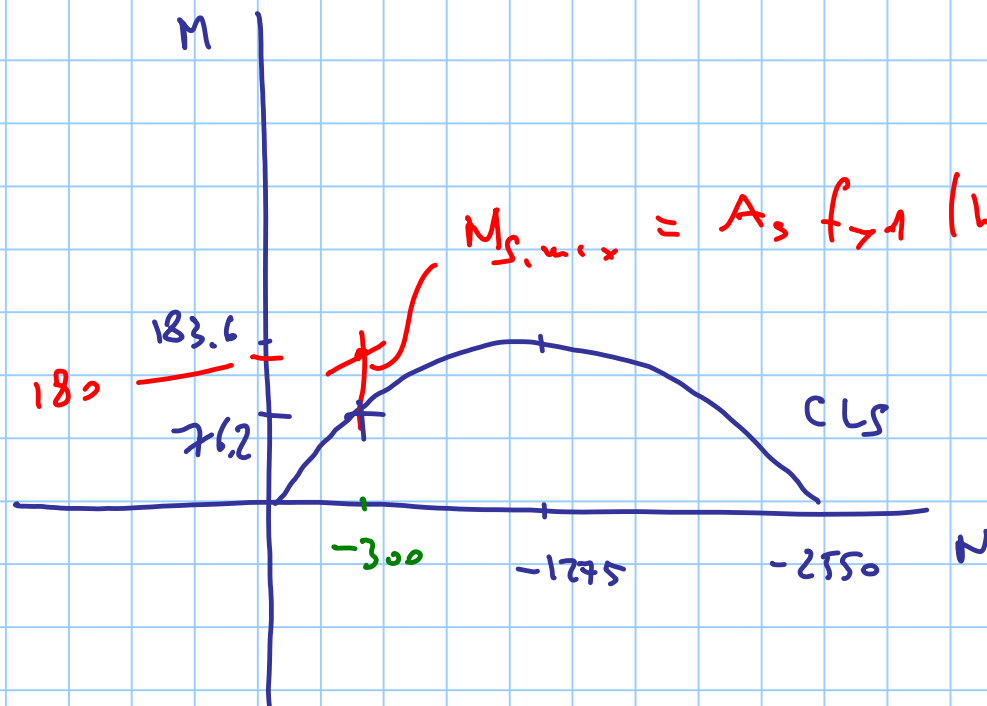
$$m = 1 + \frac{1}{1 + 2 N_{s,max} / N_{c,max}} = 1 + \frac{1}{1 + 2 \times 939 / 2551} = 1.576$$

$$M_{RA} = (M_{c,max} + M_{s,max}) \left[1 - \left| \frac{N_{rd} + \nu_n N_{c,max}}{\nu_n N_{c,max} + N_{s,max}} \right|^m \right] =$$

$$= \underbrace{(183.6 + 244.2)}_{427.8} \left[1 - \underbrace{\left| \frac{-1300 + 0.5 \times 2551}{0.5 \times 2551 + 939} \right|^{1.576}}_{0.959} \right] = 427.4 \text{ kNm}$$

$$N_{E1} = -300 \text{ kN}$$

$$M_{R1} = \underbrace{(183.6 + 244.2)}_{427.8} \left[1 - \underbrace{\left| \frac{-300 + 0.5 \times 2551}{0.5 \times 2551 + 939} \right|^{1.576}}_{0.725} \right] = 310.3 \text{ kNm}$$



$$A_s = \frac{\Delta M}{(h - 2c) f_{yd}} = \frac{103.8 \times 10}{0.52 \times 391.3} = 5.1 \text{ cm}^2$$

sol CLS

$$M_{Rd} = M_{s,max}$$

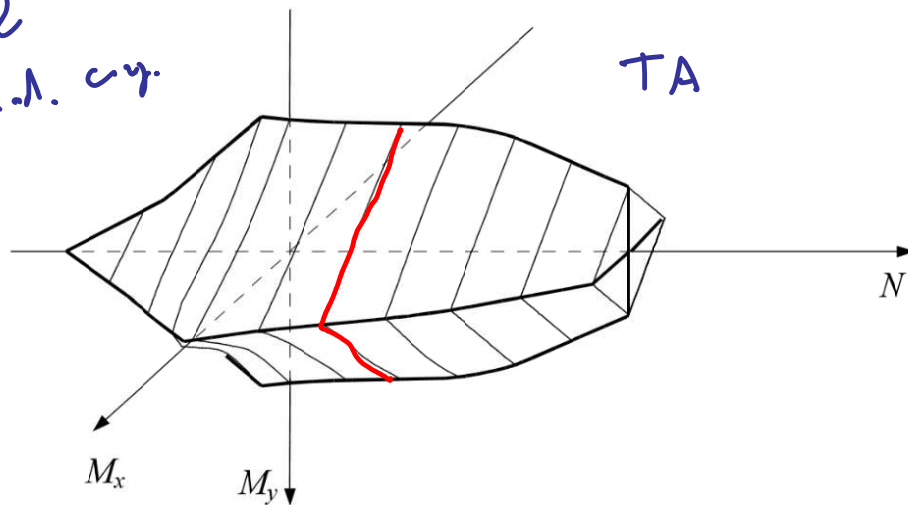
$$\Delta M = 180 - 76.2 = 103.8 \text{ kNm}$$

