

Spoleto
06049 PG
42.754215, 12.731721

distanza da mare 120 km
quota 286 m
zone in vento = 3
classe di ingombro = D

ZONE 1,2,3,4,5					
	costa mare	2 km	10 km	30 km	500m 750m
A	--	IV	IV	V	V
B	--	III	III	IV	IV
C	--	*	III	III	IV
D	I	II	II	II	III
* Categoria II in zona 1,2,3,4 Categoria III in zona 5					
** Categoria III in zona 2,3,4,5 Categoria IV in zona 1					

ZONE 1,2,3,4,5

	2 km	10 km	30 km	500m	750m	
A	--	IV	IV	V	V	V
B	--	III	III	IV	IV	IV
C	--	*	III	III	IV	IV
D	I	II	II	II	III	**

* Categoria II in zona 1,2,3,4
Categoria III in zona 5

** Categoria III in zona 2,3,4,5
Categoria IV in zona 1

classe di ingegneria II

per calcolo c_e

$$K_2 = 0.19$$

$$Z_o = 0.05$$

$$Z_{msn} = 4 \text{ m}$$

Tab. 3.3.I - Valori dei parametri $v_{b,0}$, a_0 , k_s

Zona	Descrizione	$v_{b,0}$ [m/s]	a_0 [m]	k_s
1	Valle d'Aosta, Piemonte, Lombardia, Trentino Alto Adige, Veneto, Friuli Venezia Giulia (con l'eccezione della provincia di Trieste)	25	1000	0,40
2	Emilia Romagna	25	750	0,45
3	Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la provincia di Reggio Calabria)	27	500	0,37
4	Sicilia e provincia di Reggio Calabria	28	500	0,36
5	Sardegna (zona a oriente della retta congiungente Capo Teulada con l'Isola di Maddalena)	28	750	0,40
6	Sardegna (zona a occidente della retta congiungente Capo Teulada con l'Isola di Maddalena)	28	500	0,36
7	Liguria	28	1000	0,54
8	Provincia di Trieste	30	1500	0,50
9	Isole (con l'eccezione di Sicilia e Sardegna) e mare aperto	31	500	0,32

zona 3

$$v_{b,0} = 27 \text{ m/s}$$

$$a_0 = 500 \text{ m}$$

$$k_s = 0.37$$

$$q_{nota} = 286 \text{ m} < 500 \text{ m} \rightarrow v_b = 27 \text{ m/s}$$

$$q_2 = \frac{1}{2} \rho v_b^2 = \frac{1}{2} \times 1.25 \times 27^2 = 456 \text{ N/m}^2 = 0.456 \text{ kN/m}^2$$

