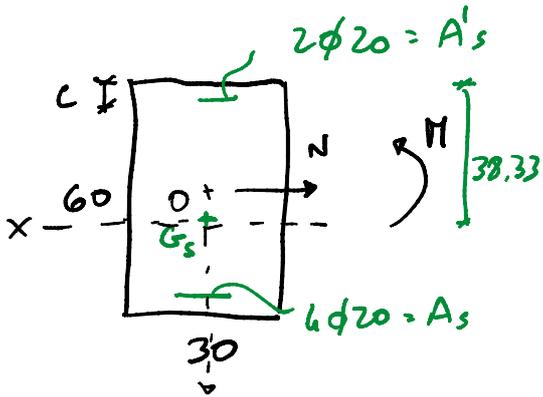


ESEMPIO $N > 0$; $M > 0$ PICCOLA ECCENTRICITA'

mercoledì 13 maggio 2020 13:56



II STADIO, $n = 15$

$N = 360 \text{ kN}$

$A_s' = 6,28 \text{ cm}^2$

$M = 54 \text{ kNm}$

$A_s = 12,56 \text{ cm}^2$

$c = 5 \text{ cm}$

$d = 55 \text{ cm}$

1. DETERMINARE G_s

$$d_{G_s, \text{sup}} = \frac{S_{\text{sup}}}{A_{s, \text{tot}}} = \frac{6,28 \text{ cm}^2 \times 5 \text{ cm} + 12,56 \text{ cm}^2 \times 55 \text{ cm}}{(6,28 + 12,56) \text{ cm}^2} = 38,33 \text{ cm}$$

$$d_{G_s, \text{inf}} = H - 38,33 = 60 - 38,33 = 21,67 \text{ cm}$$

2. DETERMINO $I_{s, G_s} = 12,56 \text{ cm}^2 \times (d_{G_s, \text{inf}} - c)^2 + 6,28 \text{ cm}^2 \times (d_{G_s, \text{sup}} - c)^2$

$$\rightarrow I_{s, G_s} = 12,56 \times (21,67 - 5)^2 + 6,28 \times (38,33 - 5)^2 = 20466,7 \text{ cm}^4$$

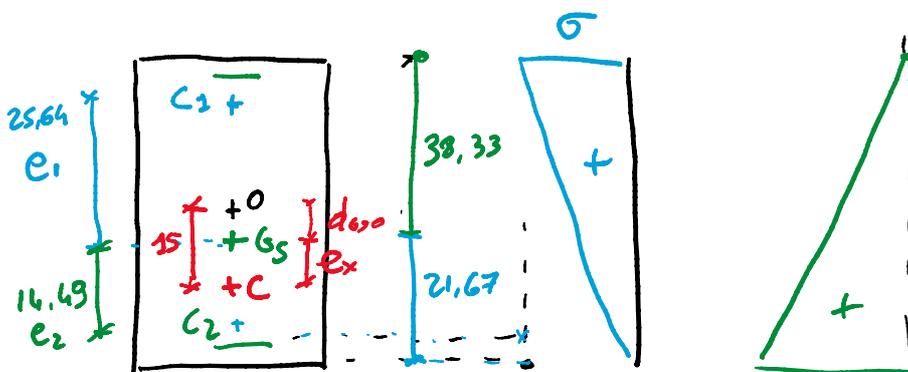


DIAGRAMMA DI σ PER $C \equiv C_2$

DIAGRAMMA σ PER $C \equiv C_2$

$$e_1 = \frac{I_s}{A_{s,inf} \cdot d_{GS,inf}} \rightarrow e_1 = \frac{10466,7 \text{ cm}^4}{(12,56 + 6,28) \times 21,67} = 25,64 \text{ cm}$$

