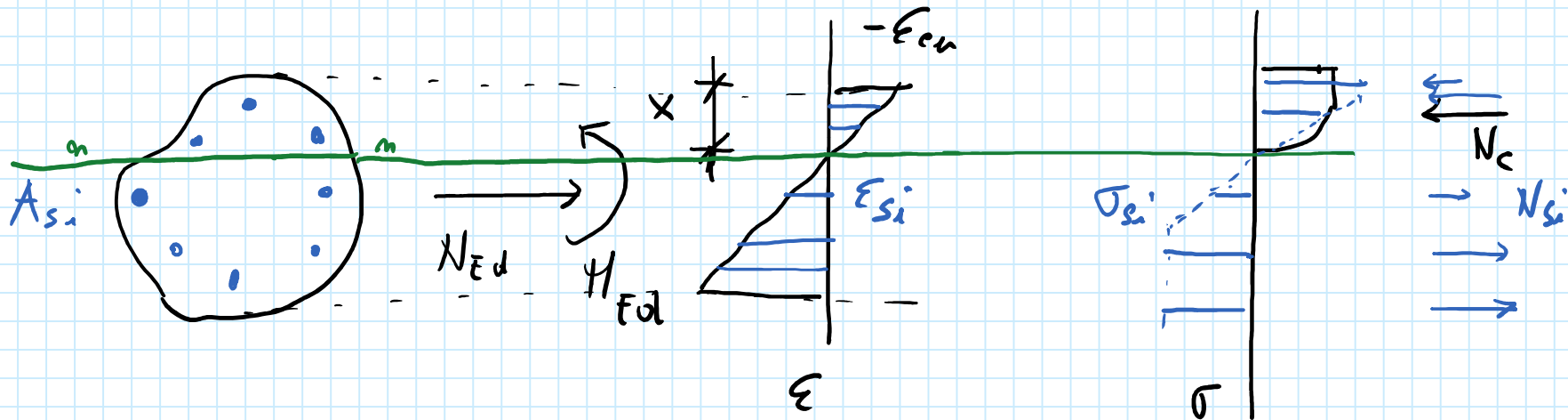


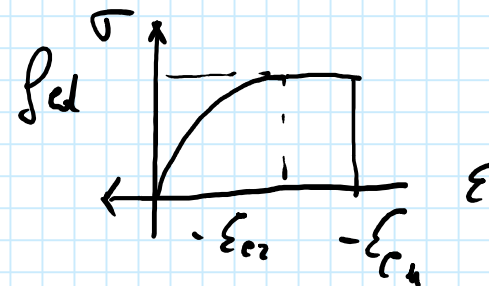
Flusso composto di trazione generata nel III stadio  
 caso delle trazioni parziali

