

$$\gamma_{m0} = \gamma_{m1} = 1.05$$

$$\gamma_{m2} = 1.25$$

TRAZIONE

VERIFICA

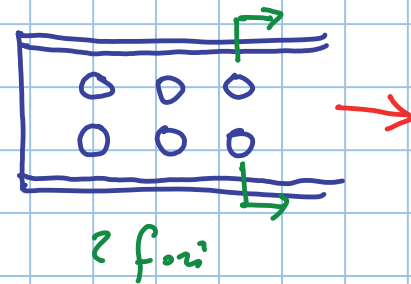
$$N_{Rd,pl} = A \frac{f_y}{\gamma_{m0}}$$

PROGETTO

$$A \geq \frac{N_{Ed} \gamma_{m0}}{f_y}$$

in presenza di fori

$$A_{net} = A - \sum d \cdot t$$



$$N_{Rd,n} = 0.9 A_{net} \frac{f_u}{\gamma_{m2}}$$

dunque

$$N_{Rd,n} > N_{Rd,pl}$$

$$\frac{A_{net}}{A} > \frac{f_y / \gamma_{m0}}{0.9 f_u / \gamma_{m2}}$$

# COMPRESSIONE

classi 1, 2, 3

ASTA

VERIFICA

$$N_{b,Rd} = \chi A \frac{f_y}{\gamma_m}$$

$$\lambda = \frac{l_0}{i}$$

$$\bar{\lambda} = \frac{\lambda}{\lambda_1}$$

vedere  $\lambda_{max}$

seguire curva o coeff. imperf.

$\Downarrow$   
 $\chi$

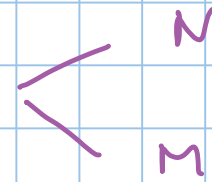
PROGETTO

$$A \geq \frac{N_{Ed} \gamma_{M1}}{f_y \chi}$$

ma  $\chi$  dipende dalle sezioni

CLASSIFICAZIONE

SEZIONI



dipende da  
distribuzione  
di tensioni

i limiti non differenziati

➤ per elementi vincolati — ad entrambi gli estremi  
— a un solo estremo

➤ diagramma delle tensioni — costante  
— variabile

# FLESSIONE SEMPLICE RETTA

VERIFICA

PROGETT.

$$M_{Rd} = W_{pl} \frac{f_y}{\gamma_{mo}}$$

classe 1, 2

$$W_{pl} \geq \frac{M_{Ed} \gamma_{mo}}{f_y}$$

$$W_{el} \frac{f_y}{\gamma_{mo}}$$

classe 3

l'asse neutro divide in due parti di area uguali

$$W_{pl} = 2 S_{y_{2ms}} \quad \text{rispetto a asse baricentrico}$$

contemporaneamente

SLE limiti fucina

$$I \geq I_{me}$$

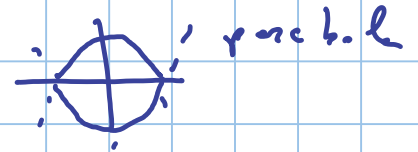
FLESSIONE

SEMPLICE

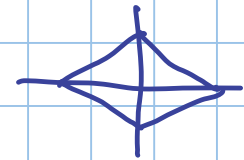
DEVIATA

$$\left( \frac{M_{Ed,y}}{M_{Rd,y}} \right)^2 + \left| \frac{M_{Ed,z}}{M_{Rd,z}} \right| \leq 1$$

per profilo I



$$\left| \frac{M_{Ed,y}}{M_{Rd,y}} \right| + \left| \frac{M_{Ed,z}}{M_{Rd,z}} \right| \leq 1$$

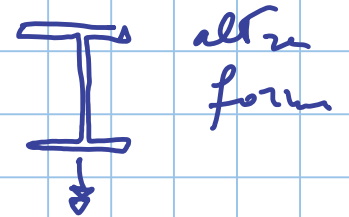
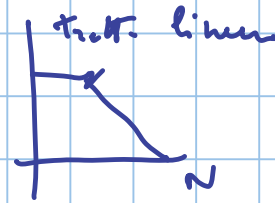
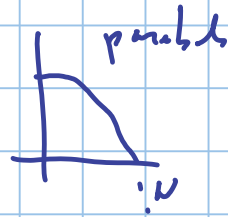
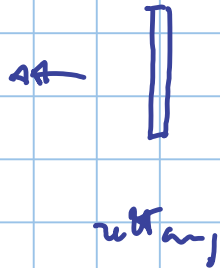


tenso  
FLESSIONE

COMPOSTA

RETTEA

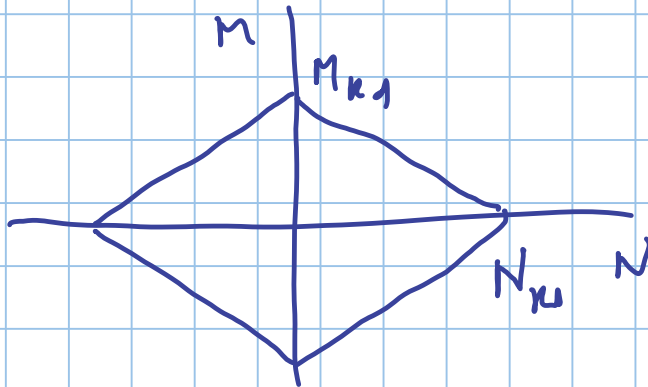
caso 1, 2



altra  
forma

DIPENDE DALLA FORMA DELLA SEZIONE

caso 3



$$\left| \frac{M_{Ed}}{M_{Rd}} \right| + \left| \frac{N_{Ed}}{N_{Rd}} \right| \leq 1$$