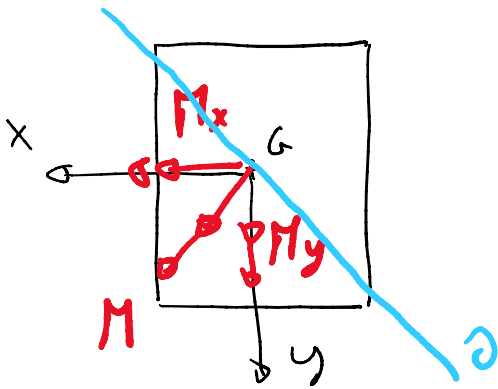


VERIFICA A FLESSIONE

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SEZ. CON MATERIALE OMOGENEO E ISOTROPO



$$\varepsilon = \varepsilon_G + \chi_x X + \chi_y Y$$

$$\varepsilon_G = \frac{N}{EA}$$

$$\chi_x = -\frac{M_y}{EI_y} ; \quad \chi_y = \frac{M_x}{EI_x}$$

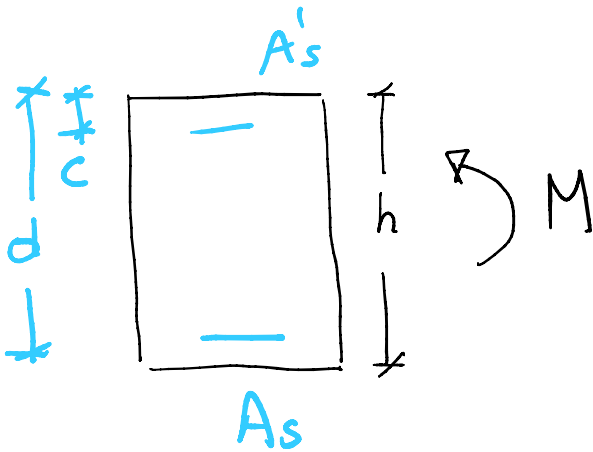
$$N = 0 \Rightarrow \varepsilon_G = 0 \iff \text{ASSE NEUTRO BARICENTRICO}$$

FLESSIONE RETTA $M = M_x$

SEZ. IN C.A

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DEFINIZIONI



A_s ARMATURA TESA

A'_s ARMATURA COMPRESSA

$d =$ ALTEZZA UTILE

(DISTANZA A_s DAL BORDO COMPRESSO)

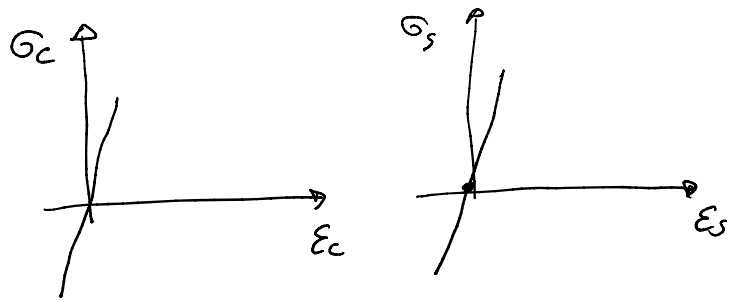
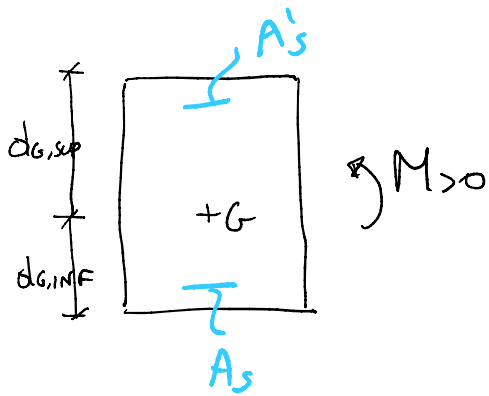
$c =$ COPRIFERRO

$$d = h - c$$

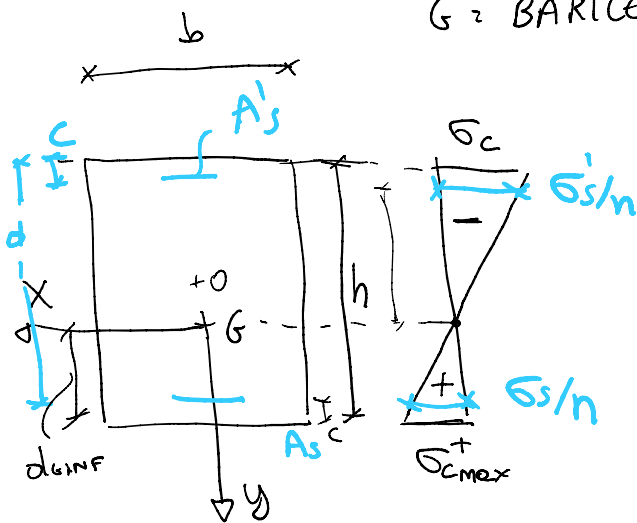
I STADIO

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SEZ. OMOGENEIZZATA



G = BARICENTRO SEZ. OMOGEN.