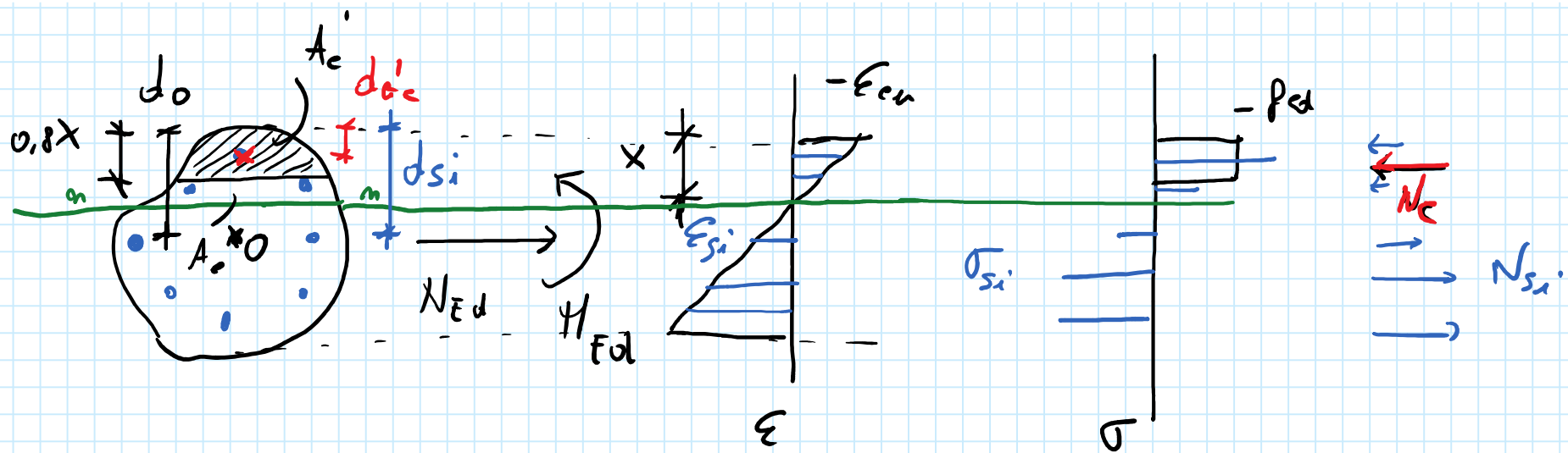


$$M_{Ed} \leq M_{Rd}(N_{Ed})$$

Legge  
 parabola - rettangolo

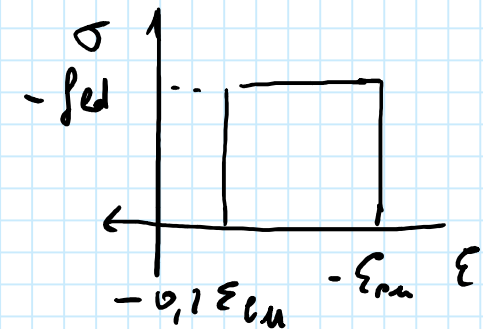
$$N_c = \int_{A_c} \sigma_c dA$$



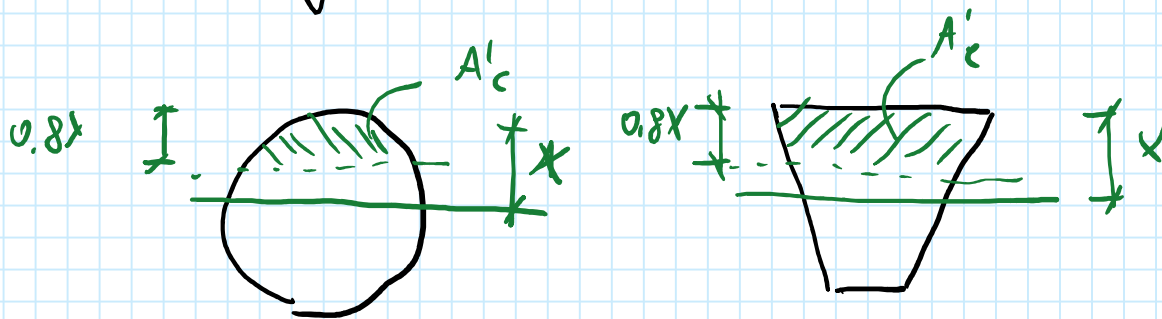


$$N_c = \int_{A_c} \sigma_c dA = \int_{A_c'} \sigma_c dA + \int_{A_c''} \sigma_c dA$$

$$= -A_c' f_{cd}$$



Se una la  
stura - block  
tutto alimen to  
diu semplice



$$-\frac{\epsilon_{em}}{x} = \frac{\epsilon_{si}}{ds_i - x} \Rightarrow \epsilon_{si} = \frac{ds_i - x}{x} \epsilon_{em}$$

$$\epsilon_{si} < -\epsilon_{yd} \quad \sigma_{si} = -f_{yd}$$

$$-\epsilon_{yd} < \epsilon_{si} < \epsilon_{yd} \quad \sigma_{si} = \frac{\epsilon_{si}}{\epsilon_{yd}} f_{yd}$$