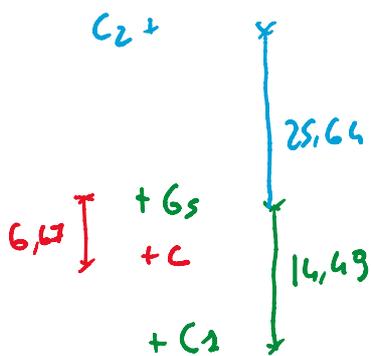
$$e_2 = \frac{I_s}{A_{s,tot} \cdot d_{GS,sup}} \rightarrow e_2 = \frac{10466,7 \text{ cm}^4}{(12,56 + 6,28) \text{ cm}^2 \times 38,33 \text{ cm}} = 14,49$$

PER CARIC SE SEZ. PARZIALIZZATA, VALUTO C

$$e_0 = \frac{M}{N} = \frac{54 \text{ kNm}}{360 \text{ kN}} \times 100 = 15 \text{ cm}$$

$$e_x = e_0 - d_{GS,0} = 15 \text{ cm} - 8,33 \text{ cm} = 6,67 \text{ cm}$$

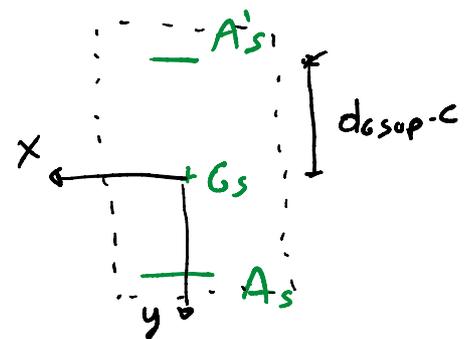
$$d_{GS,0} = d_{GS,sup} - h/2$$



$$-e_2 \leq e_x \leq e_2 \Rightarrow$$

SEZ. A PICCOLA ECCENTRICITÀ
 → SEZ. INTERAMENTE TESA

$$\sigma_s = \frac{N}{A_{s,tot}} + \frac{N \cdot e_x}{I_{x,GS}} \cdot y$$



ARMATURE INFERIORI

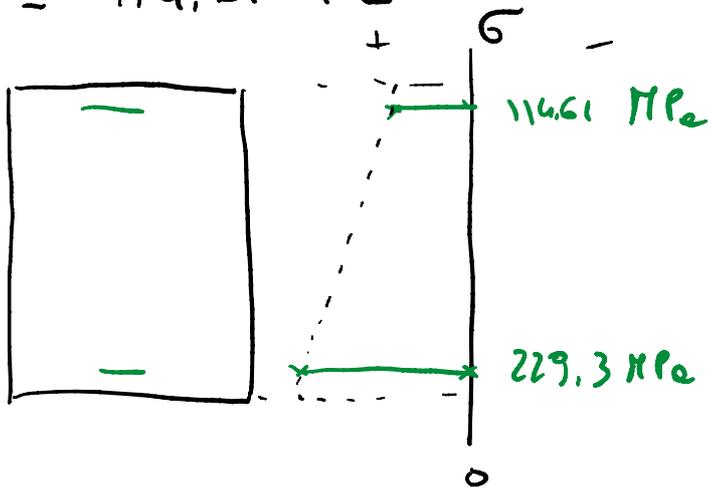
$$\sigma_s = \frac{360 \text{ kN} \times 10}{(12,56 + 6,28) \text{ cm}^2} + \frac{360 \text{ kN} \cdot 6,67 \text{ cm}}{10466,7 \text{ cm}^4} \left(d_{GS,inf} - c \right) \text{ cm} \times 10$$

$$= 229,3 \text{ MPa}$$

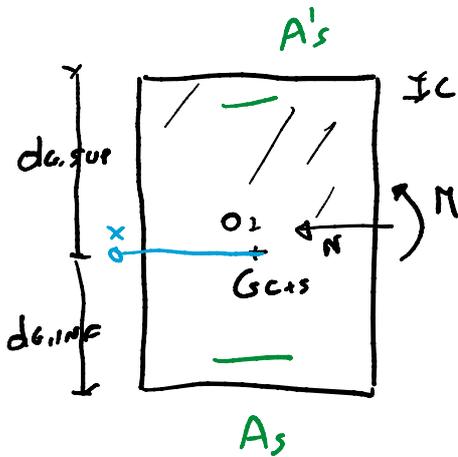
ARMATURE SUPERIORI

$$\sigma_s' = \frac{360}{(12,56 + 6,28)} \times 20 - \frac{360 \times 6,67}{10466,7} \left(\frac{d_{G.SUP} - c}{38,33 - 5} \right) \times 20$$

$$= 114,61 \text{ MPa}$$



DEVO CAPIRE SE LA SEZIONE È - INTERAMENTE COMPRESA
- PARZ.