$$= 183.6 \left[1 - \left(\frac{-300 + 1275}{1275} \right)^2 \right] = 76.2 \text{ kNm}$$

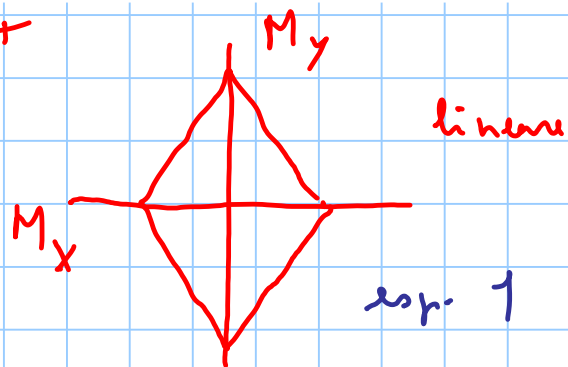
FLESSIONE COMPOSTA DEVIATA

N, M_x, M_y

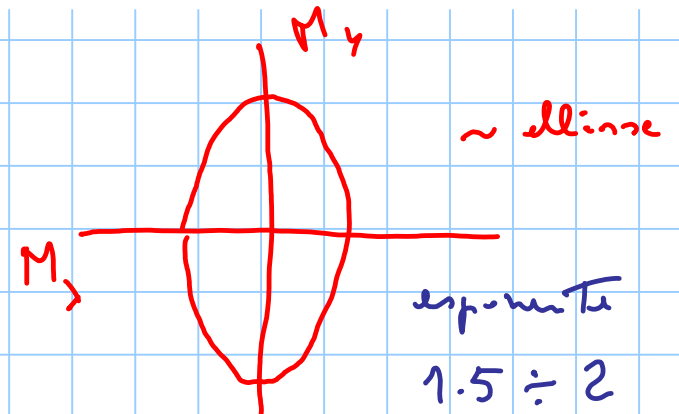
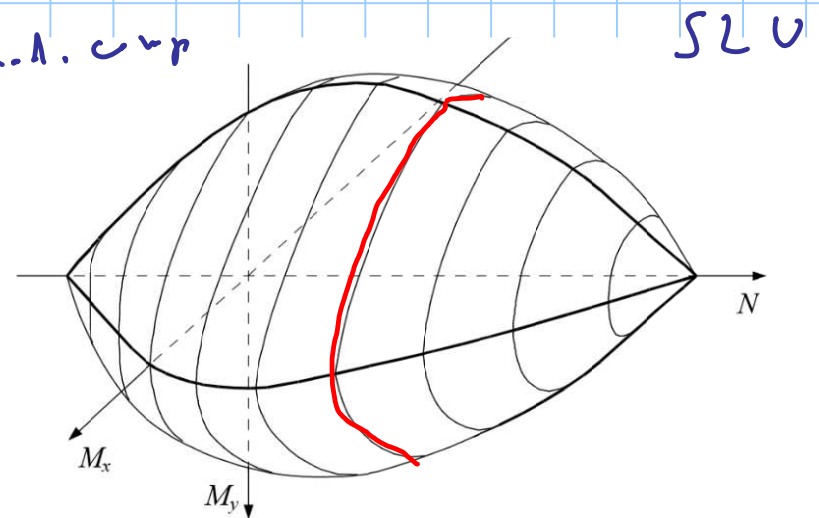
2°
m.l. c.y.



$N = \text{cost}$



3°
m.l. c.y.p



$$\left[\frac{M_{x,Ed}(N)}{M_{x,Rd}(N)} \right]^p + \left[\frac{M_{y,Ed}(N)}{M_{y,Rd}(N)} \right]^p \leq 1$$

$p = 1$ per 2° mod. comp.

$p = 1.5 \div 2$ per 3° mod. comp.

usare 1.5 cautelativamente

