

tensioni normali  $\sigma$   
tangenziali  $\tau$

snervamento (acciaio) yielding  $\sigma_y$

resistenza: simbolo  $f$  resist. a snervamento  $f_y$

valore caratteristico di resistenza: pedice  $k \rightarrow f_{yk}$

calcestruzzo  $f_{ck}$

# CARICHI

statici — dinamici

permanenti

$g$

— variabili

$q$

$q_k$  [ raro  
frequente  
quasi permanente ]

fattile 95%  
dei massimi  
nelle vite d. strutture

medio nel tempo

— strutturali

— non strutturali  
(parimento, intonaco)  
trasmissione

— definiti forfaitariamente  
tenenza

[ compiutamente definiti  
definiti genericamente ]

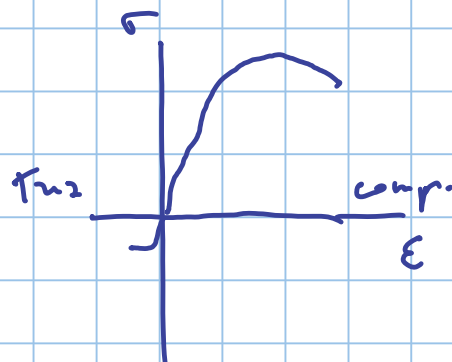
$g_k$

valore  
nominale

fattile 95%

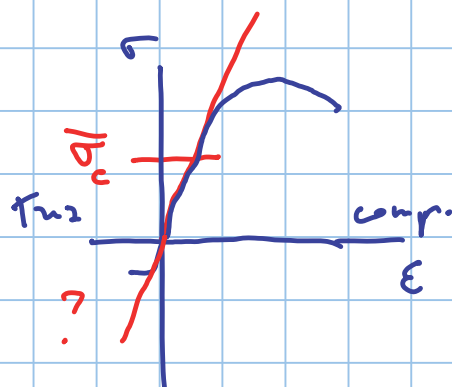
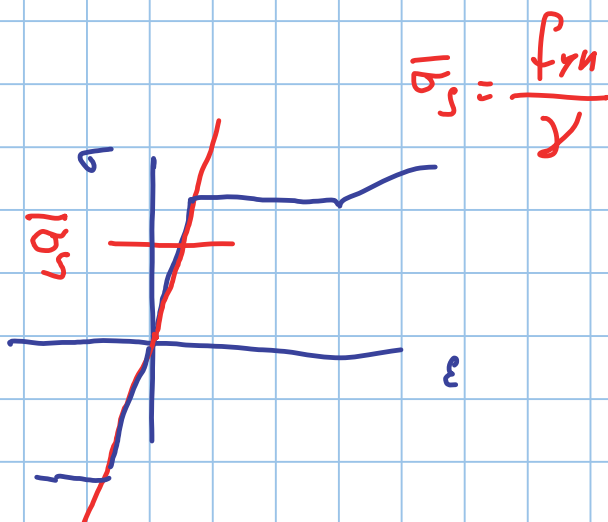
# ANALISI STRUTTURALE E VERIFICHE

ACC



CLS

ACC



CLS

modello lineare

tensioni ammissibili

resist. a trazione?

NO

$g_k$   $q_k$

METODO DELLE TENSIONI AMMISSIBILI

## CALCOLO A ROTTURA

date le resistenze dei materiali ( $f_{yk}$ ,  $f_{ck}$ )

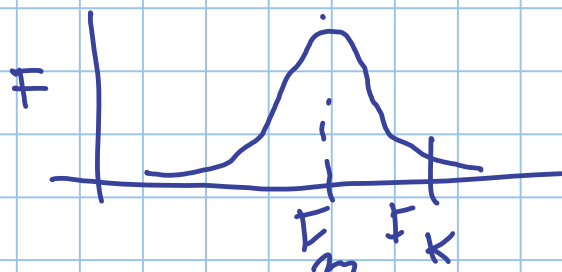
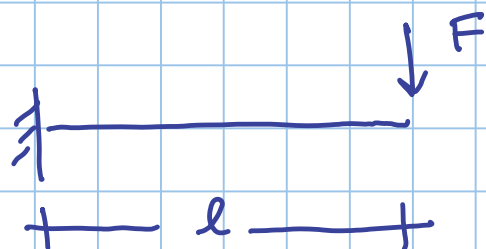
calcolare il valore del carico che porta a collasso

applicare coeff. sicurezza al carico

$$\frac{Q_k}{\gamma}$$

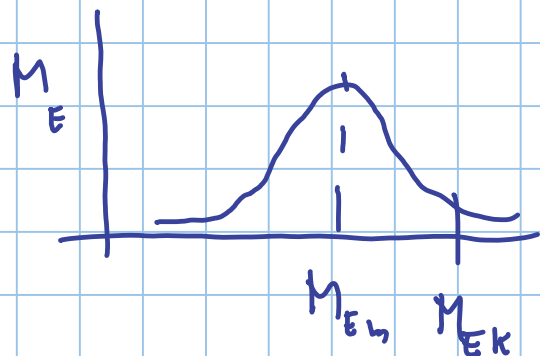
## METODO SEMIPROBABILISTICO

### AGLI STATI LIMITE



$$M_E = F l$$

momento  
flexante  
solicitante

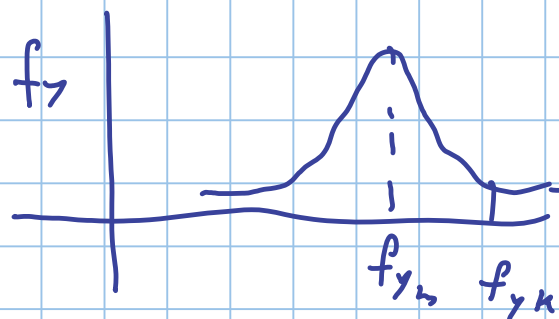


$$I \quad f_y$$

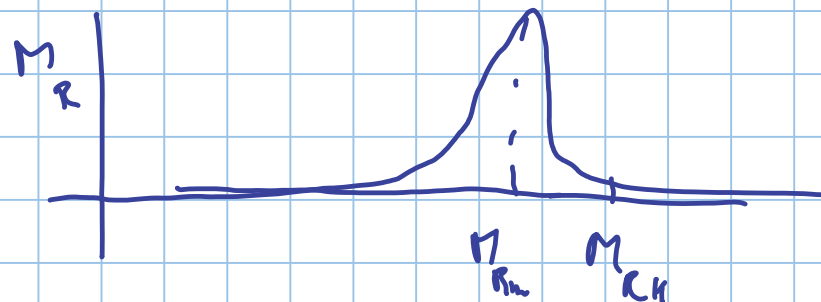
$$\sigma = \frac{M}{I} y$$

$$\sigma_{max} = \frac{M}{W}$$

$$W = \frac{I}{y_{max}}$$



$$M_R = f_y W$$



CARICO

$$g_d = \gamma_g g_k$$

$$\gamma_g > 1$$

RESISTENZA

$$f_d = \frac{f_k}{\gamma_n}$$

$$\gamma_n > 1$$

con legge costitutivo non lineare