$$\sigma_c = \frac{M_x}{I_x} y$$

$$\sigma_s = n \sigma_c$$

$$n = E_s / E_c$$

$$d_{G,sup} = \frac{S_{sup}}{A}$$

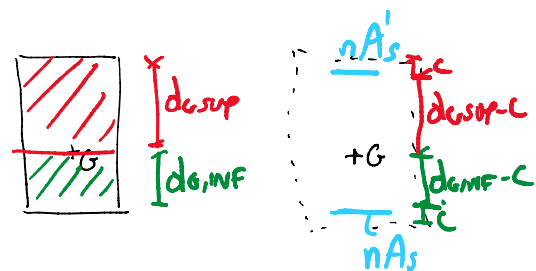
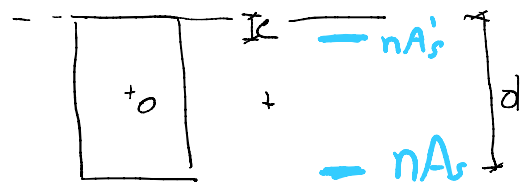
$$A = bh + nA's + nA_s$$

$$S_{sup} = bh \cdot \frac{h}{2} + nA'sc + nA_s d$$

$$I_x = \frac{bd_{G,sup}^3}{3} + \frac{bd_{G,inf}^3}{3} + nA's(d_{G,sup} - c)^2 + nA_s(d_{G,inf} - c)^2$$

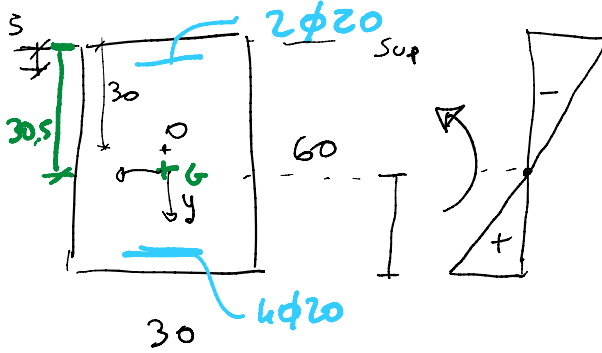
$$\sigma_{c,max}^{\oplus} = \frac{M}{I_x} \cdot d_{G,inf}$$

$$\sigma_s = n \frac{M}{I_x} (d_{G,inf} - c); \quad \sigma_s' = -n \frac{M}{I_x} (d_{G,sup} - c)$$



ESEMPIO

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$$M = 50 \text{ KNm}$$

B450C
C25/30

$$c = 5 \text{ cm}$$

$$d = 60 - 5 = 55 \text{ cm}$$

$$\eta = \frac{E_s}{E_c} = 6,35$$

$$A_s = 4 \times \pi \cdot \frac{2^2}{4} = 12,56 \text{ cm}^2$$

$\frac{4}{3.14 \text{ cm}^2}$

$$A'_s = 2\phi 20 \rightarrow 6,28 \text{ cm}^2$$

1. DETERMINO G

$$S_{sup} = 30 \times 60 \times \frac{60}{2} + 6,35 \times 6,28 \times 5 + 6,35 \times 12,56 \times 55$$
$$= 58586 \text{ cm}^3$$

$$A = 30 \times 60 + 6,35 (6,28 + 12,56) = 1919,6 \text{ cm}^2$$

$$d_{G, sup} = \frac{58586}{1919,6} = 30,52 \text{ cm} \quad d_{G, inf} = 60 - 30,52 = 29,48 \text{ cm}$$

$$I_x = \frac{30 \times 30,52^3}{3} + \frac{30}{3} \times 29,48^3 + 6,35 \times \left[6,28 (30,5 - 5)^2 + 12,56 (29,48 - 5)^2 \right]$$
$$= 614213 \text{ cm}^4$$

$$\sigma_{cmex} = \frac{50 \text{ KNm}}{614213 \text{ cm}^4} \times 29,48 \text{ cm} \times \frac{10^3 \times 10^7}{10^3} \frac{N}{\text{mm}^2} = 2,4 \text{ MPa}$$

LA SEZIONE E' FESSURATA ?