$$z_{\min} = 4 \text{ m}$$

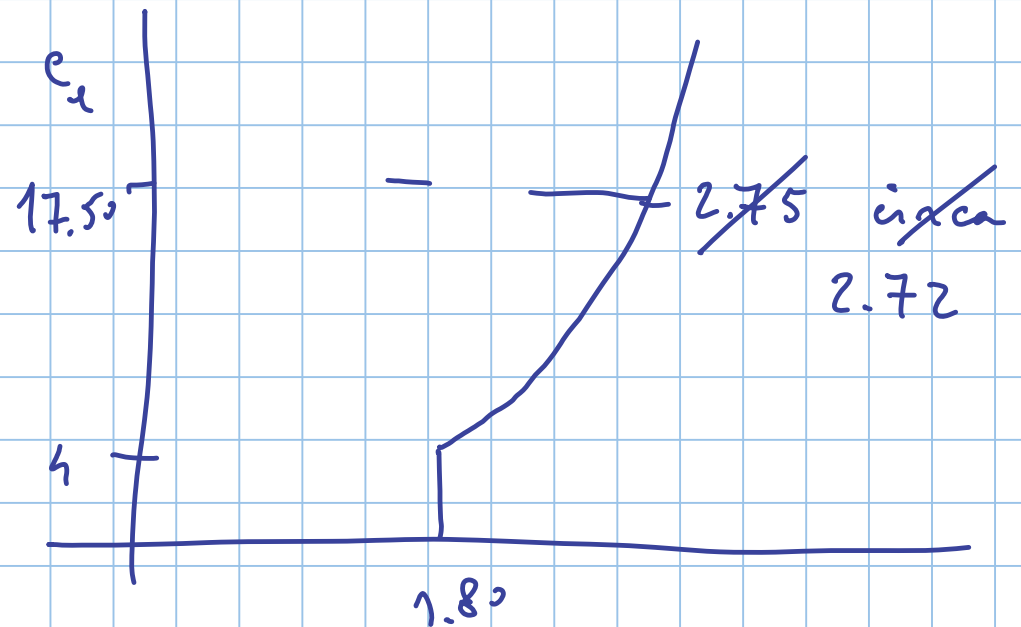
$$K_2 = 0.19$$

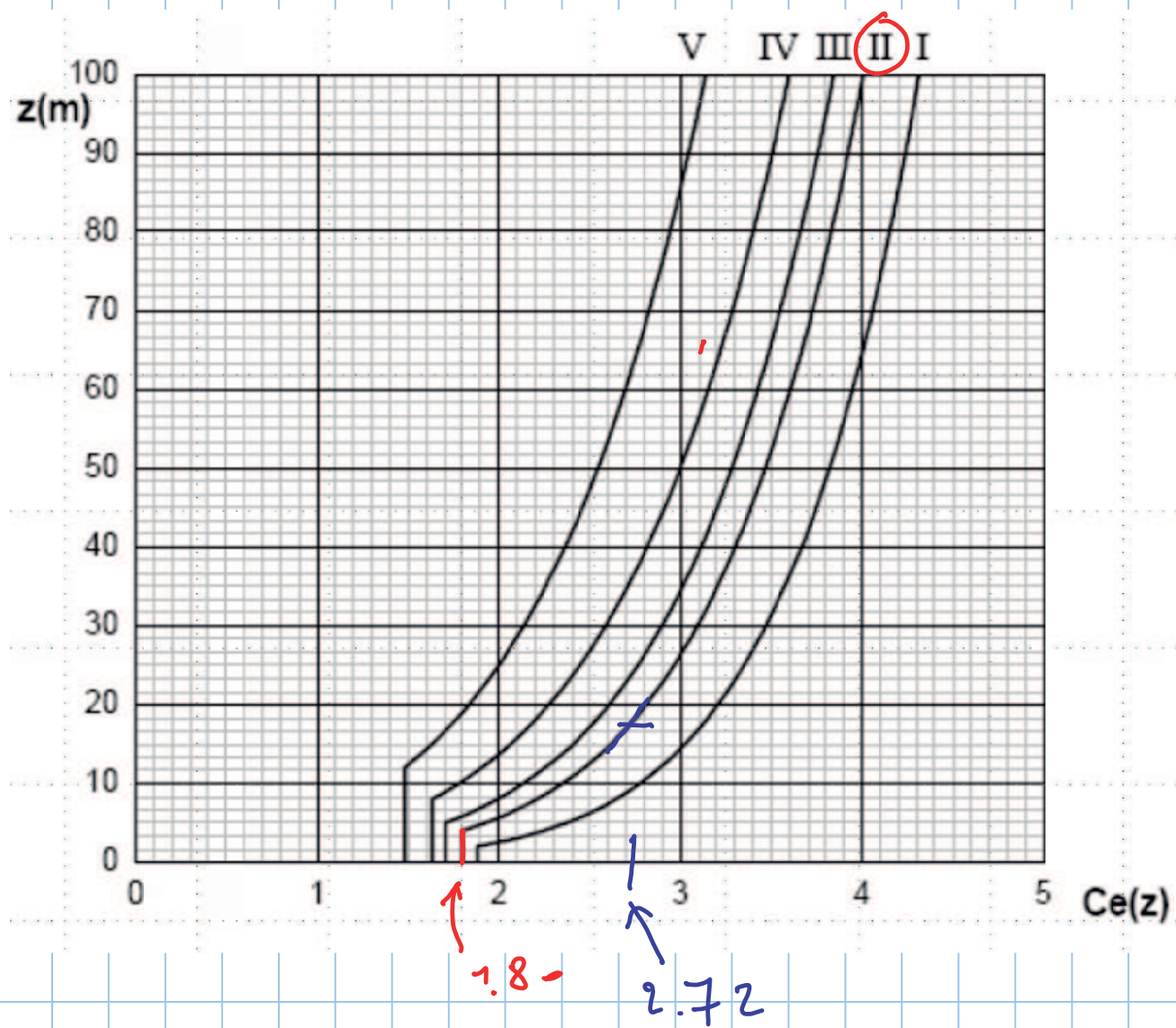
$$z_0 = 0.05$$

$$c_e(z) = K_r^2 c_t \ln\left(\frac{z}{z_0}\right) \left[7 + c_t \ln\left(\frac{z}{z_0}\right) \right] \text{ per } z \geq z_{\min}$$