1. CALCOLO G_{C+S}

$$d_{G,SUP} = \frac{S_{SUP}}{A_{ci}} = \frac{bh^2/2 + nA'_s c + nA_s \cdot d}{bh + n(A_s + A'_s)}$$

2. ESTREMI NOCCIOLO

$$e_1 = \frac{I_{G,x}}{A_{ci} \cdot d_{G,INF}} ; e_2 = \frac{I_{G,x}}{A_{ci} d_{G,SUP}}$$

$$I_{G,x} = \frac{bd_{G,SUP}^3}{3} + \frac{bd_{G,INF}^3}{3} + nA'_s (d_{G,SUP} - c)^2 + nA_s (d_{G,INF} - c)^2$$

3. CALCOLO $e_x = e_0 - d_{G0} = \frac{M}{N} - \left(d_{G,SUP} - \frac{h}{2}\right)$

4. SEZIONE INTERAMENTE COMPRESA SE

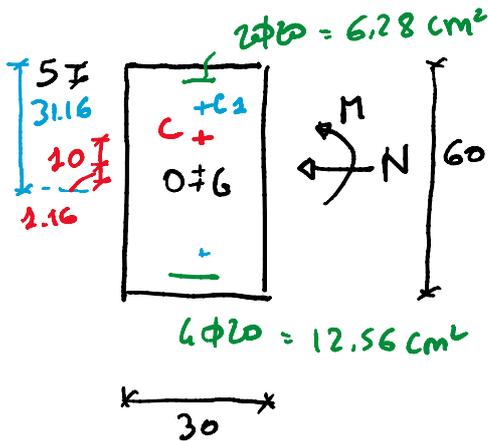
$$-e_2 \leq e_x \leq e_2 \Rightarrow \text{PICCOLA ECCENTRICITÀ}$$

$$\sigma_c = \frac{N}{A_{ci}} + \frac{N \cdot e_x}{I_{G,x}} \cdot y$$

$$\sigma_s = \sigma_c \cdot n$$

ESEMPIO $N < 0$, PICCOLA ECCENTRICITÀ

mercoledì 13 maggio 2020 14:44



$$N = -500 \text{ KN}$$

$$M = 50 \text{ KNM}$$

$$e_0 = \frac{M}{N} = \frac{50}{-500} = -0,10 \text{ m}$$

II STADIO

CARICHI LUNGA DURATA $\Rightarrow \eta = 1,5$

$$A'_s = 6,28 \text{ cm}^2$$

$$A_s = 12,56 \text{ cm}^2$$

$$d = 55 \text{ cm}$$

1. BARICENTRO

$$\begin{aligned} \hat{S}_{\text{sup}} &= \frac{30 \times 60^2}{2} + 15 \times 6,28 \times 5 + 15 \times 12,56 \times 55 = \\ &= 64833 \text{ cm}^3 \end{aligned}$$

$$\begin{aligned} A_{ci} &= 30 \times 60 + 15 \times (6,28 + 12,56) = \\ &= 2082,6 \text{ cm}^2 \end{aligned}$$

$$d_{G, \text{sup}} = \frac{64833 \text{ cm}^3}{2082,6 \text{ cm}^2} = 31,13 \text{ cm}$$