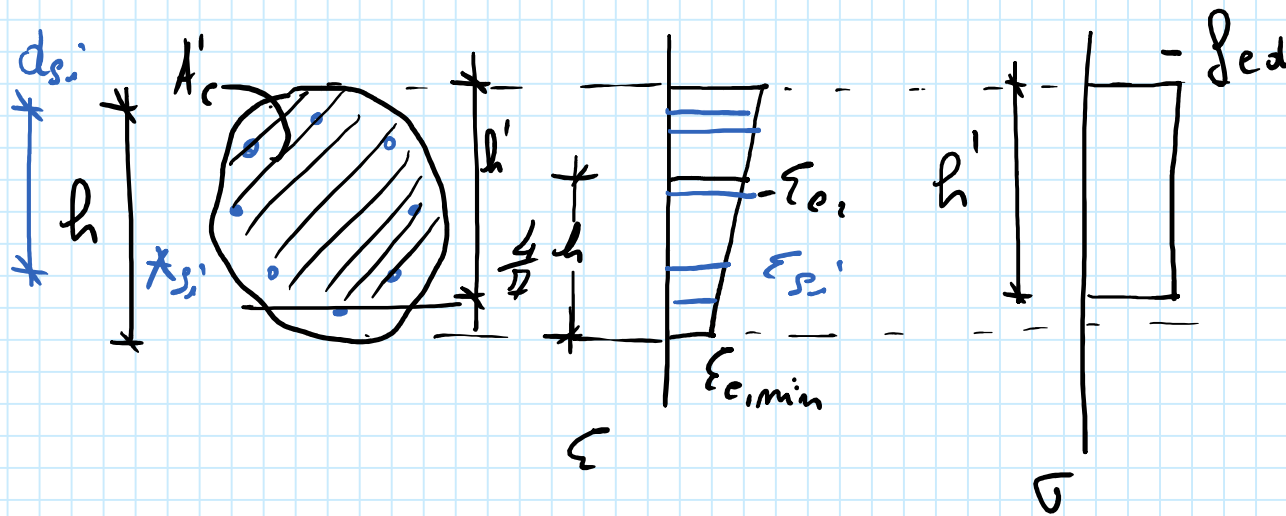
$$\epsilon_{si} > \epsilon_{yd} \quad \sigma_{si} = f_{yd}$$

$$N_{si} = A_s \sigma_{si}$$

$$N_c + \sum N_{si} = N_{fd} \Rightarrow x$$

Calcolo del momento resistente

$$M_{Rd}(N_{Ed}) = -N_c(d_o - d_{e'c}) - \sum N_{s,i}(d_o - d_{s,i})$$



Caso delle sezioni  
intereamente  
comprese

$$h' = \left[ 1 - 0,2(1 - \eta_{min})' \right] h$$

$$\eta_{min} = - \frac{\epsilon_{e,min}}{\epsilon_{e,2}}$$

$$N_c = -A'_c f_{cd}$$

$$\epsilon_{s,i} = - \left[ \frac{h - d_{s,i}}{\frac{1}{2} h} (1 - \eta_{min}) + \eta_{min} \right] \epsilon_{e,2} \Rightarrow \sigma_{s,i} \Rightarrow N_{s,i} = A_{s,i} \sigma_{s,i}$$