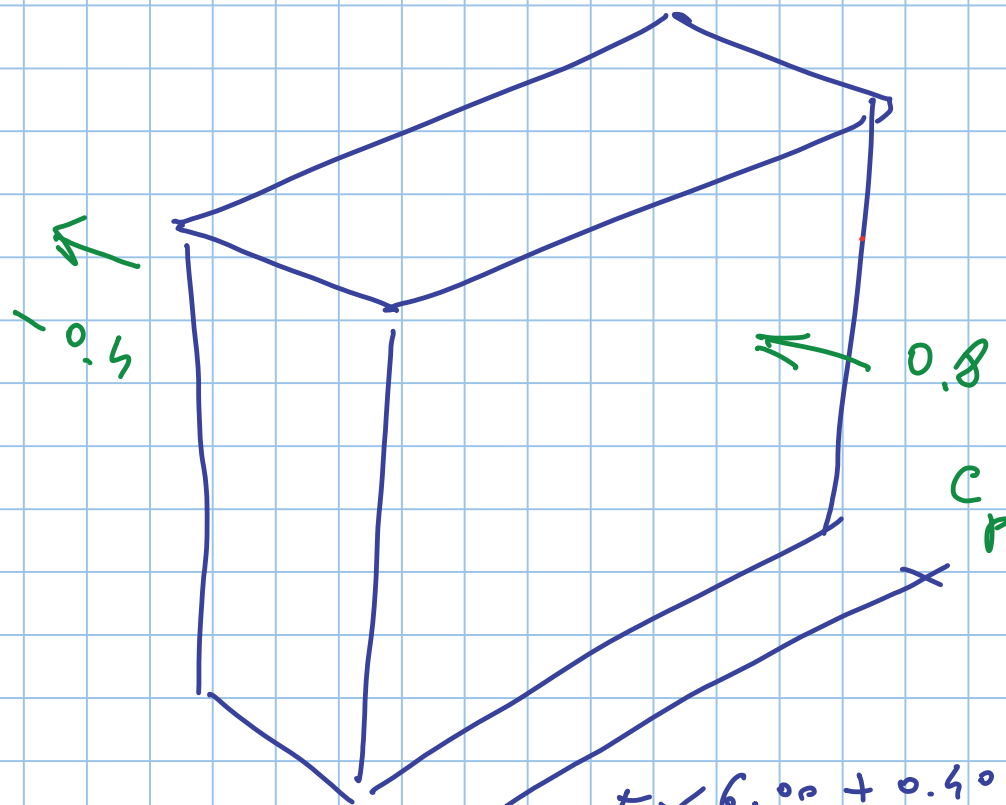
$$c_t = 1$$

$$c_e(z_{\min}) = 0.19^2 \underbrace{\ln\left(\frac{4}{0.05}\right)}_{4.38} \left[7 + \ln\left(\frac{4}{0.05}\right) \right] = 1.80$$





AZIONE sull'edif.