$$\rightarrow d_{G, \text{inf}} = 60 - 31,13 \text{ cm} = 28,87 \text{ cm}$$

2. CALCOLO ESTREMI DEL NOCCIOLO

$$e_1 = \frac{I_{xG}}{A_{ci} \cdot d_{G, \text{inf}}}$$

$$\begin{aligned} I_{xG} &= \frac{30 \times 31,13^3}{3} + \frac{30 \times 28,87^3}{3} + 15 \times 6,28 \times (31,13 - 5)^2 + \\ &+ 15 \times 12,56 \times (28,87 - 5)^2 = \\ &= 713962 \text{ cm}^4 \end{aligned}$$

$$e_1 = \frac{713962 \text{ cm}^4}{2082,6 \text{ cm}^2 \times 28,87 \text{ cm}} = 11,88 \text{ cm}$$

$$e_2 = \frac{713962}{2082,6 \times 31,13} = 11,01 \text{ cm} \quad \left(\text{NON NECESSARIO PERCHÉ } e_x < 0 \right)$$

$$e_x = -11,13 \text{ cm} = e_0 - d_{G0} = -0,10 - \left(31,13 - \frac{6}{2} \right) \frac{1}{100}$$

\downarrow
 $d_{\text{sup}} - \frac{h}{2}$

$$-e_1 \leq e_x < e_2$$

$$-13,87 < -11,13 < 12,87 \Rightarrow \text{SEZ. INTERAMENTE COMPRESSA}$$

CALCOLO σ_c AL BORDO SUPERIORE ($y = -d_{G,\text{sup}}$)

$$\sigma_c^{\text{sup}} = \frac{N}{A_{ci}} - \frac{N e_x}{I} \cdot (d_{G,\text{sup}})$$

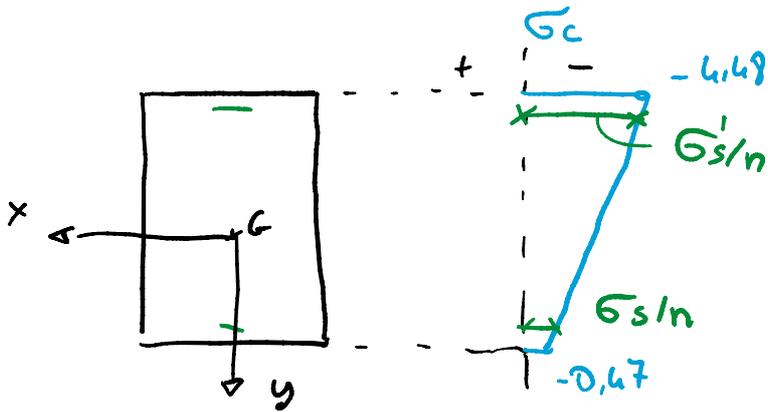
$$= \frac{-500 \text{ kN} \times 10}{2082,6 \text{ cm}^2} - \frac{(-500) \text{ kN} (-11,13) \text{ cm}}{713962 \text{ cm}^4} \times 31,13 \text{ cm} \times 10$$

$$= -2,4 - 2,43 = -4,83 \text{ MPa}$$

CALCOLO σ_c AL BORDO INFERIORE ($y = d_{G,\text{inf}}$)