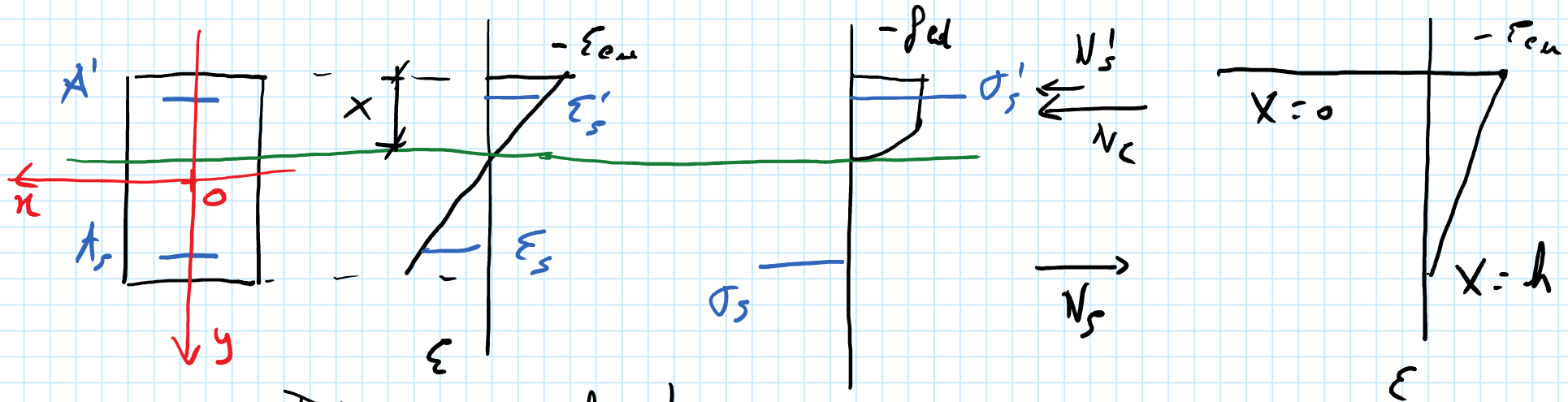
$$N_c + \sum N_{s,i} = N_{Ed} \Rightarrow \eta_{min}$$