CONFRONTO CON $f_{ctk} = 1,2 f_{ctk} = 2,15 \text{ MPa}$

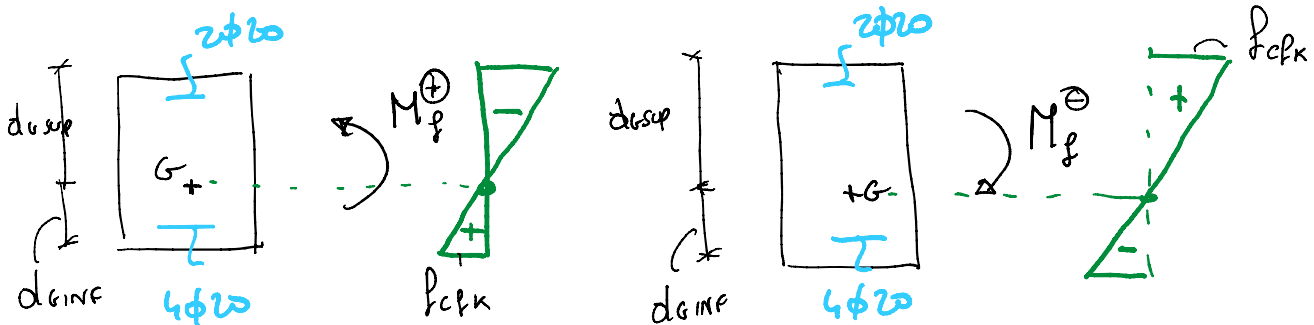
$$f_{ctk} = 0,7 \times 0,3 \sqrt[3]{f_{ck}^2} = 0,7 \times 0,3 \sqrt[3]{25^2} = 1,8 \text{ MPa}$$

$\sigma_{cmex}^+ > f_{ctk} \Rightarrow \text{SEZ. E' FESSURATA}$

MOMENTO DI FESSURAZIONE

$$\sigma_{cmex}^+ = \frac{M}{I} d_{G,INF} \quad M > 0$$

PONGO $\sigma_{cmex}^+ = f_{ctk} \Rightarrow M_{fess} = f_{ctk} \cdot \frac{I}{d_{G,INF}}$



$$M_{fess}^{\ominus} = f_{ctk} \cdot \frac{I}{d_{G,SUP}}$$

NEL CASO DELL'ESEMPLO

$$50 \text{ kNm} : 2,4 \text{ MPa} = M_f : 2,15 \text{ MPa} \Rightarrow$$

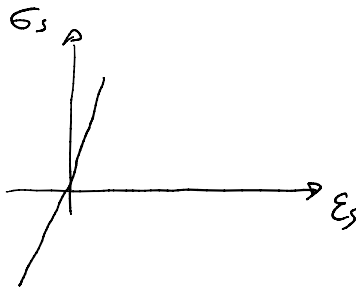
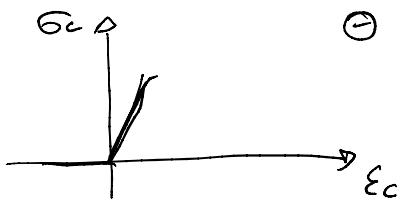
$$M_f = 44,58 \text{ kNm}$$

$$\sigma_s = \frac{n}{635} \times \frac{44,58 \text{ kNm}}{614213 \text{ cm}^4} \times (29,48 - 5) \times 10^3 = 11,34 \text{ MPa}$$