$$\sigma_c^{\text{inf}} = -2,4 + 2,25 = -0,15 \text{ MPa}$$

$$y = d_{G,\text{inf}} = 28,87$$



TENSIONE ARMATURE SUP. $y = - (d_{\text{sup}} - c)$

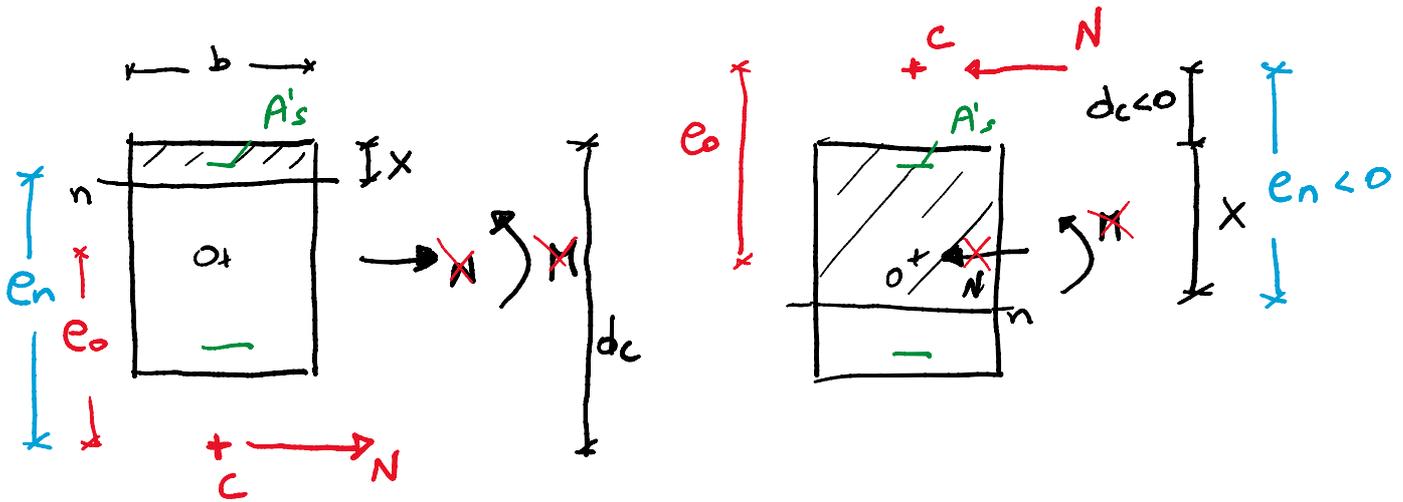
$$\sigma'_s = \left[\frac{N}{A} - \frac{N e_x}{I} \cdot (d_{\text{sup}} - c) \right] n$$

$$15 \times \left[\frac{500}{2086} \times 10 - \frac{(-500) \times (-11.13) \text{ kNcm}}{713962 \text{ cm}^4} \times (31.13 - 5) \text{ cm} \times 10 \right]$$

$$= -66,56 \text{ MPa}$$

PRESSO - TENSO FLESSIONE (GRANDE ECCENTRICITA')

mercoledì 13 maggio 2020 15:34



DETERMINO ASSE NEUTRO $e_n = \frac{I_n}{S_n}$

RIFERIMENTO ALLA SEZ. REAGENTE OMOGENEIZZATA

x DISTANZA ASSE NEUTRO DAL BORDO COMPRESSO

$$e_0 = \frac{M}{N}$$

e_n DISTANZA DI C DALL'ASSE NEUTRO

d_c DISTANZA DI C DAL BORDO COMPRESSO

$$e_n = d_c - x \quad d_c = e_0 + \frac{h}{2} \Rightarrow e_n = e_0 + \frac{h}{2} - x$$

$$I_n = \frac{bx^3}{3} + nA's(x-c)^2 + nA_s(d-x)^2$$

$$S_n = -\frac{bx^2}{2} - nA's(x-c) + nA_s(d-x)$$

SOSTITUISCO IN $e_n = \frac{I_n}{S_n} \rightarrow e_n \cdot S_n = I_n$

$$(d_c - x) \left(-\frac{bx^2}{2} - nA'_s(x-c) + nA_s(d-x) \right) = \frac{bx^3}{3} + nA'_s(x-c)^2 + nA_s(d-x)^2$$

$$x^3 - 3d_c x^2 + \frac{6n}{b} \left[A_s(d-d_c) + A'_s(c-d_c) \right] x + \frac{6n}{b} \left[A_s d(d-d_c) + A'_s c(c-d_c) \right] = 0$$