Calculo del momento resistente

$$M_{Rd} = -N_c (d_o - d_{e'i}) - \sum N_{s_i} (d_o - d_{s_i})$$

$$= N_c (d_{e'i} - d_o) + \sum N_{s_i} (d_{s_i} - d_o)$$

# Costruzione dei diagrammi di resistenza e dello SLD



Diagrammi limite  
di deformazione

$$N = \int \sigma dA$$

$$H = \int \sigma y dA$$

||  
↓

$$N_e = - \beta b \times \int \epsilon_1$$

$$N'_s = A'_s \sigma'_s$$

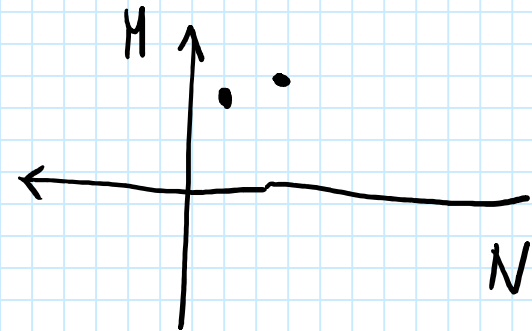
$$N_s = A_s \sigma_s$$

||  
↓

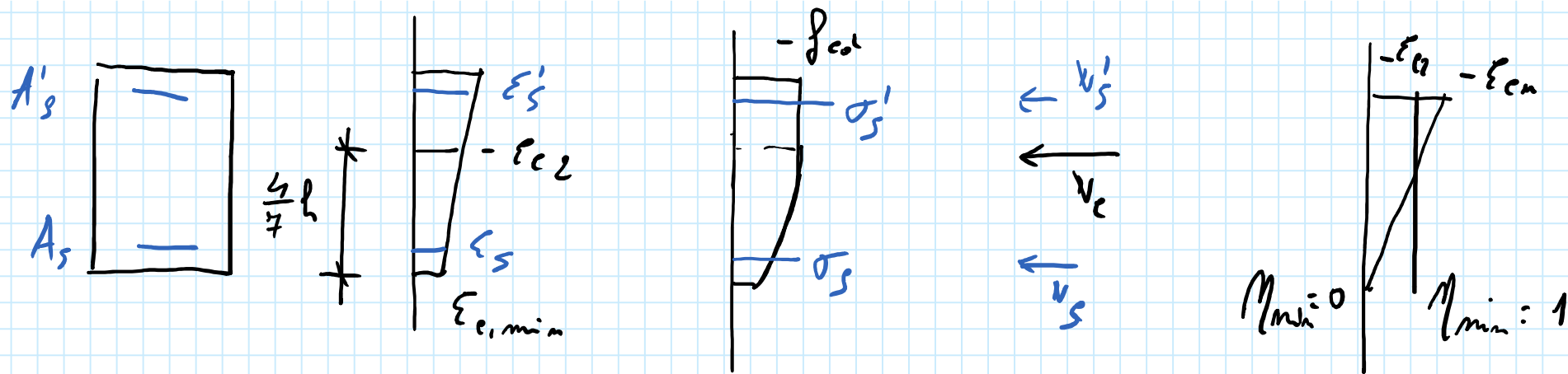
$$N = N_e + N'_s + N_s$$

$$H = -N_e \left( \frac{b}{2} - \kappa X \right) + (A_s \sigma_s - A'_s \sigma'_s) \left( \frac{b}{2} - c \right)$$

⇒

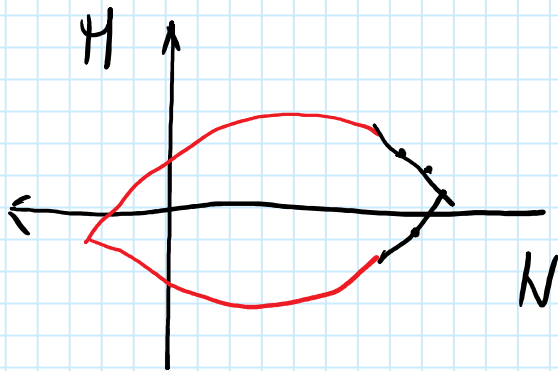






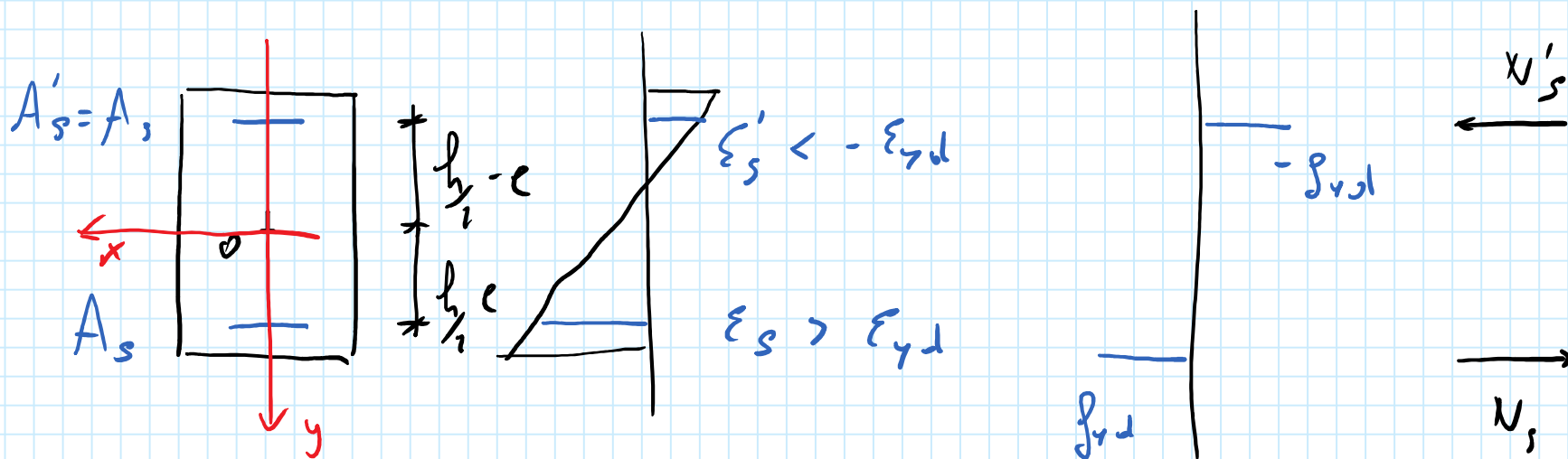
$$N = \int \sigma dA = N_c + N'_s + N_s$$

$$M = \int \sigma y dA = -N_c \left( \frac{l}{2} - \kappa h \right) + (A_s \sigma_s - A'_s \sigma'_s) \left( \frac{l}{2} - c \right)$$