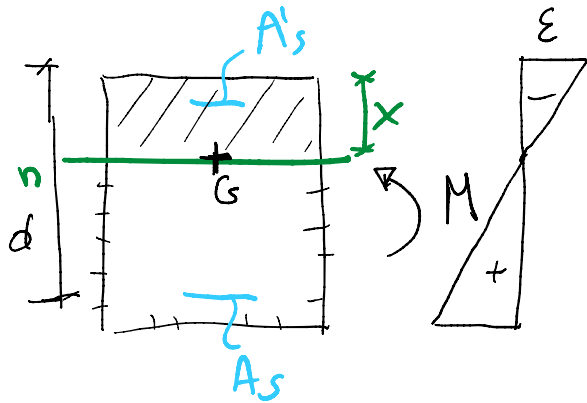
II STADIO

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LEGAMI COSTITUTIVI

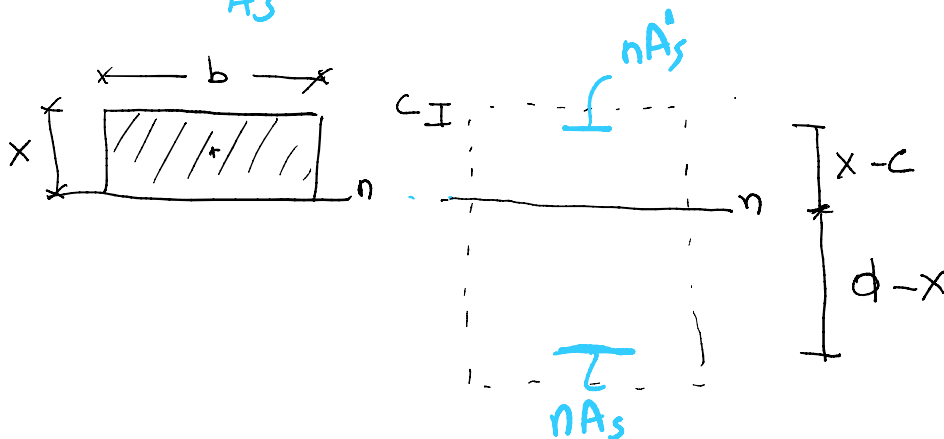


SEZIONE DI RIFERIMENTO : SEZ. REAGENTE OMOGEN.



x DISTANZA ASSE NEUTRO DAL BORDO COMPRESSO

$$\sum n = 0 \Leftrightarrow \text{ASSE NEUTRO BARILENTRICO}$$



$$\sum n = -\frac{bx^2}{2} - nA'_s(x-c) + nA_s(d-x) = 0$$

$$\frac{bx^2}{2} + nA'_s x - nA'_s c - nA_s d + nA_s x = 0$$

$$x^2 + \frac{2n}{b} (A'_s + A_s)x - \frac{2n}{b} (A'_s c + A_s d) = 0$$

$$x = -\frac{n}{b} (A'_s + A_s) \pm \sqrt{\frac{n^2}{b^2} (A'_s + A_s)^2 + \frac{2n}{b} (A'_s c + A_s d)}$$

UNICA SOLUZIONE CON SIGNIFICATO FISICO $x > 0$

$$x = -\frac{n}{b} (A'_s + A_s) + \sqrt{\frac{n^2}{b^2} (A'_s + A_s)^2 \left[1 + \frac{b^2 \cdot \frac{2n}{b} (A'_s c + A_s d)}{n^2 (A'_s + A_s)^2} \right]}$$

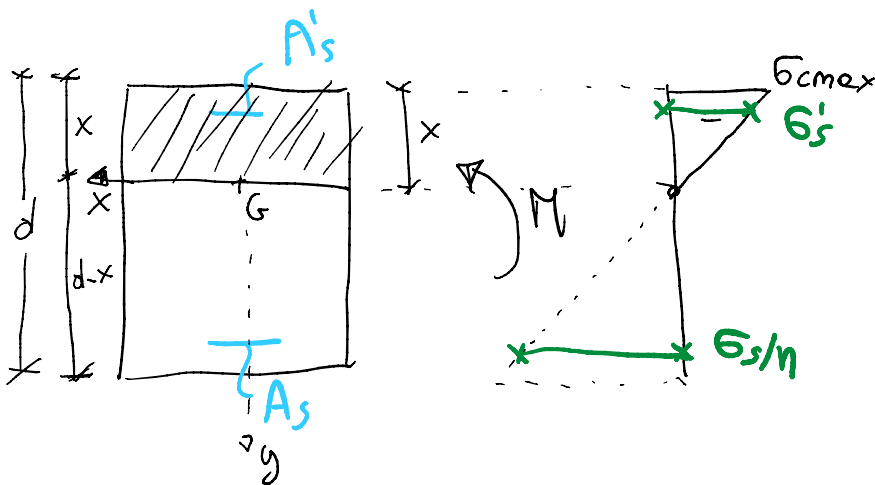
$$x = \underbrace{\frac{dn}{bd} (A'_s + A_s)}_{\psi} \left[-1 + \sqrt{1 + \frac{2bd (A'_s c + A_s d)}{dn (A'_s + A_s) (A'_s + A_s)}} \right]$$

$\psi =$ PERC. ELASTICA DI ARMATURA $= \frac{n(A'_s + A_s)}{bd}$

$$x = \psi d \left[-1 + \sqrt{1 + \frac{2}{\psi d} \cdot \frac{A'_s c + A_s d}{(A'_s + A_s)}} \right]$$

