Titolo nota 17/10/2018

RESILIENZA

prova: pendolo di Charpy

per temperature molto basse

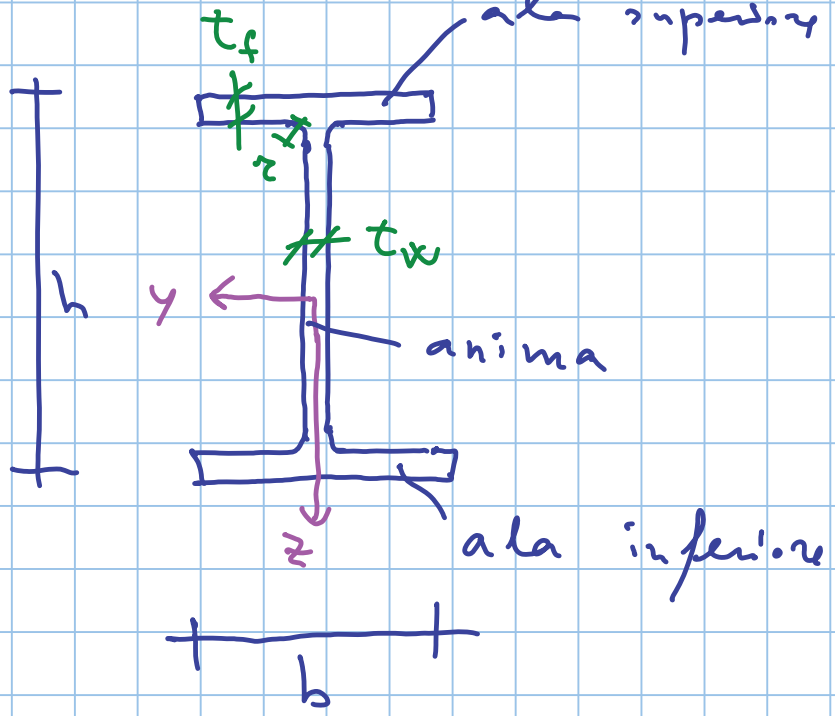
RESISTENZA al fuoco

la alla corrosione
(zincatura)

ELEMENTI IN ACCIAIO

formati a caldo

doppio T



$t_w < t_f$

flange = ala

web = anima

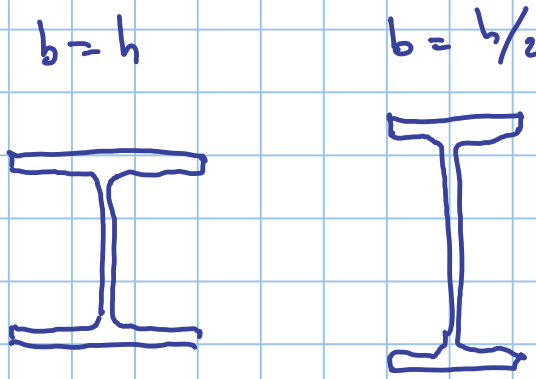
A = area

I = momento d'inerzia

$I_y > I_z$

i P.T. non nel

SAGOMARIO



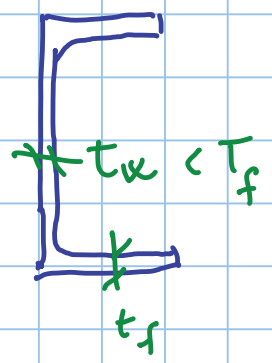
HE IPE

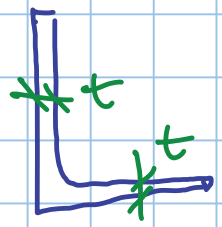
$$N = \int \sigma \, dA$$

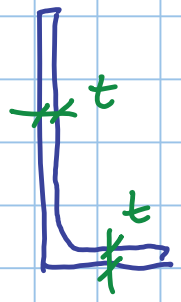
$$M_y = \int \sigma \, y \, dA$$

$$V_z = \int_{anima} \tau_{zx} \, dA$$

leggere	HE A 300	IPE A
bene	HE B 300 b = h = 300 mm	IPE 300 b = 150 mm h = 300 mm
pesanti	HE M 300	IPE O