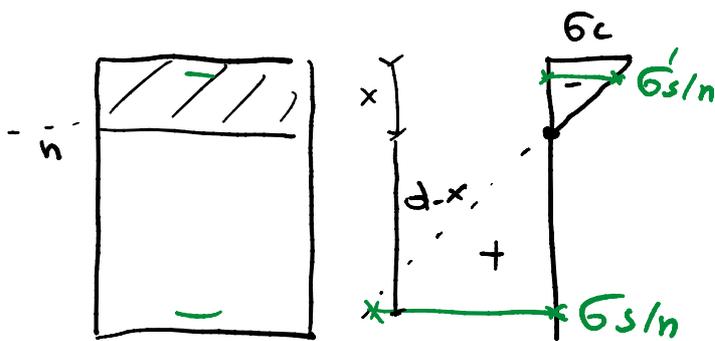
⇒ TROVO X

ERRORE ⇒ $\sigma = \frac{N}{A} + \frac{M}{I} y$

A=?
I=?

$$\sigma = \frac{N}{S_n} \cdot d$$

d DISTANZA DELL'ANTO IN CUI CALCOLO σ DA ASSE NEUTRO



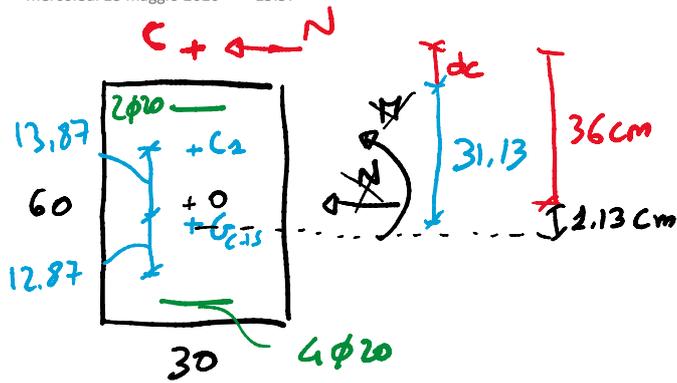
$$\sigma_c^{\max} = -\frac{N}{S_n} x$$

$$\sigma'_s = n \left[-\frac{N}{S_n} (x-c) \right]$$

$$\sigma_s = n \left[\frac{N}{S_n} (d-x) \right]$$

ESEMPIO

mercoledì 13 maggio 2020 15:57



$$N = -500 \text{ KN}$$
$$M = 180 \text{ KNM}$$

II STADIO

CARICHI LUNGA DURATA

1. PER CAPIRE SE SEZ. $\left\{ \begin{array}{l} \text{COMPRESSA INT.} \\ \text{PARZ.} \end{array} \right. \Rightarrow$ CALCOLARE e_1, e_2

$$d_{\text{sup}} = 31,13 \text{ cm}$$

$$e_1 = 13,87 \text{ cm}$$

$$e_2 = 12,87 \text{ cm}$$

$$e_0 = \frac{M}{N} = \frac{180 \text{ KNm}}{-500 \text{ KN}} \times 100 = -36 \text{ cm} \Rightarrow$$

$$e_x = -37,13 \text{ cm}$$

SEZ. PARZIALIZZATA

2. TROVO ASSE NEUTRO $e_n = \frac{I_n}{S_n} \Rightarrow e_n \cdot S_n - I_n = 0$

$$X^3 - \overbrace{3d_c}^{a_2} X^2 + \overbrace{\frac{6n}{b} [A_s(d-d_c) + A'_s(c-d_c)]}^{a_1} X + \underbrace{-\frac{6n}{b} [A_s d(d-d_c) + A'_s c(c-d_c)]}_{a_0} = 0$$

$$a_2 = -3 d_c \quad d_c = -6 \text{ cm} / 100 = -0.06 \text{ m}$$

$$a_2 = -3 \times (-0.06) = +0.18$$

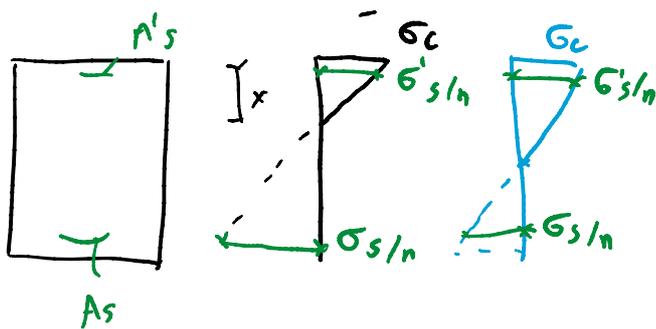
$$a_1 = \frac{6 \times 15}{0.30} \cdot \left[\frac{22.56}{100^2} (0.55 + 0.06) + \frac{6.28}{100^2} \times (0.05 + 0.06) \right]$$