$d_{G,S} =$ DISTANZA BARICENTRO ARMATURE DAL BORDO COMPRESSO $= \frac{A'_s c + A_s d}{A'_s + A_s}$

$$x = \psi d \left[-1 + \sqrt{1 + \frac{2d_{G,S}}{\psi d}} \right]$$



$$\sigma_{cmax} = -\frac{M}{I_x} x$$

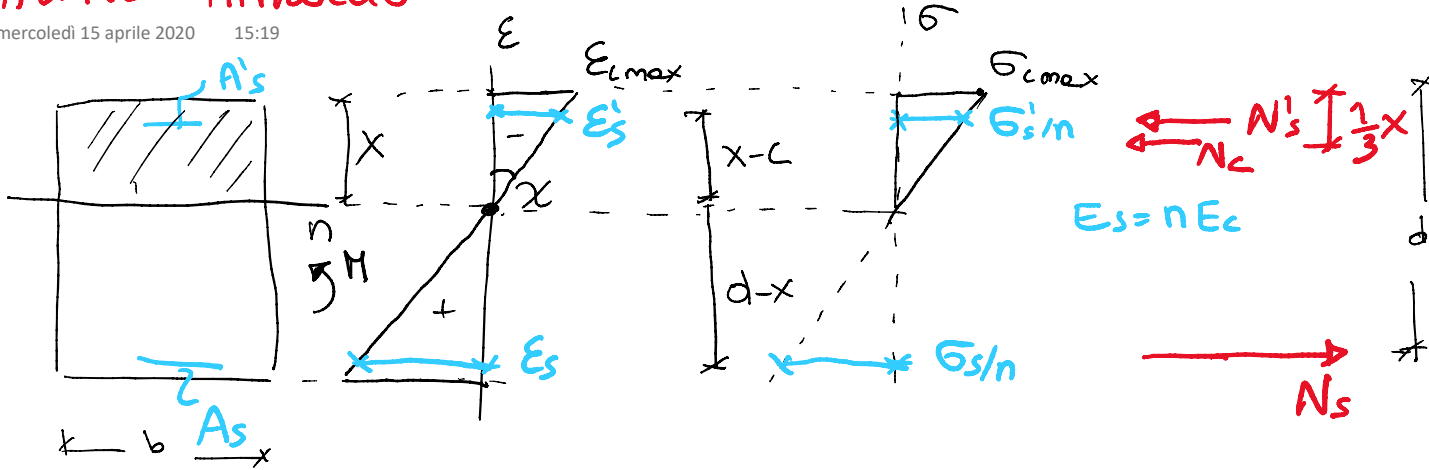
$$\sigma_s = n \frac{M}{I_x} (d-x)$$

$$\sigma'_s = -n \frac{M}{I_x} (x-c)$$

$$I_x = \frac{bx^3}{3} + n A'_s (x-c)^2 + n A_s (d-x)^2$$

ALTRO APPROCCIO

mercoledì 15 aprile 2020 15:19



$$\epsilon_{cmax} = -\chi x$$

$$\epsilon'_s = -\chi (x-c)$$

$$\epsilon_s = \chi (d-x)$$

$$\sigma_{cmax} = \epsilon_{cmax} E_c = -E_c \chi \cdot x$$

$$\sigma'_s = E_s \epsilon'_s = -n E_c \chi (x-c)$$

$$\sigma_s = E_s \epsilon_s = n E_c \chi (d-x)$$

FLESSIONE SEMPLICE $N_{TOT} = 0$ EQ. TRASLAZIONE

$$N_{TOT} = N_c + N'_s + N_s = 0$$

$$N_c = b x \frac{\sigma_{cmax}}{2} = -E_c \chi b \frac{x^2}{2}$$

$$N'_s = A'_s \cdot \sigma'_s = -A'_s \cdot n E_c \chi (x-c)$$

$$N_s = A_s \cdot \sigma_s = A_s \cdot n E_c \chi (d-x)$$

$$-E_c \chi \frac{b x^2}{2} - n A'_s E_c \chi (x-c) + n A_s E_c \chi (d-x) = 0$$

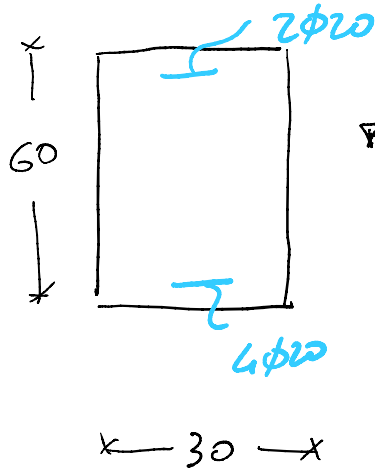
$$\boxed{-\frac{b x^2}{2} - n A'_s (x-c) + n A_s (d-x) = 0} \Rightarrow x$$