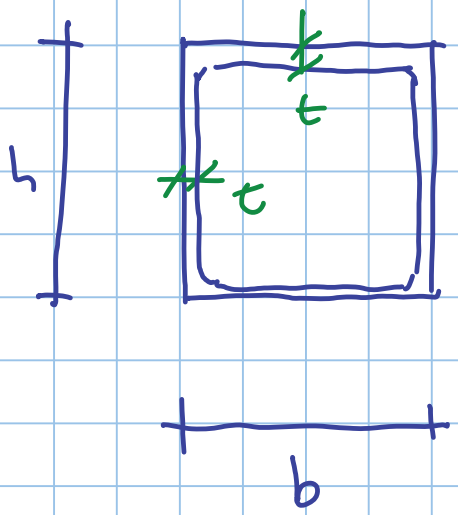
L

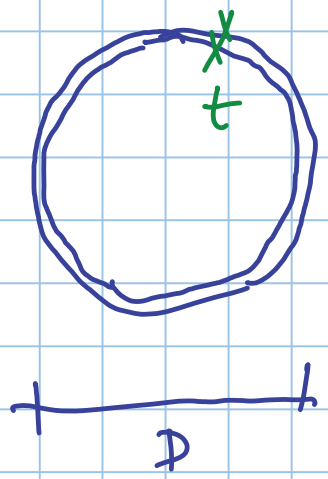
UPE 200

h: 200 mm b = 80 mm

UPN

L 120 x 80 x 10





raggio d'inerzia

$$i_y = \sqrt{\frac{I_y}{A}}$$

circolare, quadrato

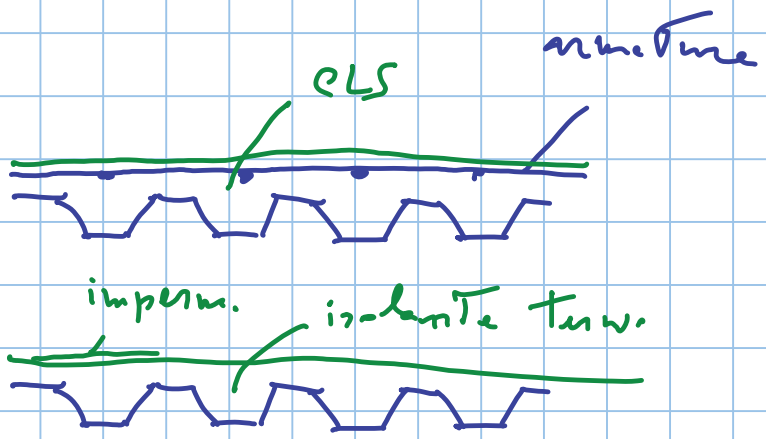
$$i_y = i_z$$

LAMIERE → piatti per collegamenti

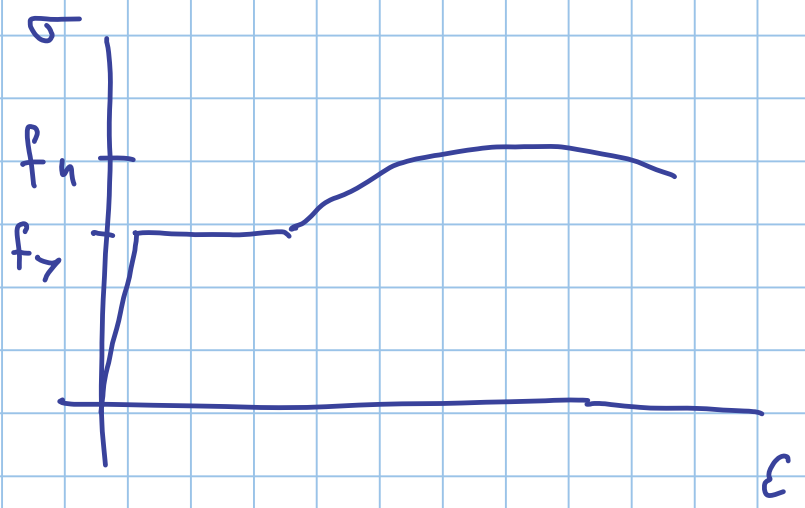
→ sezioni composte non standard

LAMIERE SOTTILI piegate a freddo

→ lamiere grecate



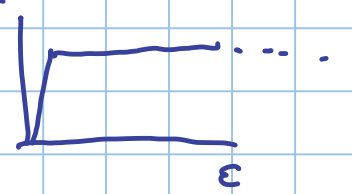
→ profili standard.



riferimento:

f_y nelle verifiche di agTe

$\gamma_M = 1.05$

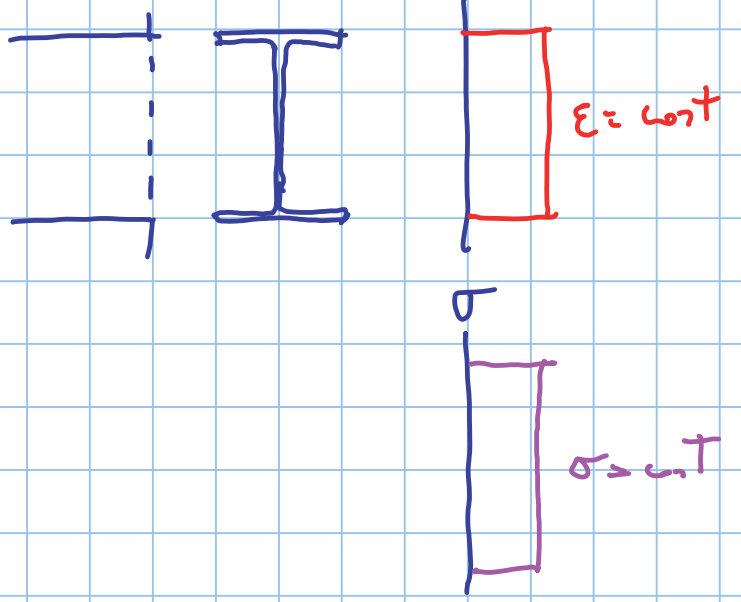


f_u verifiche localizzate

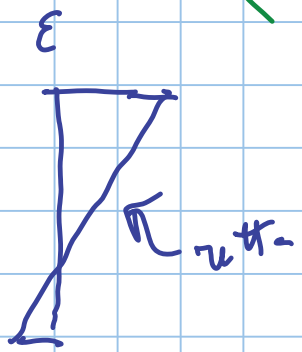
$\gamma_M = 1.25$

SFORZO NORMALE N — Trazione

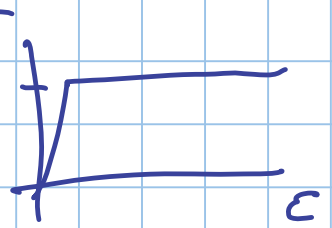
ASTA



$N_{Rd} = A \frac{f_y}{\gamma_{M0}}$



σ-ε elastico - perfett. plastico



mantenimento sezioni piane

$$\varepsilon = \underbrace{\varepsilon_G}_{\text{costanti}} + \underbrace{\frac{\partial \varepsilon}{\partial y}}_{\text{costanti}} y + \underbrace{\frac{\partial \varepsilon}{\partial z}}_{\text{costanti}} z$$