Sezione rettangolare con armatura simmetrica

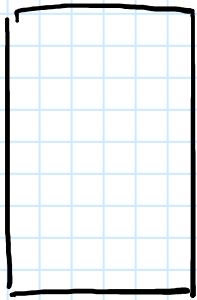
Rappresentazioni analitiche del dominio di resistenza



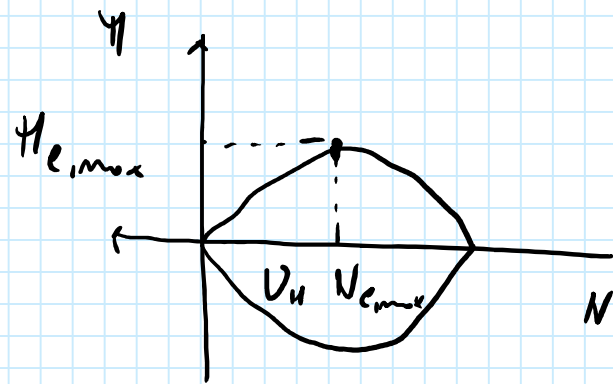
$$+ A'_s f_{yd} \left( \frac{h}{2} - e \right) + A_s f_{yd} \left( \frac{h}{2} - e \right) = 2 A_s f_{yd} \left( \frac{h}{2} - e \right)$$

$$N_{s, \max} : 2 A_s f_{yd}$$

$$M_{s, \max}$$



$\leftarrow \begin{matrix} \curvearrowright \\ V_{Ed} \end{matrix} \quad \varphi_{Rd} : ?$



$$V_{e,max} : A_c f_{cd} : b h f_{cd}$$

$$V_H \approx 0,48$$

$$\varphi_{e,max} \approx 0,12 b h^2 f_{cd}$$

Rappresentazione e "tre tratti"

$$1. M_{Rd}(N_{Ed}) = M_{S,max} \left( 1 - \frac{N_{Ed}}{N_{S,max}} \right) \quad 0 \leq N_{Ed} \leq N_{S,max}$$

$$2. M_{Rd}(N_{Ed}) = M_{e,max} \left[ 1 - \left( \frac{N_{Ed} + \nu_H N_{e,max}}{\nu_H N_{e,max}} \right)^2 \right] + M_{S,max} \quad -\nu_H N_{e,max} \leq N_{Ed} < 0$$

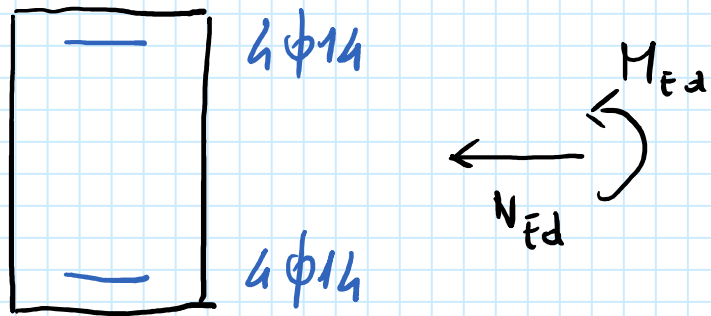
$$3. M_{Rd}(N_{Ed}) = (M_{e,max} + M_{S,max}) \left[ 1 - \left| \frac{N_{Ed} + \nu_H N_{e,max}}{(1 - \nu_H) N_{e,max} + N_{S,max}} \right|^m \right]$$

$$m = 1 + \left[ \frac{\nu_H N_{e,max}}{(1 - \nu_H) N_{e,max} + N_{S,max}} \right]^2, \quad N_{Ed} \leq -\nu_H N_{e,max}$$