EQ. ROTAZIONE

$$N'_s \cdot c + N_c \frac{x}{3} + N_s d = M_{ed} \Rightarrow E_c \chi$$

ESEMPIO

mercoledì 15 aprile 2020 15:50



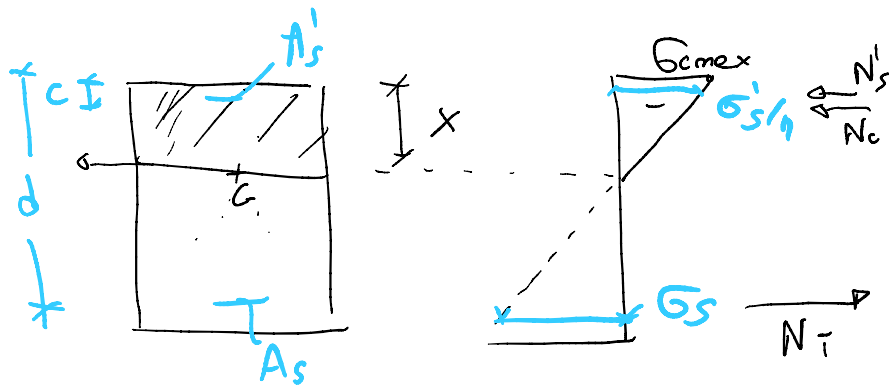
B450C c = 5 cm
C25/30 d = 55 cm

CARICHI DI LUNGA DURATA $\Rightarrow n = 15$

$$\sigma_{cmax} = ?$$

$$\sigma_s = ?$$

1. TROVARE X



$$A_s = 12,56 \text{ cm}^2$$

$$A'_s = 6,28 \text{ cm}^2$$

$$X = \psi d \left[-1 + \sqrt{1 + \frac{2 \phi \omega_s}{\psi d}} \right]$$

$$\psi = \frac{n (A'_s + A_s)}{bd} = \frac{15 \times (6,28 \text{ cm}^2 + 12,56 \text{ cm}^2)}{30 \times 55 \text{ cm}^2}$$

$$= 0,17$$

$$d_{g,s} = \frac{A_s \cdot d + A'_s c}{A_s + A'_s} = \frac{12,56 \times 55 + 6,28 \times 5}{12,56 + 6,28} = 38,33 \text{ cm}$$

$$X = 0,17 \times \underset{\substack{\uparrow \\ \text{cm}}}{55} \left[-1 + \sqrt{1 + \frac{2 \times 38,33}{0,17 \times 55}} \right] = 19,1 \text{ cm}$$

2. CALCOLO σ_{cmax}

$$I_x = \frac{30 \times 19,1^3}{3} + 15 \times 6,28 (19,1 - 5)^2 + 15 \times 12,56 (55 - 19,1)^2$$
$$= 331218 \text{ cm}^4$$

$$\sigma_{cmax} = - \frac{160 \text{ kNm}}{331218 \text{ cm}^4} \times 19,1 \text{ cm} \times 10^3 = -9,23 \text{ MPa}$$

CONFRONTARE $\left\{ \begin{array}{l} -0,45 f_{ck} \\ 11,25 \text{ MPa} \end{array} \right.$ (COMB. QUASI PERM.)

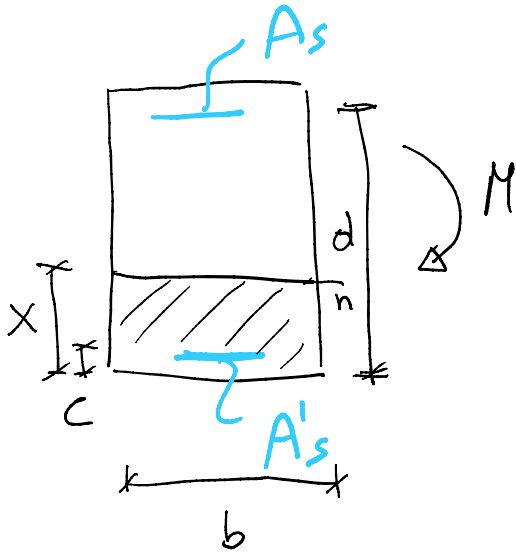
$\left\{ \begin{array}{l} -0,60 f_{ck} \\ \end{array} \right.$ (COMB. RARA)

$$\sigma_s = 15 \frac{160 \text{ kNm}}{331218 \text{ cm}^4} (55 - 19,1) \times 10^3 = 260 \text{ MPa}$$

CONFRONTARE CON $0,8 f_{yk} = 0,8 \times 450 \text{ MPa}$
(COMB. RARA) $= 360 \text{ MPa}$