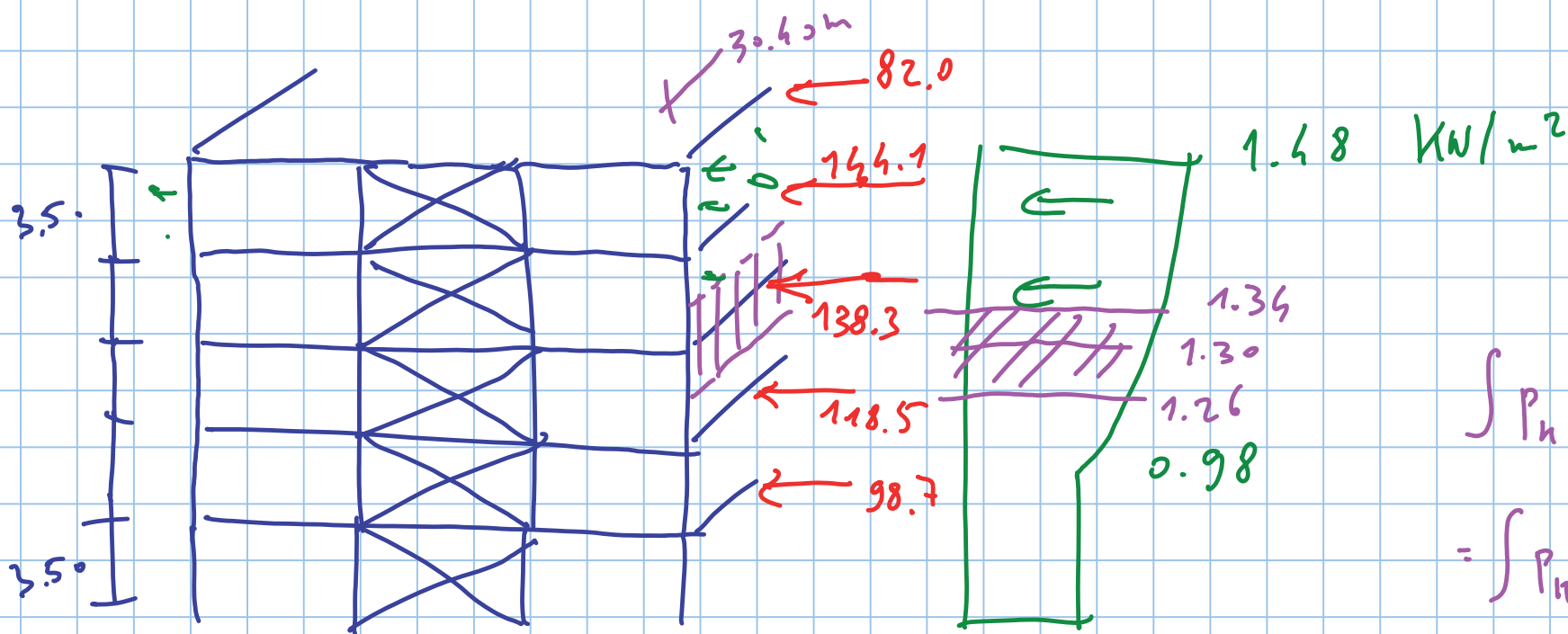


$$L_2 = 1.00 \text{ m}$$

$$5 \times 6.00 + 0.40 = 30.40 \text{ m}$$

A hand-drawn diagram of a vertical rectangular prism with horizontal arrows pointing left, representing wind pressure. The diagram is labeled with a green 's'.

$$0.456 \times 2.72 \times 1.2 = 1.48 \text{ kW/m}^2$$
$$0.456 \times 1.80 \times 1.2 = 0.98 \text{ kW/m}^2$$



force component at 3° incident.

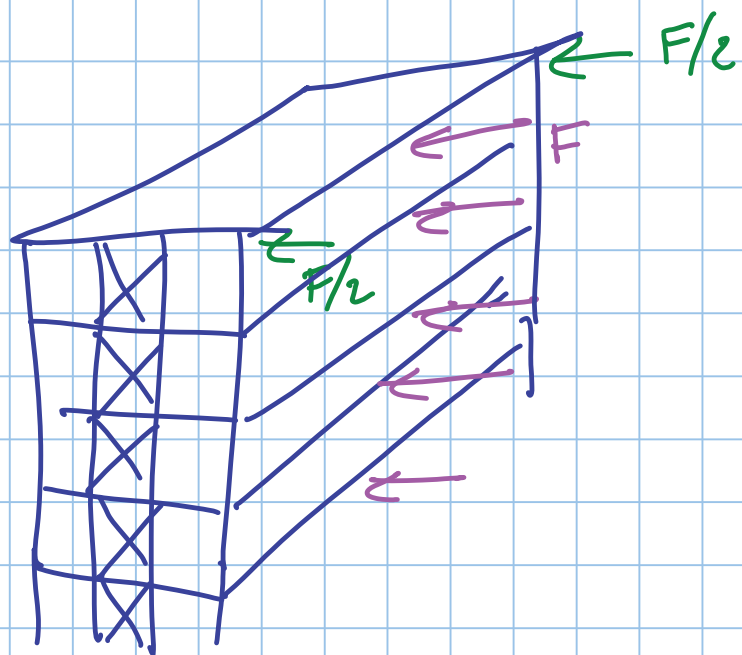
$$1.30 \times 30.40 \times 3.50 = 138.3 \text{ kN}$$

$$\int P_h dA =$$

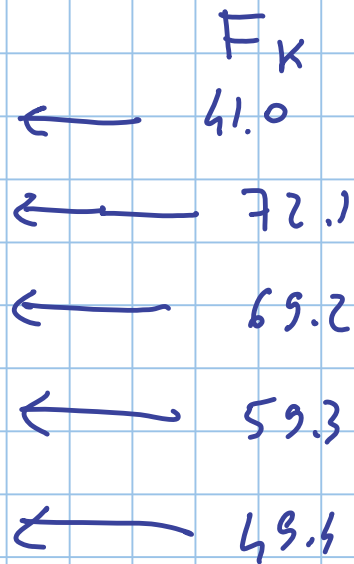
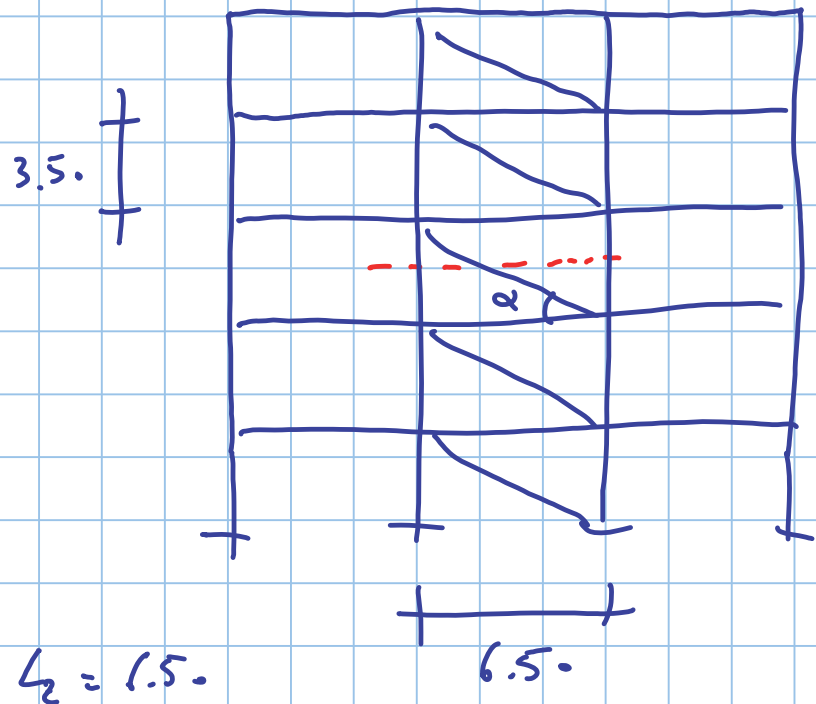
$$= \int P_h L dz =$$