$$= 0.251$$

$$a_0 = -\frac{6 \times 15}{0.30} \left[\frac{12.56}{100^2} \times 0.55 (0.55 + 0.06) + \frac{6.28}{100^2} \times 0.05 \times (0.05 + 0.06) \right]$$

$$= -0.127$$

COSA ASPETTARSI COME x ?



NEL CASO DI FLESSIONE SEMPLICE

$$N = 0 \quad x \approx \frac{1}{3} \div \frac{1}{4} h$$

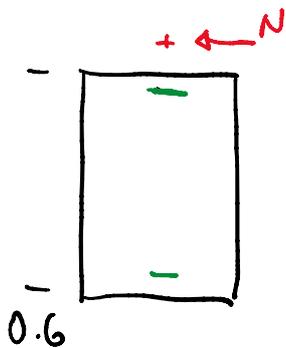
$$\int \sigma dA = 0$$

IN CASO DI PRESSO-FLESSIONE

$$N < 0 \quad \int \sigma dA = N$$

\Rightarrow DEVE CRESCERE LA ZONA COMPRESSA

PROCEDURA ITERATIVA



$$x = 0 \rightarrow x^3 + a_2 x^2 + a_1 x + a_0 = a_0 = -0.127$$

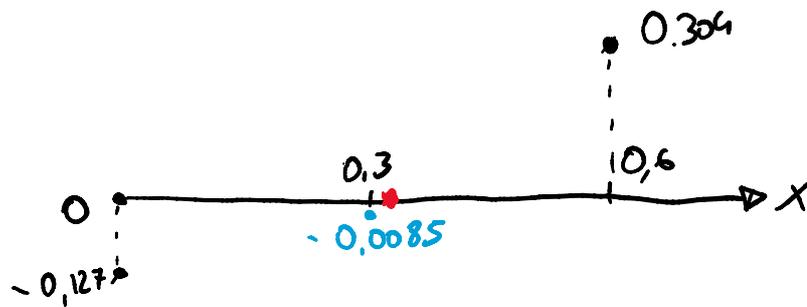
$$x = 0.6 \rightarrow 0.6^3 + 0.18 \cdot 0.6^2 + 0.251 \cdot 0.6 +$$

$$- 0.127 = 0.304$$

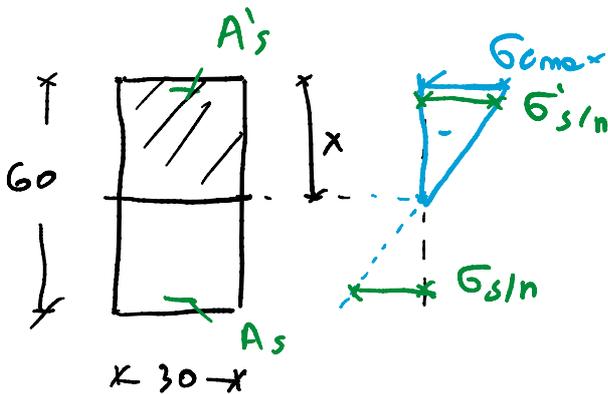
$$x = 0.3 \rightarrow 0.3^3 + 0.18 \cdot 0.3^2 + 0.251 \cdot 0.3 +$$

$$- 0.127 = -0.0085$$

$$x = 0.314 \text{ m}$$



CALCOLO LE TENSIONI



$$\sigma_c = \frac{N}{S_n} \cdot \varrho$$

$$\sigma_{cmax} \Rightarrow \varrho = -x$$

$$S_n = -\frac{bx^2}{2} + n A_s (d-x) - n A'_s (x-c)$$

$$= -\frac{30 \times 31.4^2}{2} + 15 \times 12.56 \times (55 - 31.4) - 15 \times 6.28 (31.4 - 5)$$

$$= -12830 \text{ cm}^3$$

$$\sigma_c^{\max} = \frac{-500 \text{ kN} \times 10}{-12830 \text{ cm}^3} \times (-31.4) \text{ cm} = -12.24 \text{ MPa}$$