CASO CON $M < 0$

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$$\sum N = 0$$

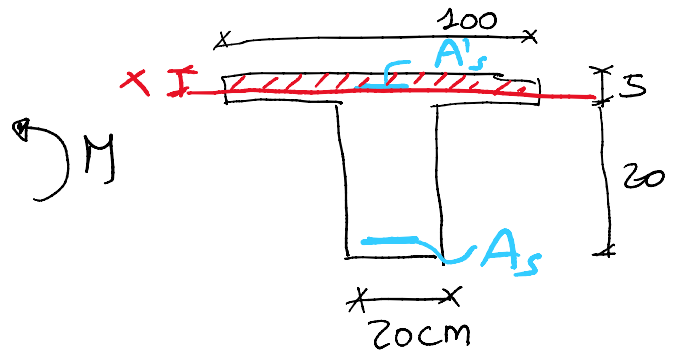
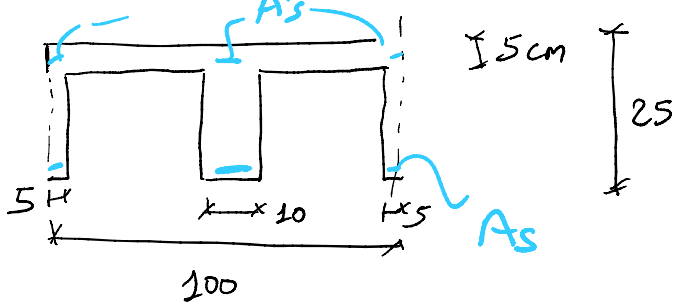
$$\frac{bx^2}{2} + nA'_s(x-c) - nA_s(d-x) = 0$$

$$c_{gs} = \frac{A'_s \cdot c + A_s \cdot d}{A_s + A'_s}$$

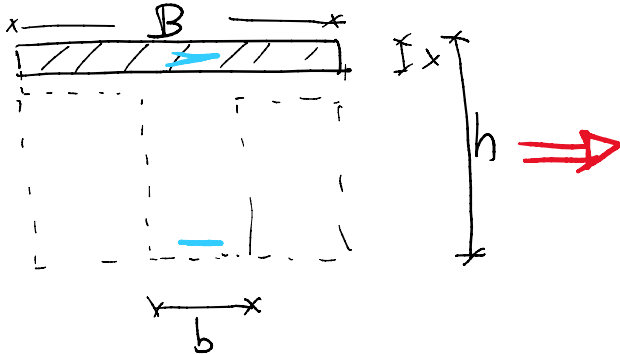
SEZIONI A T

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16:12



SE ASSE NEUTRO : $x \leq d$



SEZ. RETTANGOLARE

$$B \times h$$

(VALIDA PER SEZ. RETTANGOLARE)