$$= P_{k,med.} \cdot L \cdot \Delta z$$

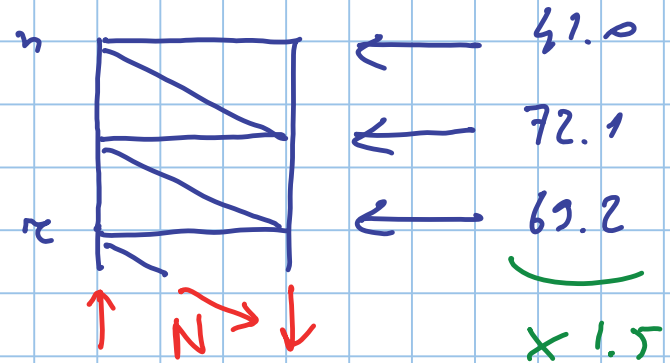
\uparrow
 3.50
 30.40



- ← 41.0
- ← 72.1
- ← 69.2
- ← 59.3
- ← 49.4



$$F_d = \gamma_F F_k = 1.5 F_k$$



Equilibrium

Translation horizontal

$$\sum_{i=1}^n F_i = N \cos \alpha$$

$$\alpha = \arctan \frac{3.50}{6.50} = 0.53 \text{ rad} = 28.3^\circ$$

$$\cos \alpha = 0.88$$

$$N = \frac{\sum F}{\cos \alpha} = \frac{41.0 + 72.1 + 69.2}{0.88} \times 1.5 = 207.2 \text{ kN}$$

DIMENSIONAMENTO

centrovento

$$N_{Ed} = \frac{310.8}{207.2} \text{ KN}$$

$$N_{Rd} = A \frac{f_y}{\gamma_{m0}} \quad \text{sempre}$$

acciaio S 275

$$f_y = 275 \text{ MPa}$$

$$N_{u,Rd} = 0.9 A_{nt} \frac{f_u}{\gamma_{m2}} \quad \text{in presenza di fori}$$

$$A \geq \frac{N_{Ed} \cdot \gamma_{m0}}{f_y} = \frac{\frac{310.8}{207.2} \times 10^3 \cdot 1.05}{275} = \frac{11.87}{7.91} \times 10^2 \text{ mm}^2$$

L 80 x 80 x 8

$$A = 12.3 \times 10^2 \text{ cm}^2$$

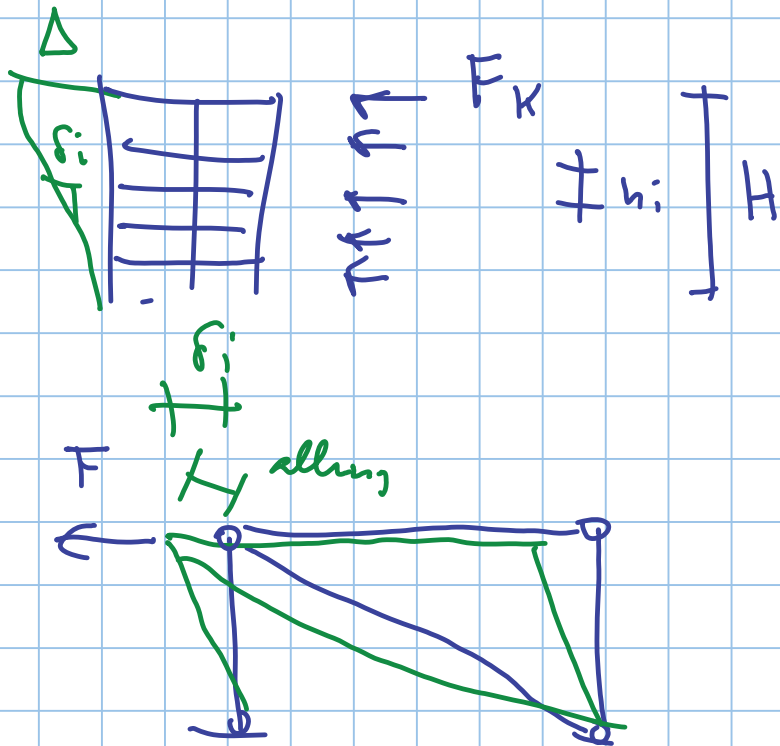
UPE 100

$$A = 12.5 \times 10^2 \text{ cm}^2$$

LIMITI DI DEFORMAZIONE

SLE

~ K_0 i carichi di servizio.



$$\frac{\Delta}{H} \leq \frac{1}{500}$$

$$\frac{\delta_i}{h_i} \leq \frac{1}{300}$$

$$E = 210000 \text{ MPa}$$

!