Rappresentazione ed "un Tre Ho"

$$M_{Ed}(N_{Ed}) = (H_{e,max} + H_{s,max}) \left[ 1 - \left| \frac{N_{Ed} + \gamma_H N_{e,max}}{\gamma_H N_{e,max} + N_{s,max}} \right|^m \right]$$

$$m = 1 + \frac{\gamma_H N_{e,max}}{\gamma_H N_{e,max} + N_{s,max}}$$



e30/32

B450 C

$$N_{Ed} = -1000 \text{ kN}$$

$$M_{Ed} = 380 \text{ kNm}$$

$$N_{c,max} = b h f_{cd} = 30 \times 60 \times \frac{17}{10} = 3060 \text{ kN}$$

$$M_{c,max} = 0,12 b h^2 f_{cd} = 0,12 \times 30 \times 60^2 \times 17 \frac{1}{10^3} = 220,3 \text{ kNm}$$

$$N_{s,max} = 2 A_s f_{yd} = 2 \times 6,16 \times \frac{391,3}{10} = 482,1 \text{ kN}$$

$$M_{s,max} = 2 A_s \left( \frac{h}{2} - e \right) f_{yd} = 2 \times 6,16 \times (30 - 4) \times \frac{391,3}{10^3} = 125,4 \text{ kNm}$$

Verificare - Dominio e tu tratt:

$$N_{Ed} = -1000 > -\nu_H N_{e,max} = -0,48 \times 3060 = -1468 \text{ kN}$$

$$2. \psi_{Rd}(N_{Ed}) = \psi_{e,max} \left[ 1 - \left( \frac{N_{Ed} + \nu_H N_{e,max}}{\nu_H N_{e,max}} \right)^2 \right] + \psi_{s,max}$$

$$-\nu_H N_{e,min} \leq N_{Ed} < 0$$

$$\psi_{Rd}(N_{Ed}) = 220,3 \times \left[ 1 - \left( \frac{-1000 + 1468}{1468} \right)^2 \right] + 125,4$$

$$= \underbrace{\quad}_{197,9}$$

$$+ 125,4 = 323,5 \text{ kN/m}$$

NO

Verificare - Domino ed un tello

$$M_{Ed}(N_{Ed}) = (M_{e,max} + M_{s,max}) \left[ 1 - \left| \frac{N_{Ed} + \gamma_H N_{e,max}}{\gamma_H N_{e,max} + N_{s,max}} \right|^m \right]$$

$$m = 1 + \frac{\gamma_H N_{e,max}}{\gamma_H N_{e,max} + N_{s,max}}$$

$$M_{Ed}(N_{Ed}) = (220,3 + 125,4) \left[ 1 - \left| \frac{-1000 + 1468}{1468 + 481,8} \right|^{1,75} \right] = 335,4 \text{ kNm}$$

NO

$$m = 1 + \frac{1468}{1468 + 481,8} = 1,75$$



## Progetto - Dominio a tre tratti

$$M_{Ed} : 380 \text{ KNm} > \eta_{Rd}(N_{Ed}) : 323,5 \text{ KNm}$$

d'armatura non basta

Considero l'agguancio n. 2

$$\eta_{Rd}(N_{Ed}) = \eta_{e, \max} \left[ 1 - \left( \frac{N_{Ed} + \eta_H V_{e, \max}}{\eta_H V_{e, \max}} \right)^2 \right] + \eta_{s, \max}$$

Momento portato dalle uti  
in elastanza

L'armature des poutres

$$M_{s,max} = M_{Ed} - M_{c,max} \left[ 1 - \left( \frac{N_{Ed} + \alpha M_{c,max}}{\alpha N_{c,max}} \right)^2 \right]$$
$$= 380 - 220,3 \times \left[ 1 - \left( \frac{-1000 + 1468}{1468} \right)^2 \right] = 182,1 \text{ KNm}$$

197,9

$$\text{on } M_{s,max} = \sigma A_s f_{yd} \left( \frac{h}{\gamma} - e \right) \Rightarrow A_s = \frac{M_{s,max}}{\sigma \left( \frac{h}{\gamma} - e \right) f_{yd}}$$

$$A_s = \frac{182,1}{2 \times (30 - 4) \times 391,3} \times 10^3 = 8,95 \text{ cm}^2 \quad 3 \phi 20 \text{ par l'axe}$$