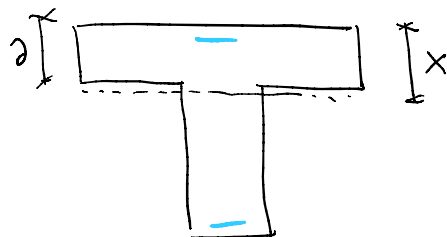
POSSO RITRAVARE x

$$x = \psi d \left[-1 + \sqrt{1 + \frac{2 \phi \sigma_s}{\psi d}} \right]$$

SE $x \leq d \Rightarrow$ OK \Rightarrow VERIFICO COME SEZ. RETTANGOLARE

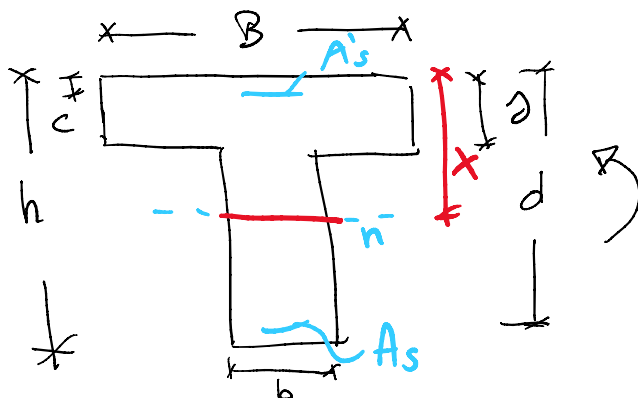
SE $x > d$

CASO 1

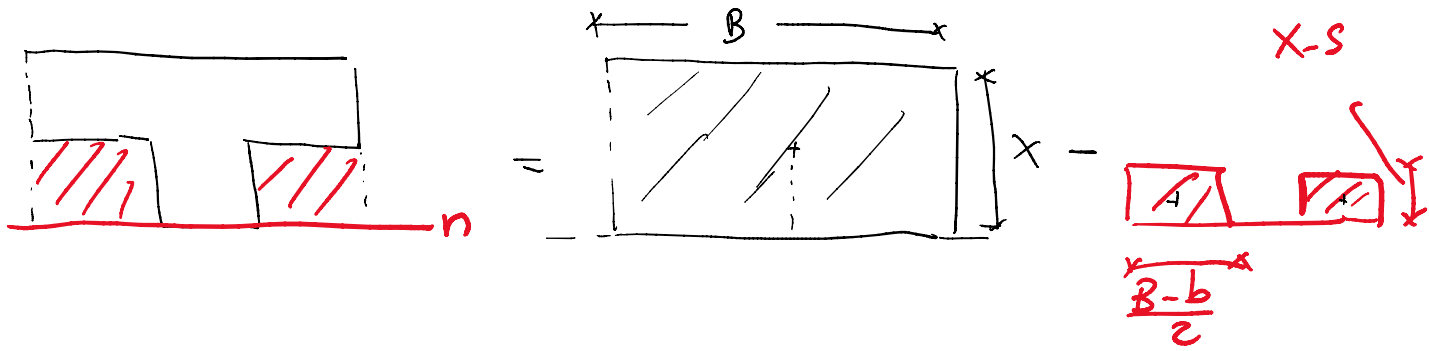


IN FUDO APPROSSIMATO CONSIDERO SEZ. RETTANGOLARE

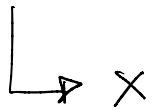
CASO 2



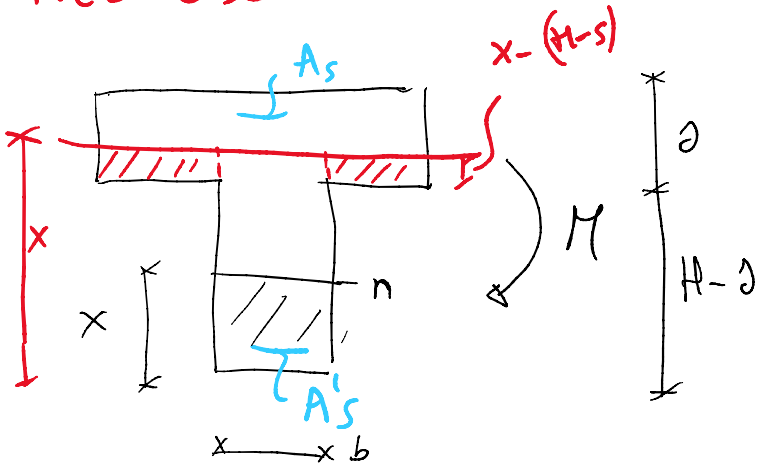
$$S_N = 0$$



$$S_N = -\frac{Bx^2}{2} + (B-b)\frac{(x-s)^2}{2} + nA_s(d-x) - nA'_s(x-c) = 0$$



NEL CASO DI $M_{ed} < 0$



Se $x \leq H-d$

$$S_{n_{cus}} = b \frac{x^2}{2}$$

Se $x > H-d$

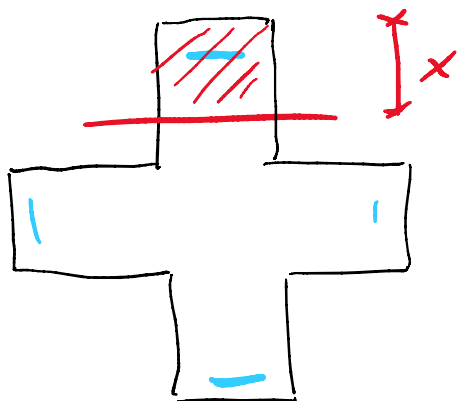
$$S_{n_{cus}}: \frac{b x^2}{2} + \frac{(B-b)}{2} \cdot [x - (H-d)]^2$$

+ ARMATURE $S_{n'_s} = A'_s n (x-c)$

$$S_{n_s} = -A_s \cdot n (d-x)$$

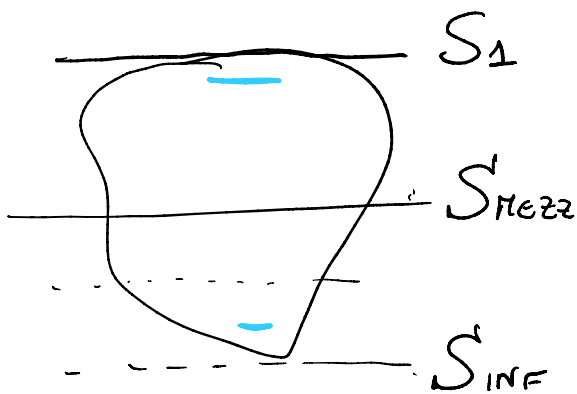
ALTRE SEZ. ASSIMILABILI ALLA RETTANGOLARE

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SOLUZIONI NUMERICHE

mercoledì 15 aprile 2020 16:29



$$S_1 > 0$$

$$S_{INF} < 0$$

$$S_{mezz} \begin{cases} > 0 \\ < 0 \end{cases}$$

METODO DI BISEZIONE

VEDI FOGLIO EXCEL PER SEZIONE A T