Cari chi variabili differenti

$$q_{1k}$$

$$q_{2k}$$

$$q_{1k} + \psi_0 q_{2k}$$

opp.

$$\psi_0 q_{1k} + q_{2k}$$

COMPRESSIONE

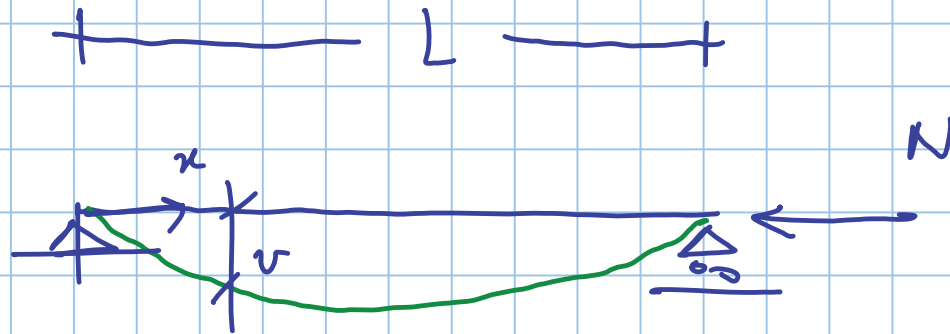
elastica

↳ non cambia
in p.e. e Tensione

$$N_{kd} = A \frac{f_y}{\gamma_{mo}}$$

plastica

↳ instabilità



$$M = N v(x)$$

$$v(x)$$

$$-\frac{M(x)}{EI} = v''(x)$$

$$M = -EI v''$$

$$-EI v'' = N v$$

$$EI v'' + N v = 0$$

$$v = K \sin \pi \frac{x}{L}$$

$$v'' = -K \frac{\pi^2}{L^2} \sin \pi \frac{x}{L}$$

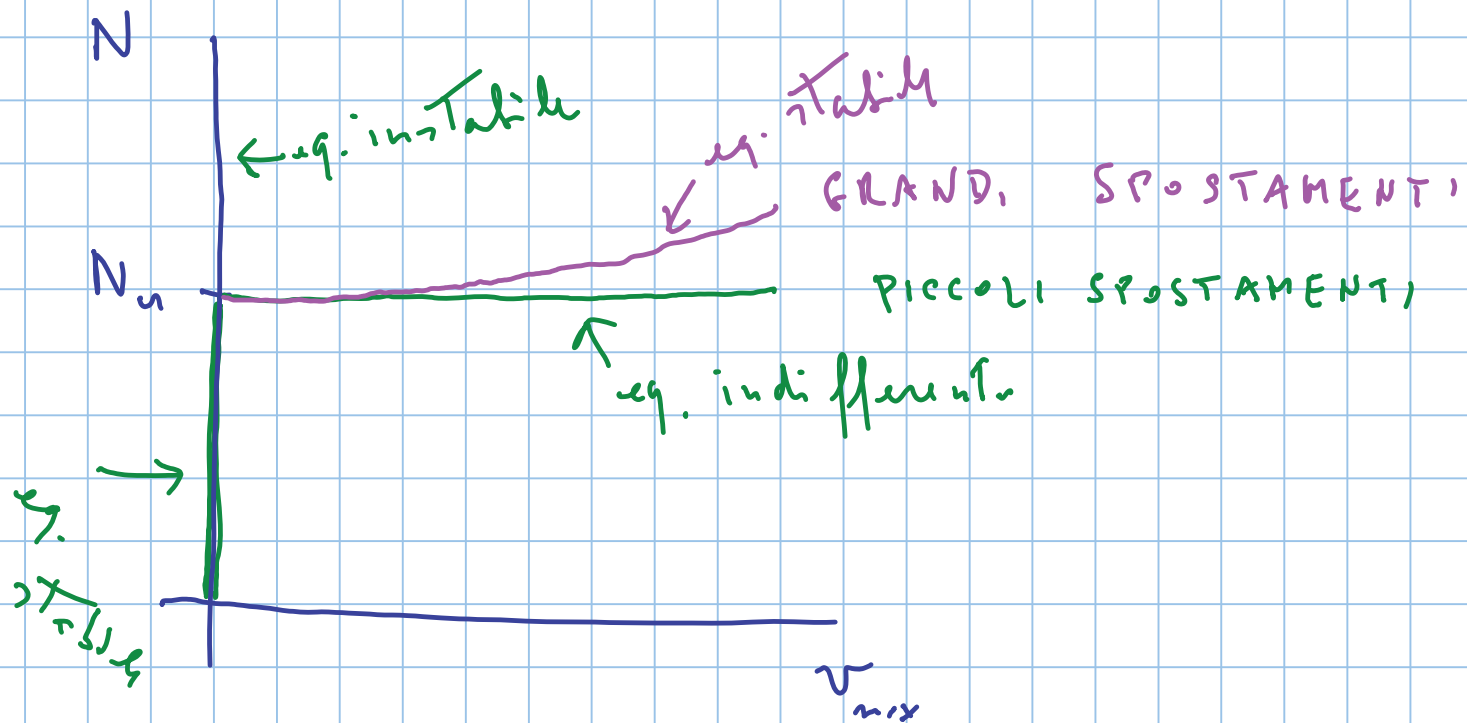
$$EI \left[-K \frac{\pi^2}{L^2} \sin \frac{\pi x}{L} \right] + N \left[K \sin \frac{\pi x}{L} \right] = 0$$