TENSIONE NELL' ARMATURA INFERIORE

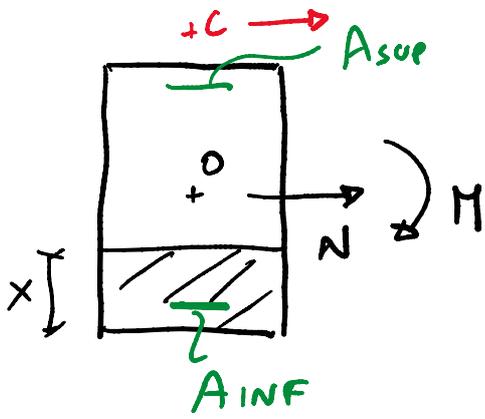
$$\varrho = d-x \Rightarrow \sigma_s = n \left[\frac{N}{S_n} \cdot (d-x) \right] =$$

$$= 15 \times \left[\frac{-500 \text{ kN} \times 10}{-12830 \text{ cm}^3} \times (55 - 31.4) \text{ cm} \right]$$

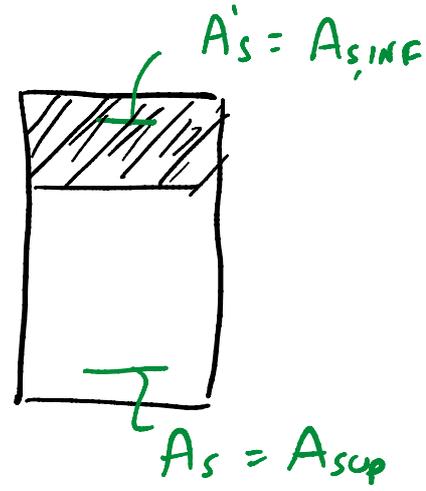
$$\Rightarrow \sigma_s = 137.96 \text{ MPa}$$

VERIFICA IN CASO DI $M < 0$

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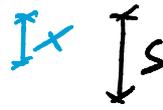
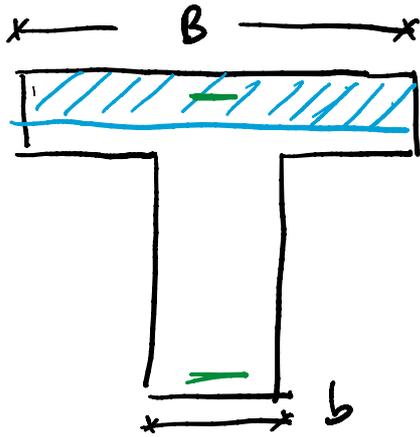


RUOTARE LA
SEZIONE

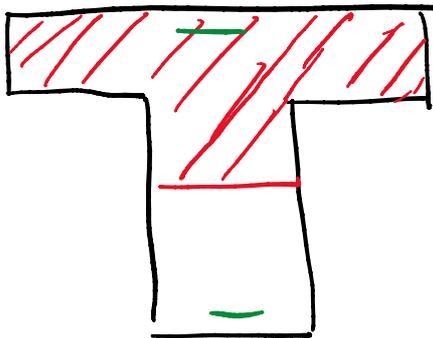


SEZIONI DIVERSE DALLA RETTANGOLARE

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$$e_n = \frac{I_n}{S_n}$$



FISSO x : SE $x \leq d$ \Rightarrow I_n, S_n DA SEZ. RETTANGOLARE $B =$

SE $x > d$ \Rightarrow I_n, S_n DA SEZIONE A T

CONDIZIONE DA IMPORRE $\Rightarrow e_n = \frac{I_n}{S_n}$