$$-\cancel{K} \frac{\pi^2 EI}{L^2} \cancel{\sin \frac{\pi x}{L}} + \cancel{K} N \cancel{\sin \frac{\pi x}{L}} = 0$$

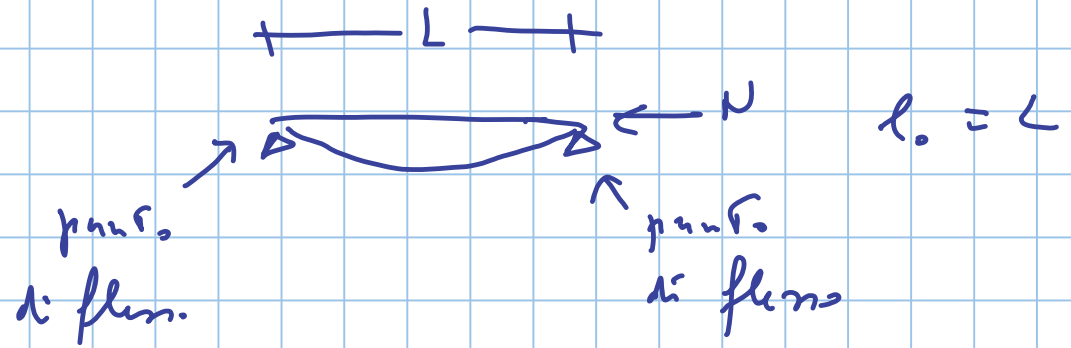
$$-\frac{\pi^2 EI}{L^2} + N = 0$$

$$N = \frac{\pi^2 EI}{L^2} = N_{cr}$$

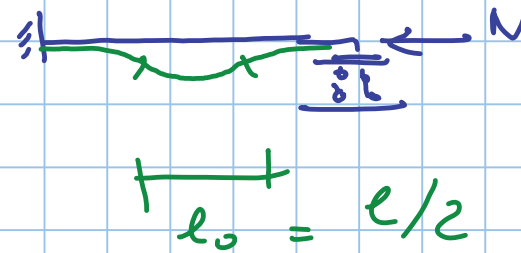
carico critico Euleroiano



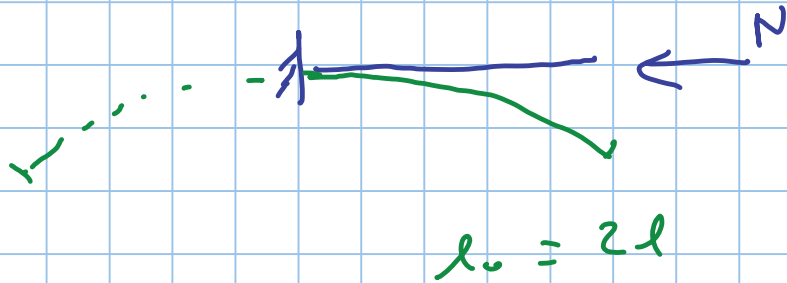
$$N_{cr} = \frac{\pi^2 EI}{l_0^2}$$



$$\sigma_{cr} = \frac{N_{cr}}{A} = \frac{\pi^2 EI}{l_0^2 A}$$



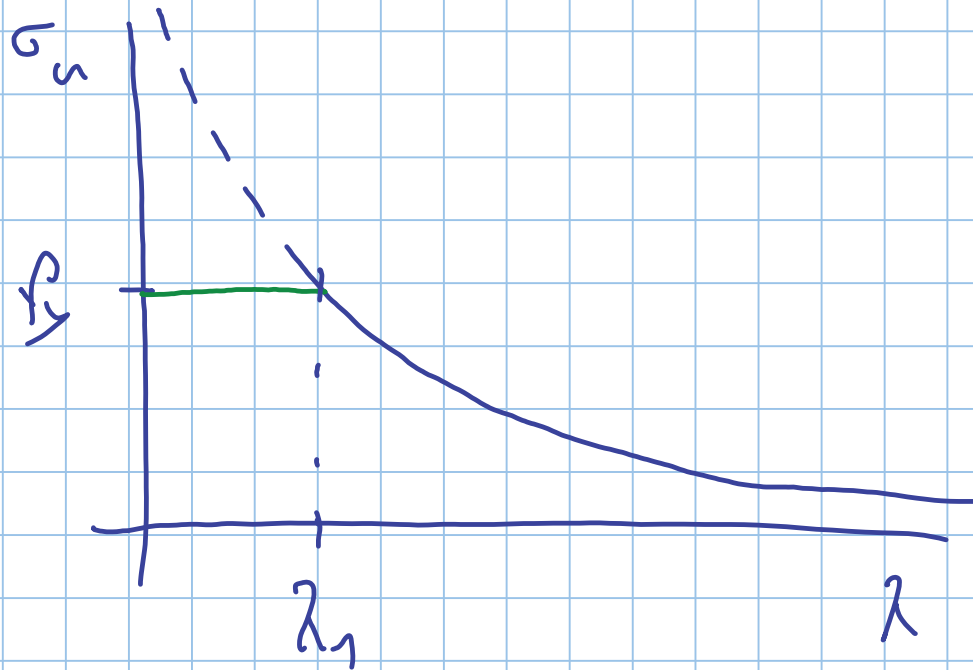
$$\sqrt{\frac{I}{A}} = i \quad \text{raggi d'inertia.}$$



$$\sigma_{cr} = \frac{\pi^2 E i^2}{l_0^2}$$

$$\lambda = \frac{h_0}{i}$$

SNELLEZZA



$$\sigma_n \sim \frac{\pi^2 E}{\lambda^2}$$



$\lambda < \lambda_1$ tozzze

$\lambda > \lambda_1$ snelle

$$\sigma_{cr} = \frac{\pi^2 E}{\lambda^2} \rightarrow$$

$$f_y = \frac{\pi^2 E}{\lambda_1^2} \rightarrow$$

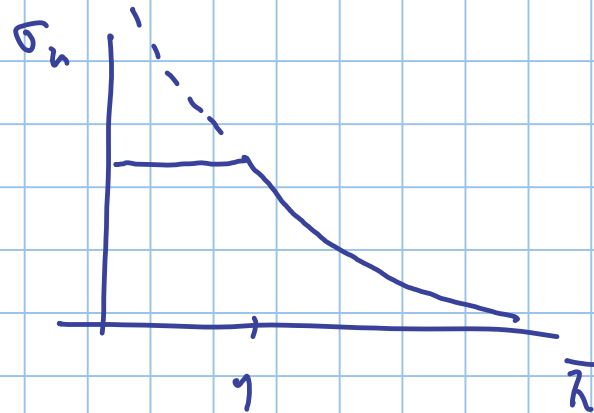
$$\lambda_1 = \pi \sqrt{\frac{E}{f_y}}$$

S 235

$$f_y = 235 \text{ MPa}$$

$$\lambda_1 = 93.9$$

$$\bar{\lambda} = \frac{\lambda}{\lambda_1}$$

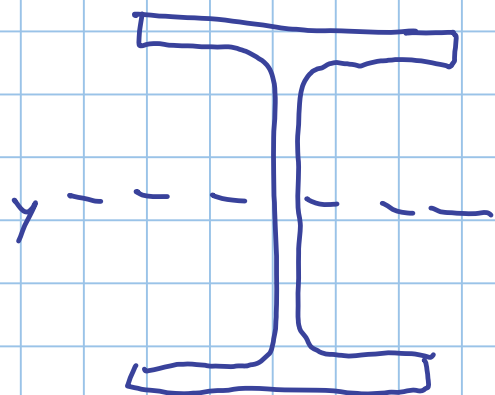


$$\bar{\lambda} = \sqrt{\frac{N_{cr}}{N_{cr}}}$$

$$\lambda = \pi \sqrt{\frac{E}{\sigma_s}}$$

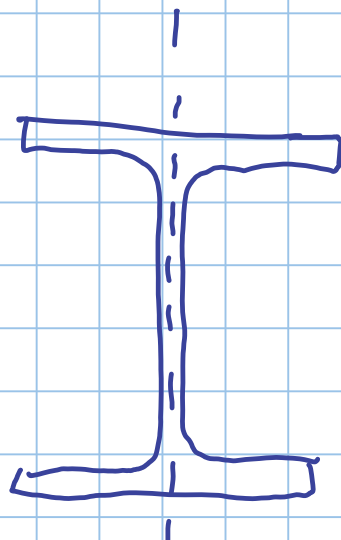
$$\lambda_1 = \pi \sqrt{\frac{E}{f_y}}$$

$$\frac{\lambda}{\lambda_1} = \sqrt{\frac{f_y A}{\sigma_s A}} = \sqrt{\frac{N_{cr}}{N_{cr}}} =$$



I_y

i_y



I_z

i_z